

SOLID STATE STUDIES:

TRANSITION IONS IN ZINC OXIDE

VOLUME II

A thesis presented for the
degree of Doctor of Philosophy in Physics
in the University of Canterbury,
Christchurch, New Zealand.

by

R S Anderson

R. S. Anderson

1967.

TABLE OF FIGURES, APPENDICES, AND PROGRAM LISTINGS

FIGURES

- 1.1 The ZnO Wurtzite Structure
 - 2 Free Ion Parameters for the First Transition Series
 - 3 Tanabe - Sugano Fit for Ni^{++} -ZnO
 - 4 Electron-vibration Interaction
- 2.1 PbF_2/ZnO Phase Diagram
 - 2 Conversion of On/Off to Proportional Control
 - 3 Thermocouple Break Protection Circuit
 - 4 Voltage Production Circuit
 - 5 Gear Mesh for Oscillate
 - 6 Sweep Drive
 - 7 Oscillatory Drive
 - 8 Oscillating Set Point Control Panel
 - 9 Oscillating Set Point Rear
 - 10 Schmitt Trigger Circuit
 - 11 Schmitt Trigger
 - 12 Furnace Controller Logic
 - 13 Variac and Furnace Front
 - 14 Furnace and Control
 - 15 Temperature/Current Plot of Furnace Operation
 - 16 Furnace Controller and Recorder
 - 17 Temperature Record of a Growing Run
 - 18 Crucibles in Brick
 - 19 Crucibles in Furnace
 - 20 Ni - ZnO Sample 6
 - 21 Co - ZnO Sample 7
- 3.1 Bausch and Lomb Schematics
 - 2 Bausch and Lomb Sample Focus
 - 3 Vibration Effects
 - 4 Bausch and Lomb Internal Modifications
 - 5 Reference Beam Filter Holder
 - 6 Slit-limited Resolution
 - 7 Quantitative Effect
 - 8 Overlapping Orders in Absorption

3.9 Ni - ZnO on Jarrell-Ash

- 10 The Jarrell-Ash Condenser System
- 11 A Schematic Jarrell-Ash Chart

4.1 Andonian Dewar Operation

- 2 Sample Holder Disassembled
- 3 Sample Holder in Position
- 4 Polaroid Slide for Dewar
- 5 Polaroid Spectrum
- 6 Bausch and Lomb Dewar Assembly
- 7 Jarrell-Ash Assembly

6.1 Ni - ZnO Low Doping Axial Spectrum

- 2 Temperature Dependence of the Ni - ZnO Axial Spectrum (Sample 21)
- 3 Ni - ZnO Axial Spectrum at 10°K
- 4 Ni - ZnO E//C at 14°K
- 5 Ni - ZnO E⊥C Variation of Spectrum with Temperature
- 6 Ni - ZnO E//C Variation of Spectrum with Temperature
- 7 7°K Axial Spectrum (Jarrell-Ash)
- 8 Temperature Dependence of Axial Jarrell-Ash Spectrum
- 9 Jarrell-Ash Sigma Spectrum
- 10 Jarrell-Ash Pi Spectrum
- 11 Histograms of Spectral Components for two Different Ni Dopings
- 12 Concentration Dependence of Weak Lines (Jarrell-Ash)
- 13 Sharp Line Temperature Dependence (Jarrell-Ash)
- 14 Temperature Dependence of Sharp Line Areas (Jarrell-Ash)
- 15 Total Integrated Absorption of Ni - ZnO Visible Band
- 16 Band Shape Fitting Ni - ZnO Sigma
- 17 Ni - ZnO Pi Band Shape Fitting
- 18 Temperature Dependence of Weak Line Areas

7.1 d⁸ Under Decreasing Perturbations

- 2 Pairs in Ni - ZnO
- 3 d² Cubic Field Energy Levels and Parameter Dependence
- 4 Depopulation and Band Intensity

- 7.5 Parameter Dependence of d^8 First Excited State
 - 6 v and v' Dependence of Splittings
 - 7 Trigonal Field Levels and Parameter Dependence
 - 8 Wurtzite $k = 0$ Modes
 - 9 Peaks in the ZnO Phonon Distribution
 - 10 Phonon Fitting for the Ni - ZnO Visible Bands
- 8.1 Co - ZnO 0.05% Axial Spectrum
 - 2 Co - ZnO 0.17% Axial Spectrum
 - 3 Temperature Dependence of Axial Spectrum
 - 4 Axial Spectrum (Jarrell-Ash)
 - 5 Pi Spectrum (Jarrell-Ash)
 - 6 Concentration Dependence of Weak Lines
 - 7 The No-Phonon Lines
 - 8 Phonon Fitting for the Co - ZnO Axial Spectrum.
- A1 Correction to Apparent Absorbance for a Crystal Wedge
- A2 Apparent Intensity of Slit-Limited Absorption Lines

APPENDICES

- 1 Heat Flow in the Sample Holder and Sample
- 2 Absorbance of a Wedge-Shaped Crystal
- 3 Instrumental Effects in Spectra
- 4 d^2 Trigonal Matrices
- 5 Cell Theory Program

PROGRAM LISTINGS

Cell Theory
 Absorbance Program 1
 Absorbance Program 2
 Fit Gauss or Lorentz Lines to Spectrum
 (Spectral Line Optimisation Program)
 Look for Similar Spacings in an Energy Table
 (Wave Number Differences)
 Common Differences Table
 Matrix Diagonalisation
 Program to Read Matrices in Surd Form
 Energy Table and Parameter Dependence.

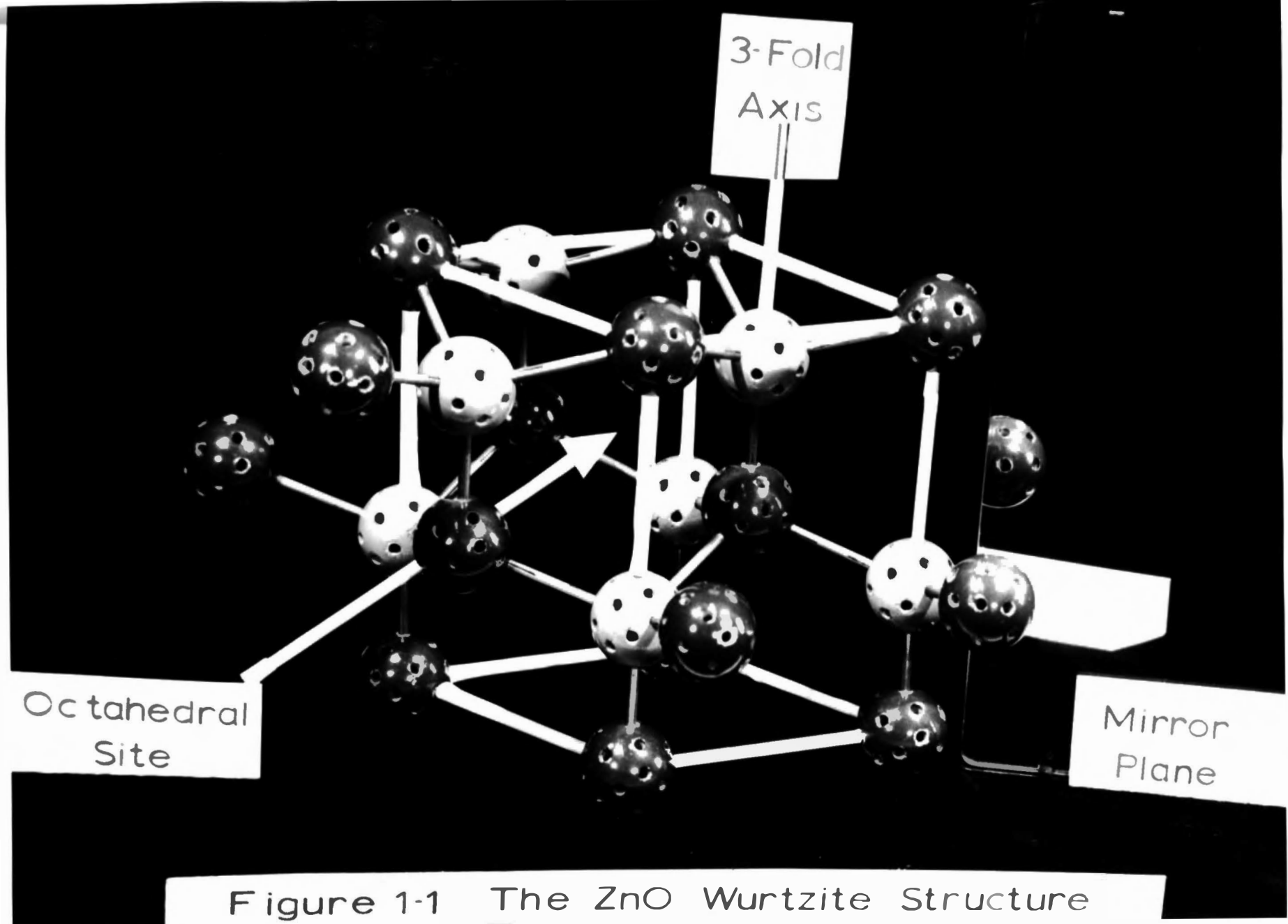
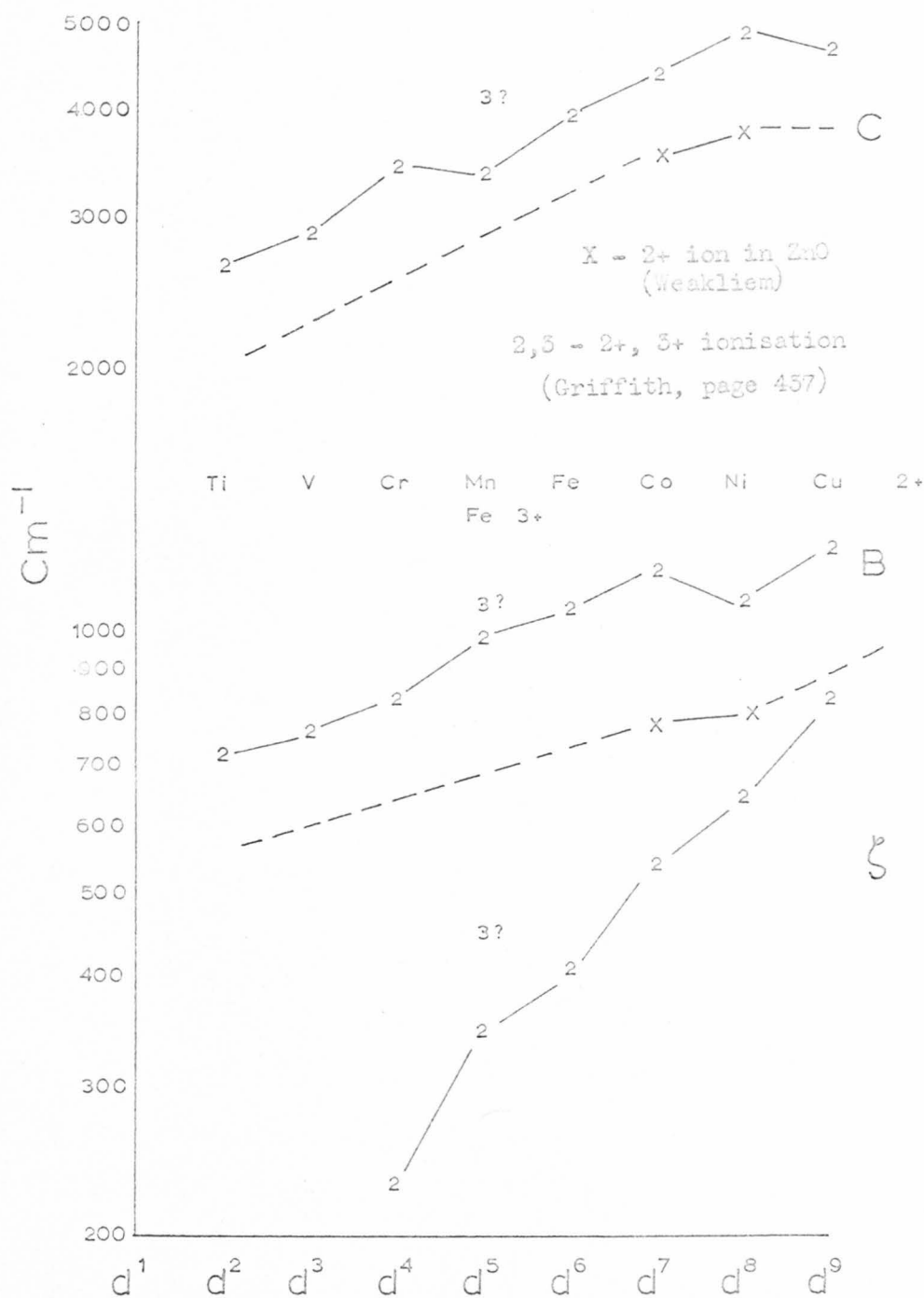


Figure 1-2 Free Ion Parameters for the First Transition Series



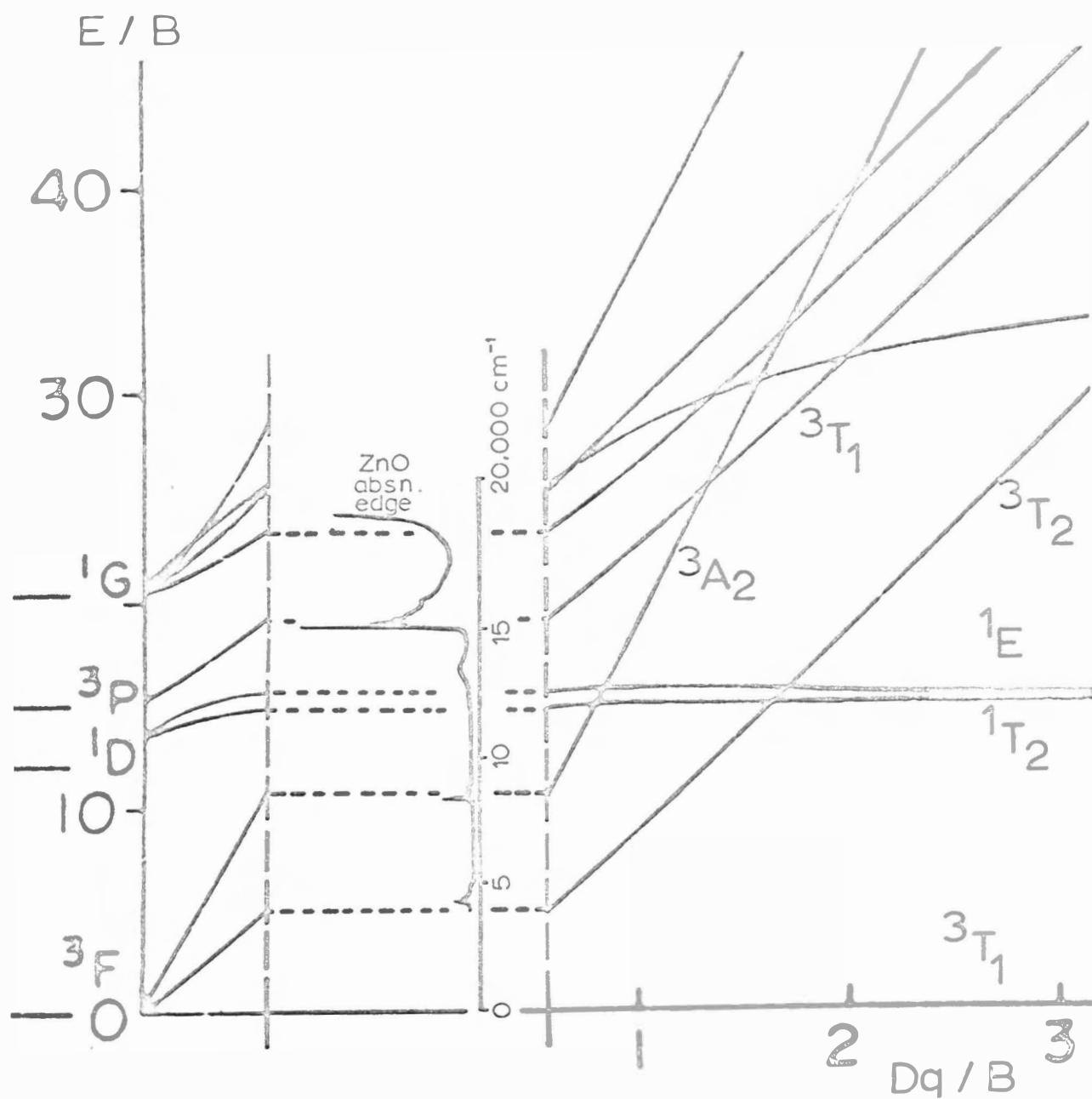
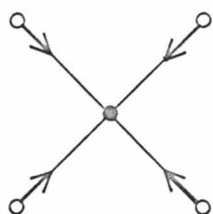


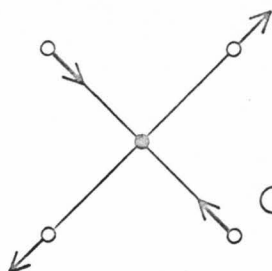
Figure 1-3 Tanabe-Sugano Fit
for Ni^{2+} -ZnO

Figure 1-4 Electron-Vibration Interaction

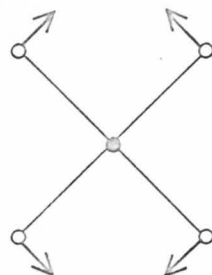
a Normal modes of Square Planar Complex



Q_1

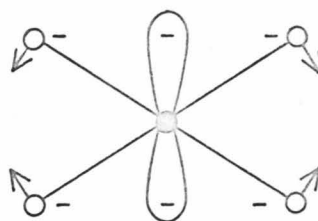


Q_2

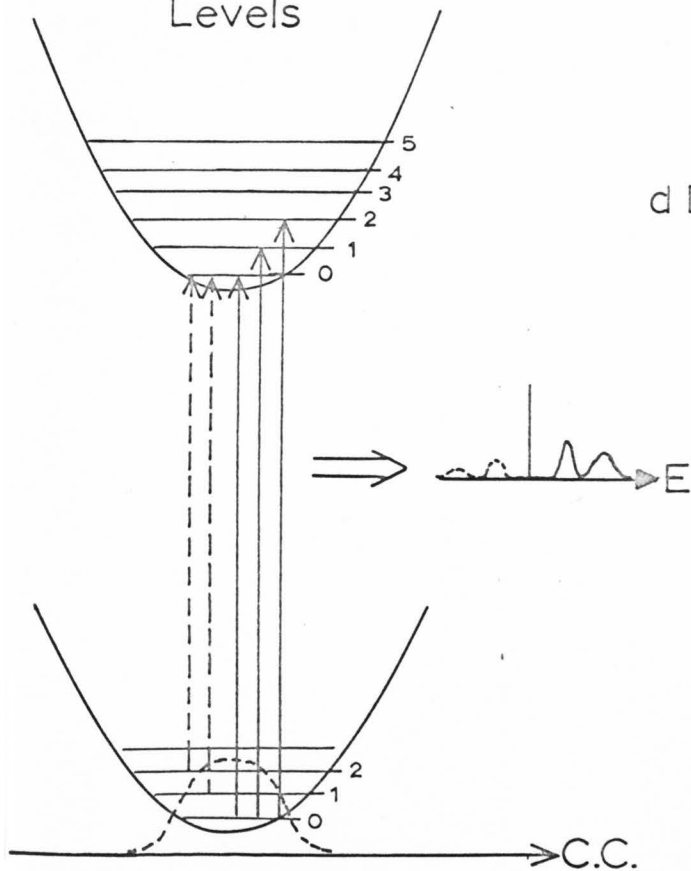


Q_3

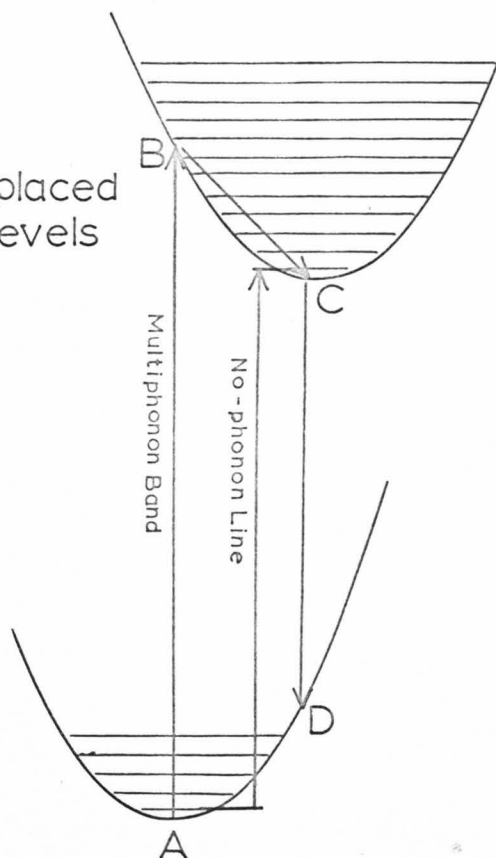
b Distortion by a Transition Ion



c Vibronic Energy Levels



d Displaced Levels



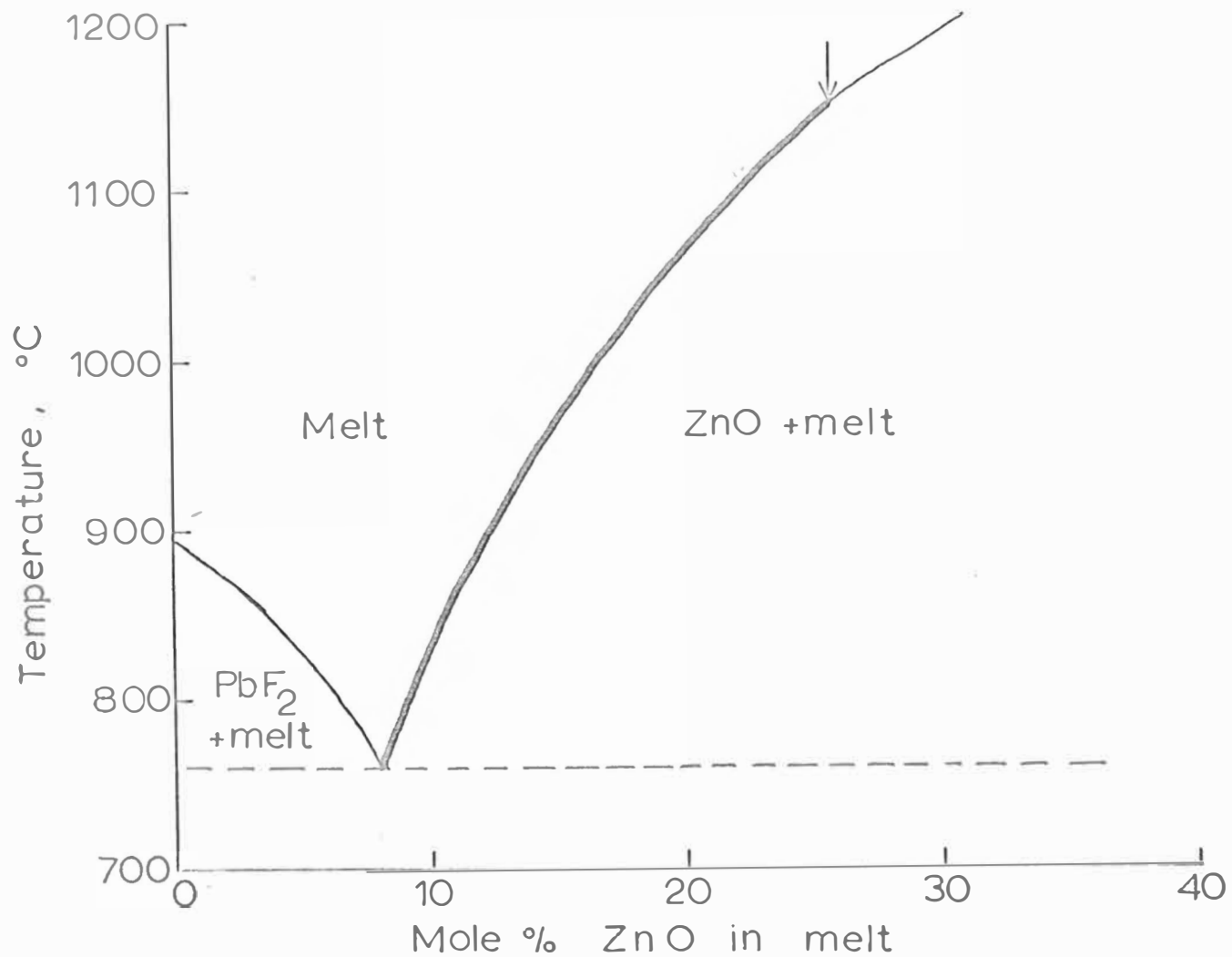


Figure 2-1 PbF_2 / ZnO Phase Diagram

Figure 2-2 Conversion of On/Off to Proportional Control

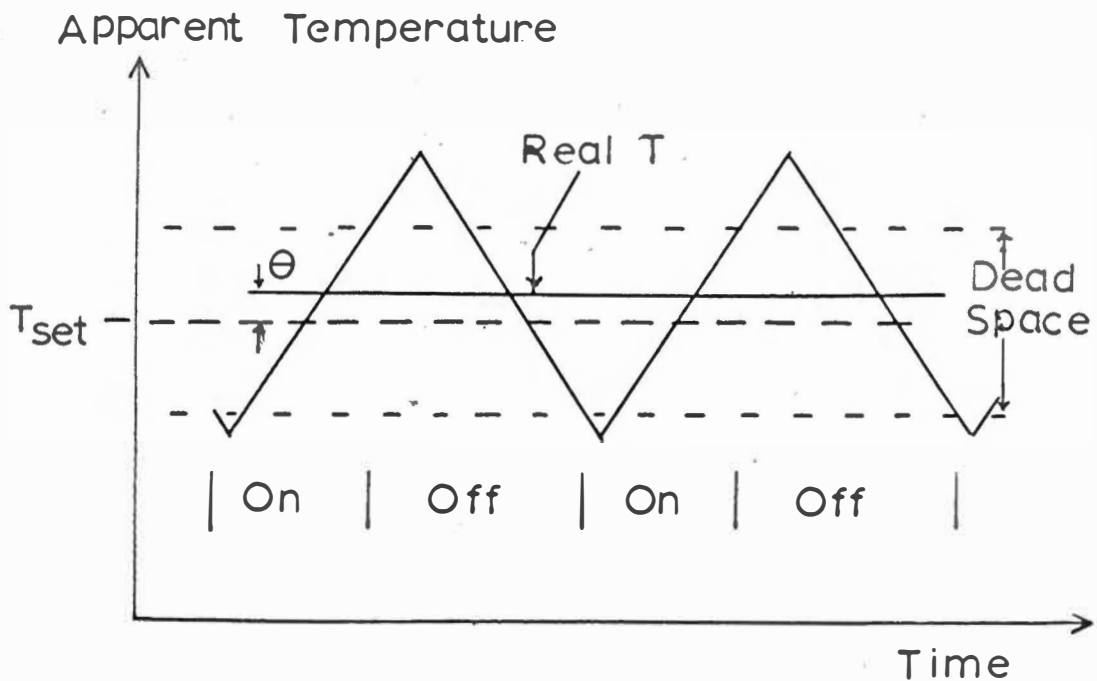


Figure 2-3 Thermocouple Break Protection Circuit

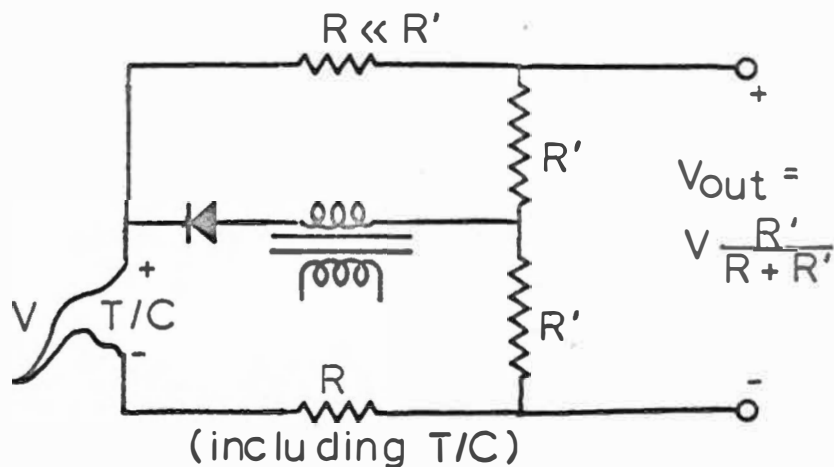


Figure 2-4 Voltage Production Circuit

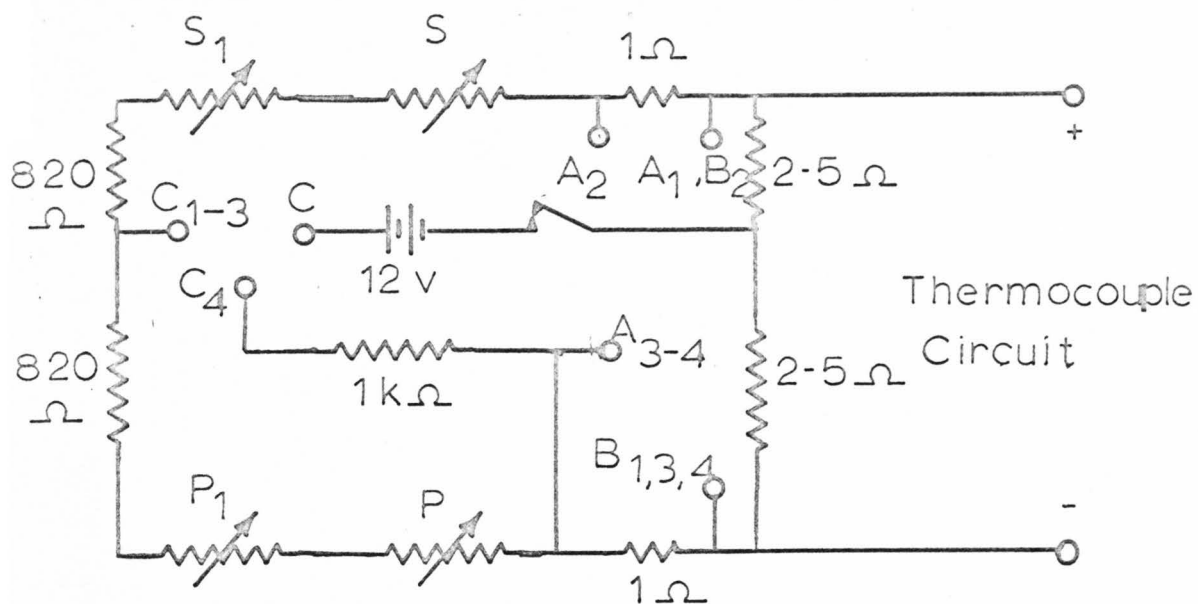
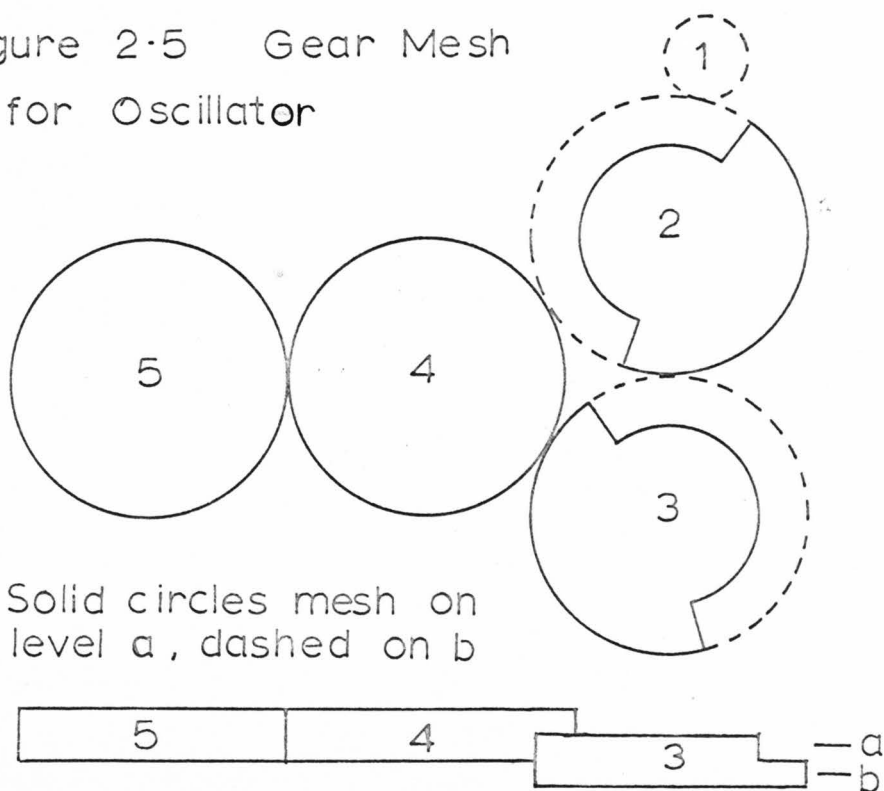


Figure 2-5 Gear Mesh for Oscillator



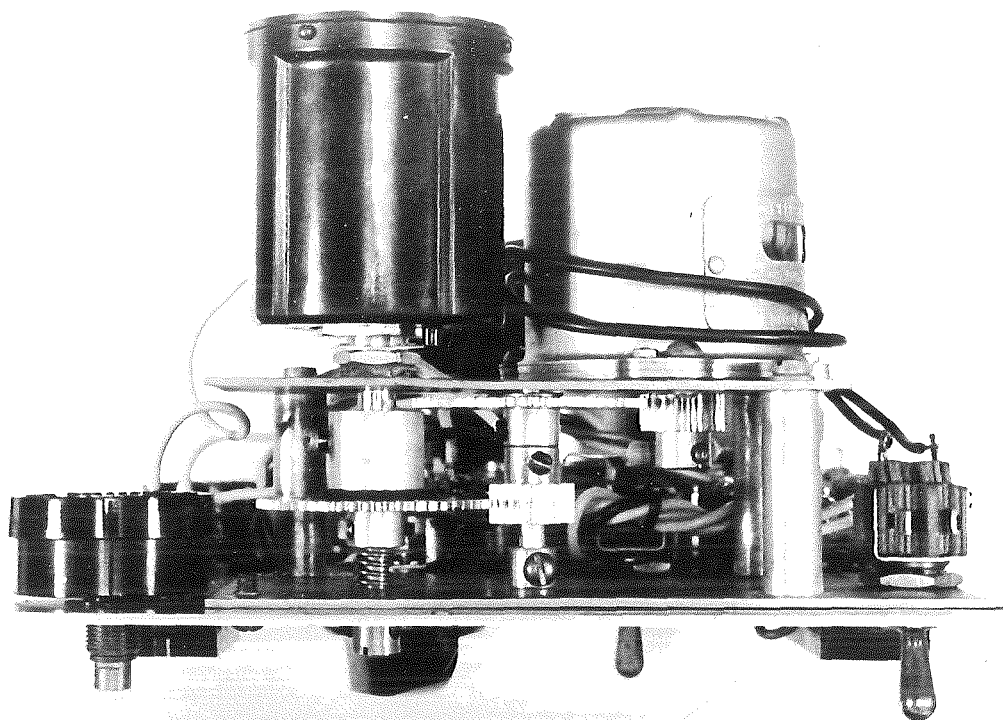
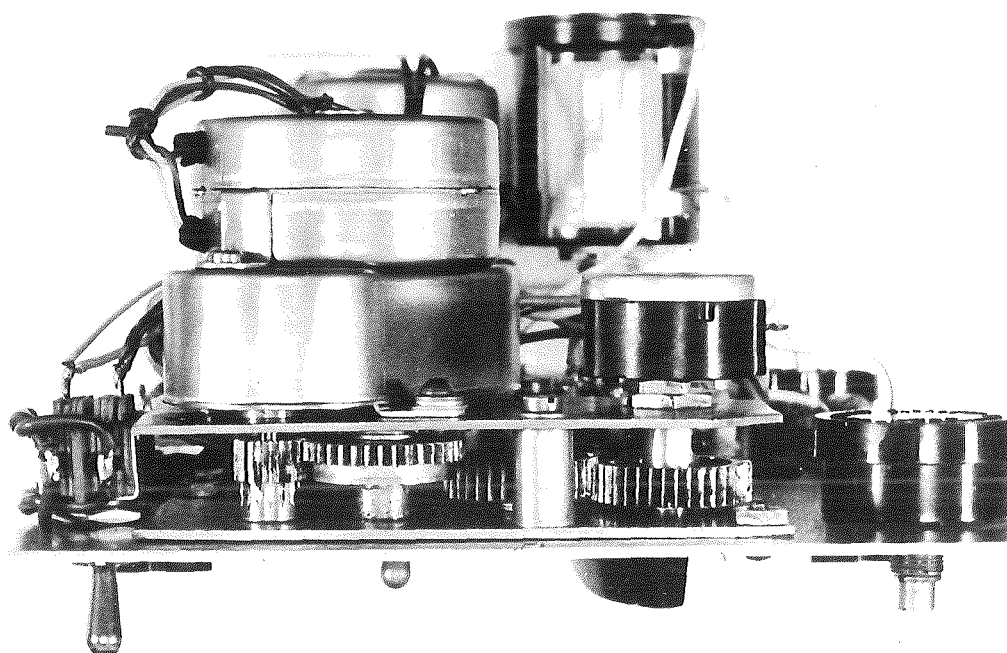


Figure 2-6 Sweep drive

Figure 2-7 Oscillatory drive



Oscillating set point control

Figure 2-8 Panel

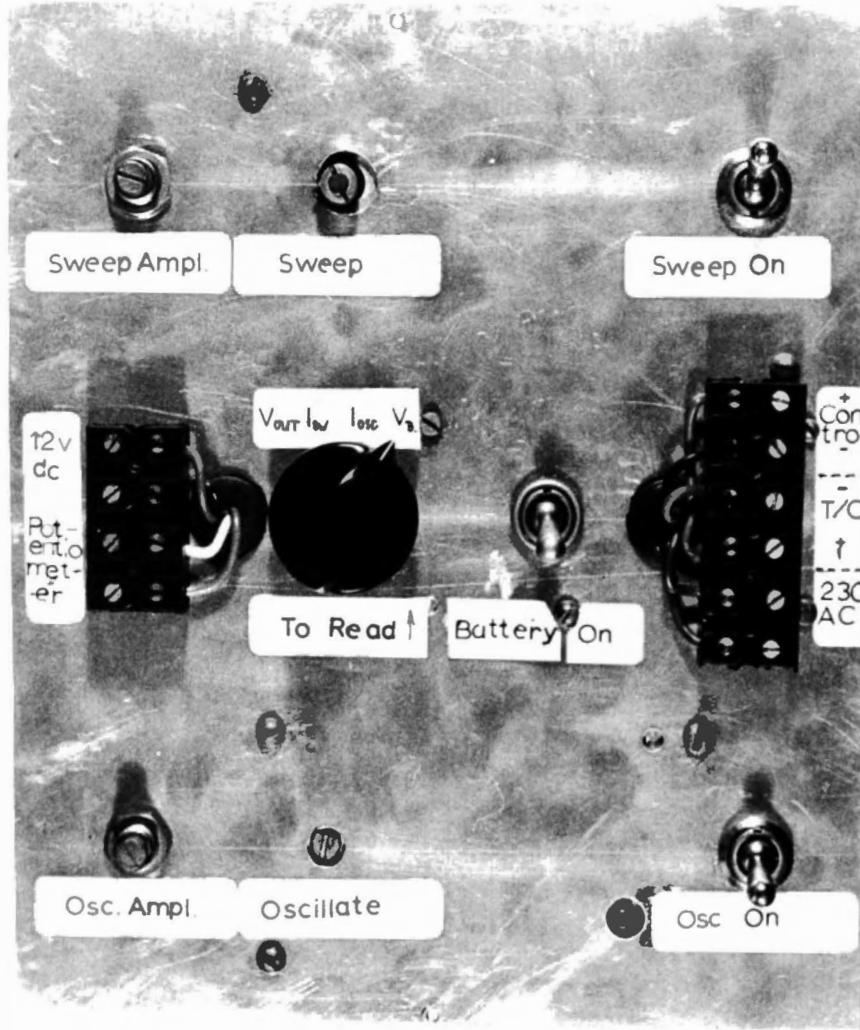
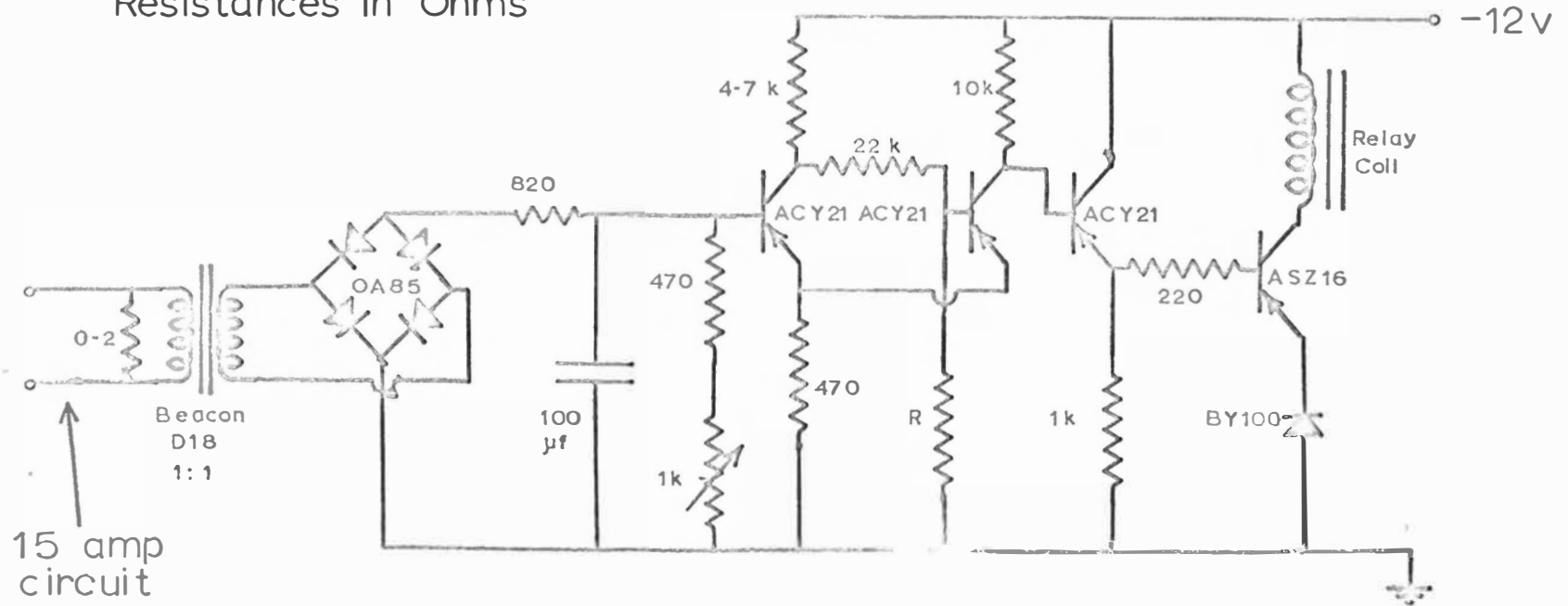


Figure 2-9 Rear



Figure 2-10 Schmitt Trigger

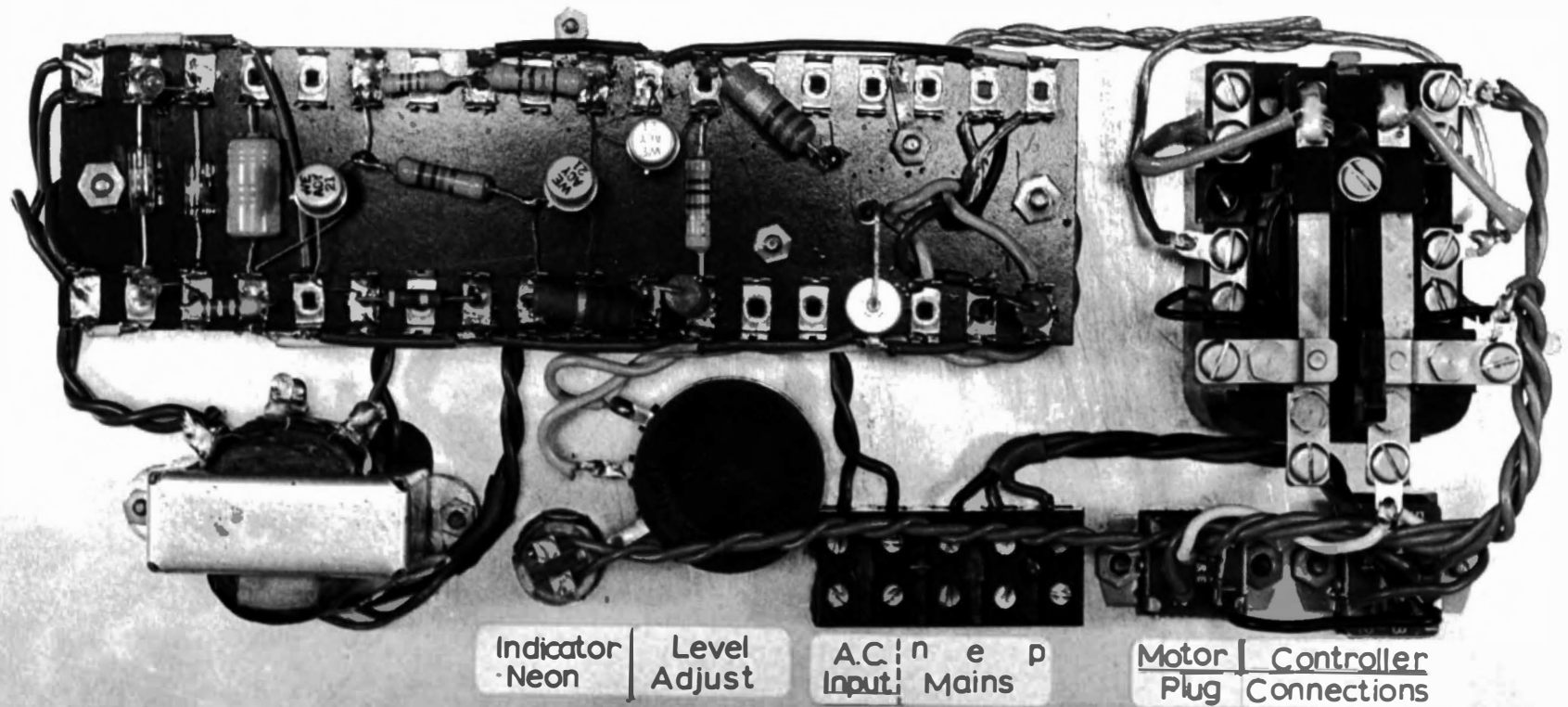
Resistances in Ohms



R for best performance 2420

Relay - Arrow 28308U with 12v coil

Figure 2-11 Schmitt Trigger



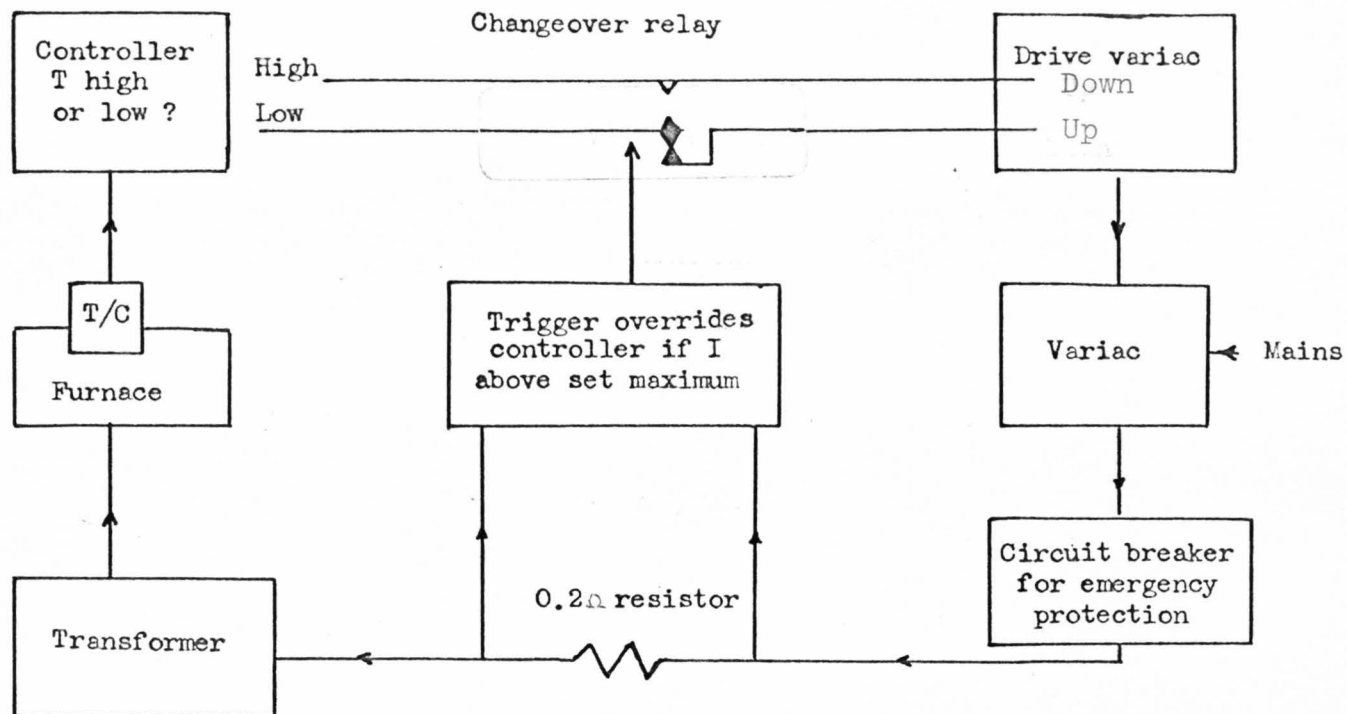
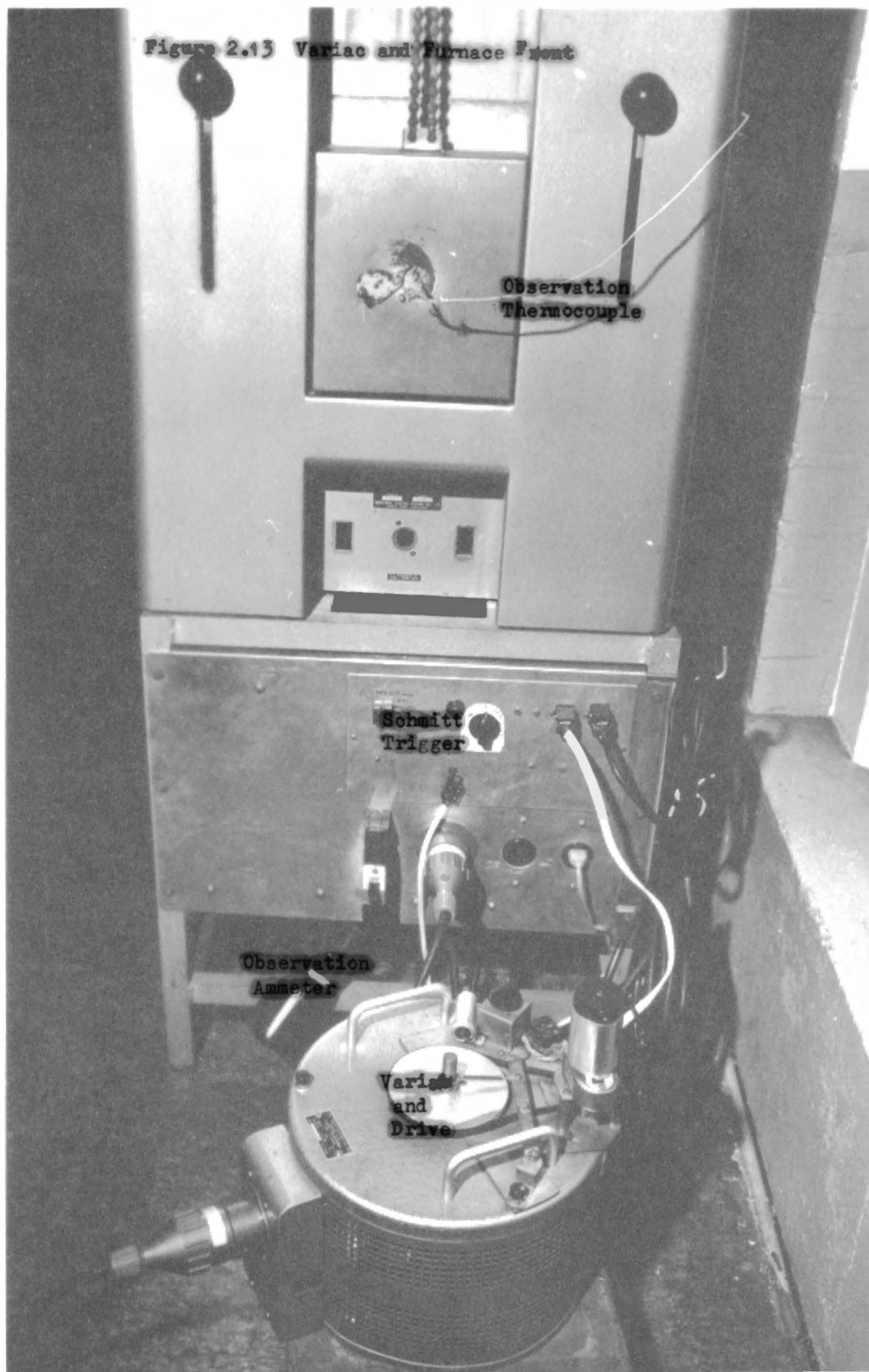


Figure 2.12 Furnace Controller Logic

Figure 2.13 Variac and Furnace Front





On-Off
Controller

Proportional
Controller

Batteries

Furnace

Observation
Thermocouple

Potentiometer

Recorder

Trigger

Transformer

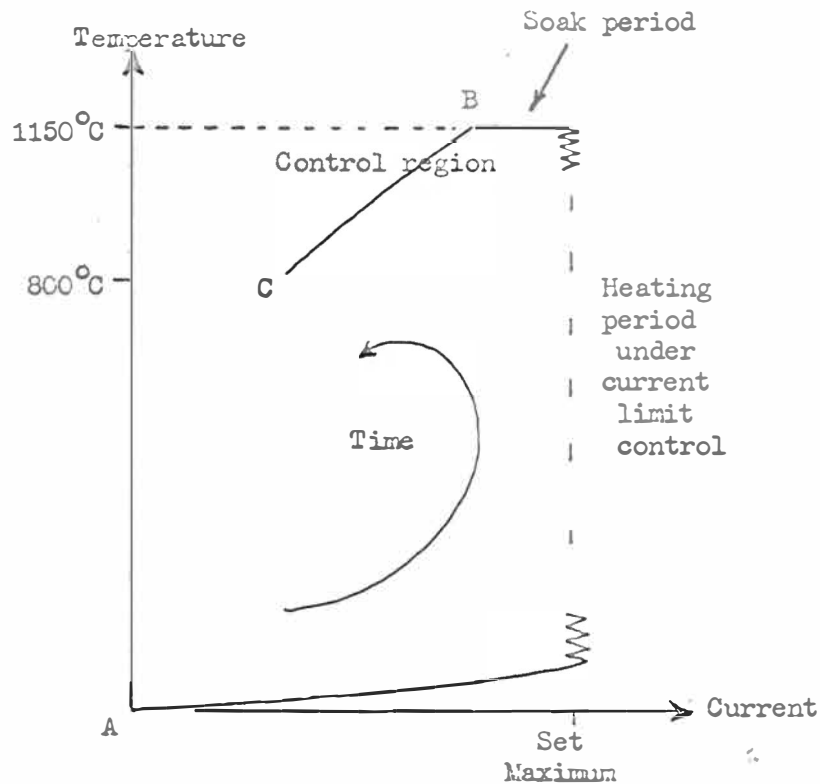
Variac

Figure 2.14
Furnace and Control



Figure 2.15

Temperature / Current Plot of
Furnace Operation



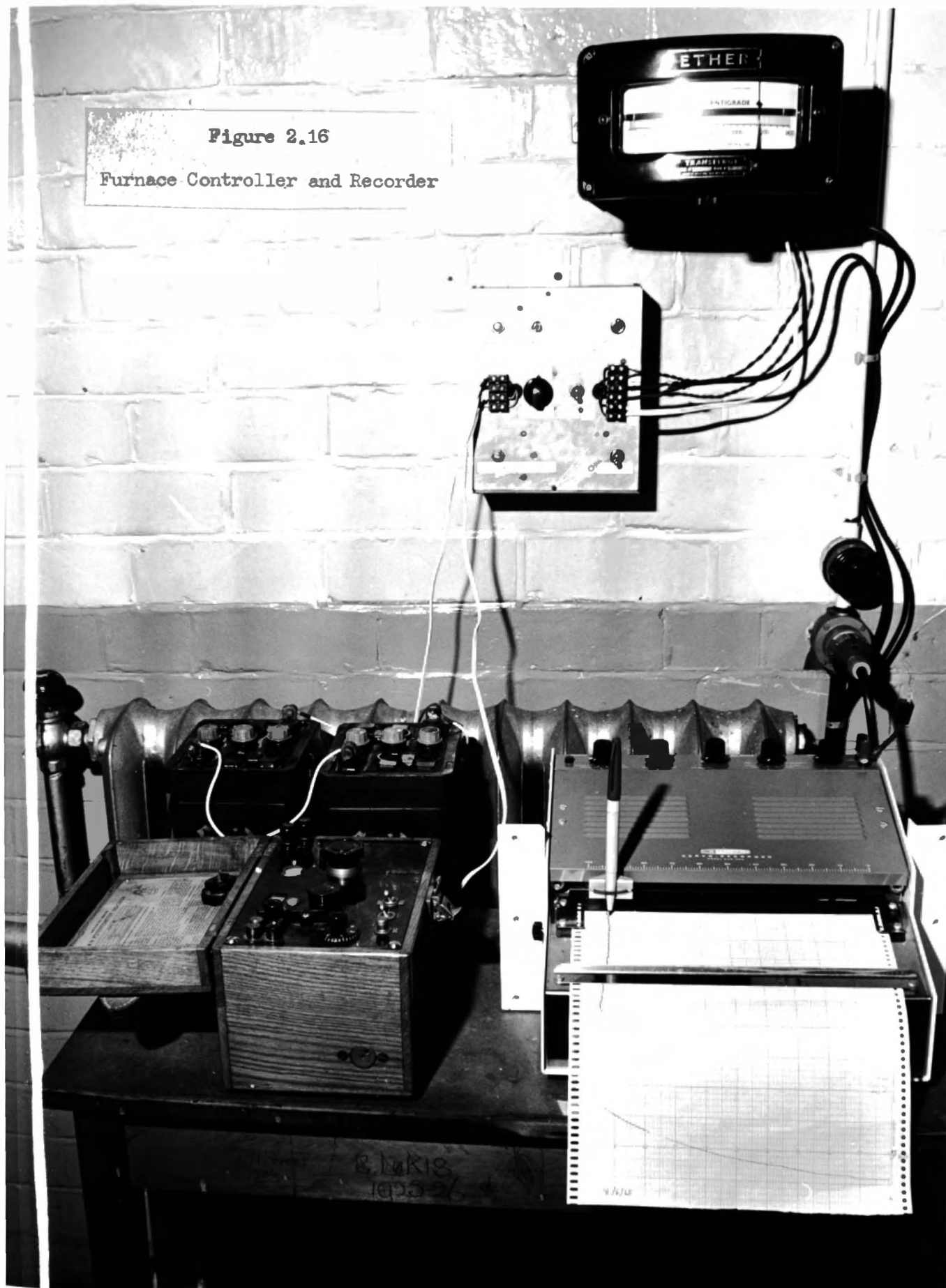
OPERATOR CONTROL

- A Turn on all but sweep motor
- B Start sweep motor after sufficient soak period
- C Turn complete system off when temperature low enough

At A, the variac should be set to a low voltage before switching on, so that the starting current is not too large.

Figure 2.16

Furnace Controller and Recorder



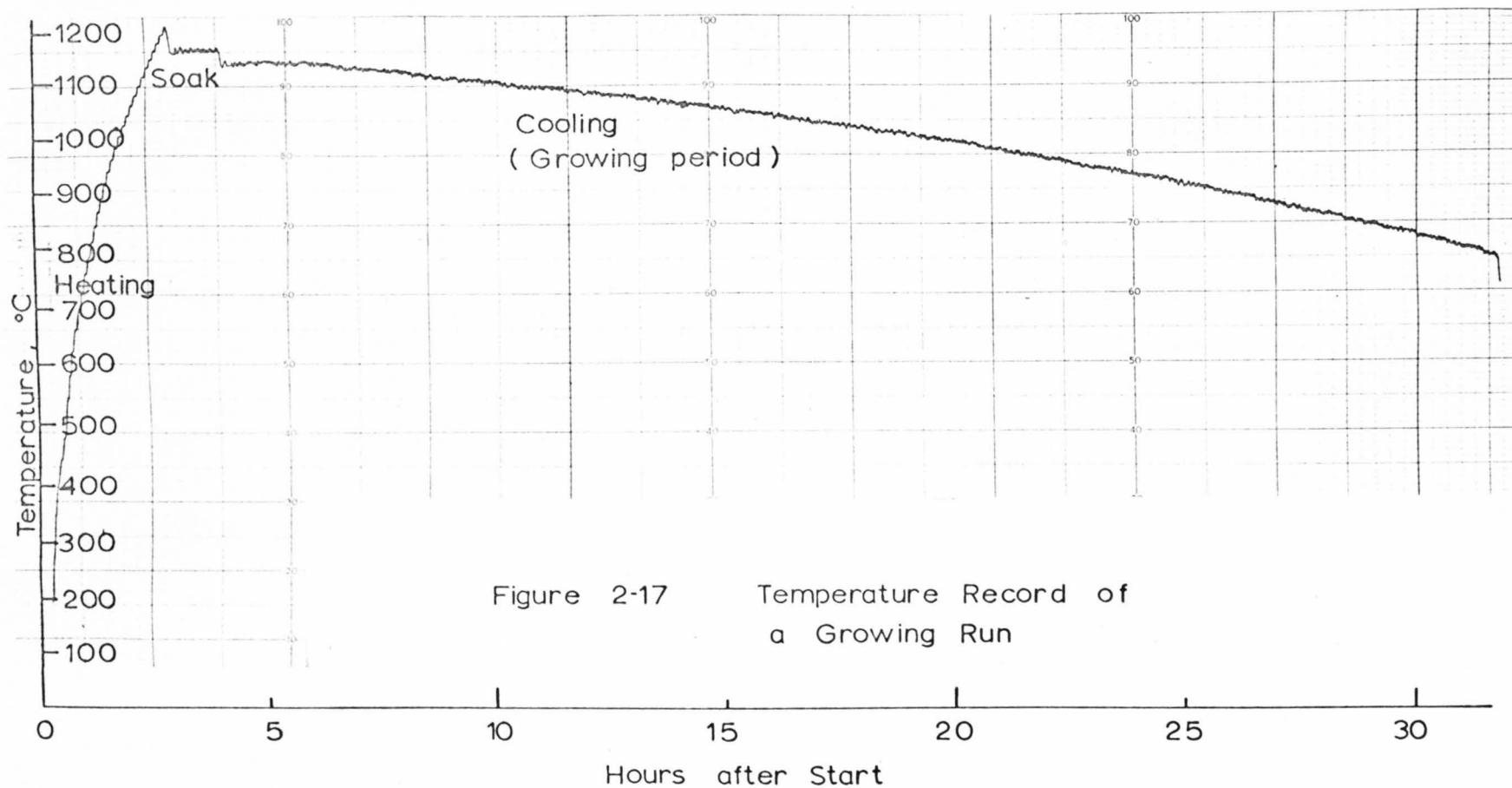


Figure 2-18 Crucibles in brick
Scale in inches

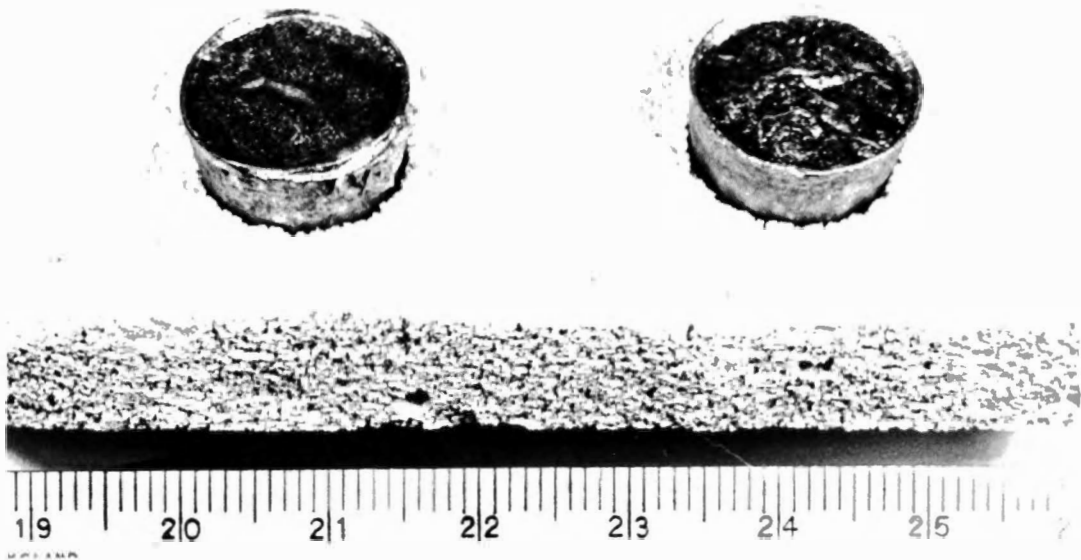


Figure 2-19 Crucibles in furnace



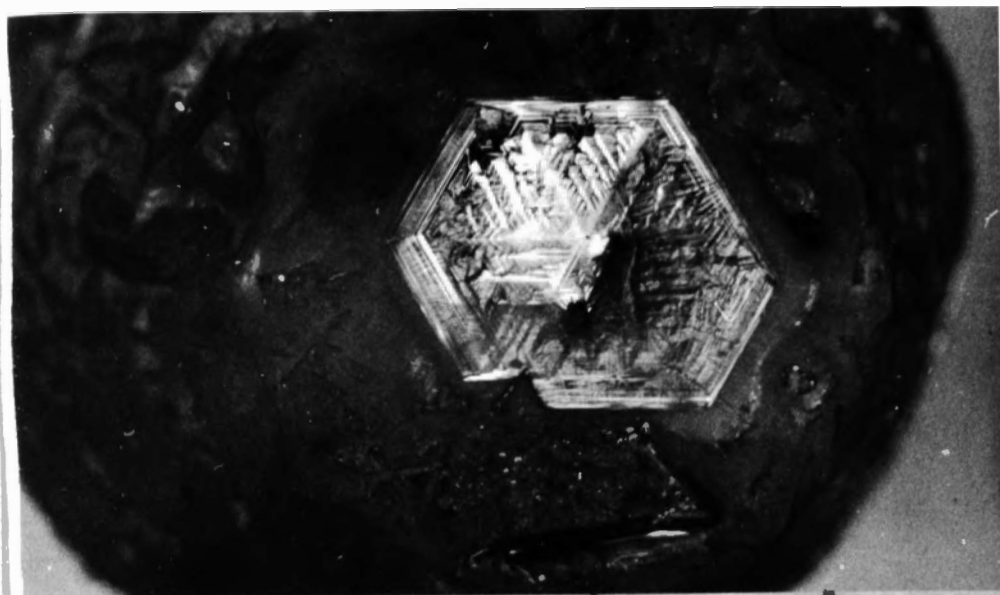


Figure 2-20
 $\text{Ni}^{++}\text{-ZnO}$
Sample 6



Scale in cm



Figure 2-21
 $\text{Co}^{++}\text{-ZnO}$
Sample 7

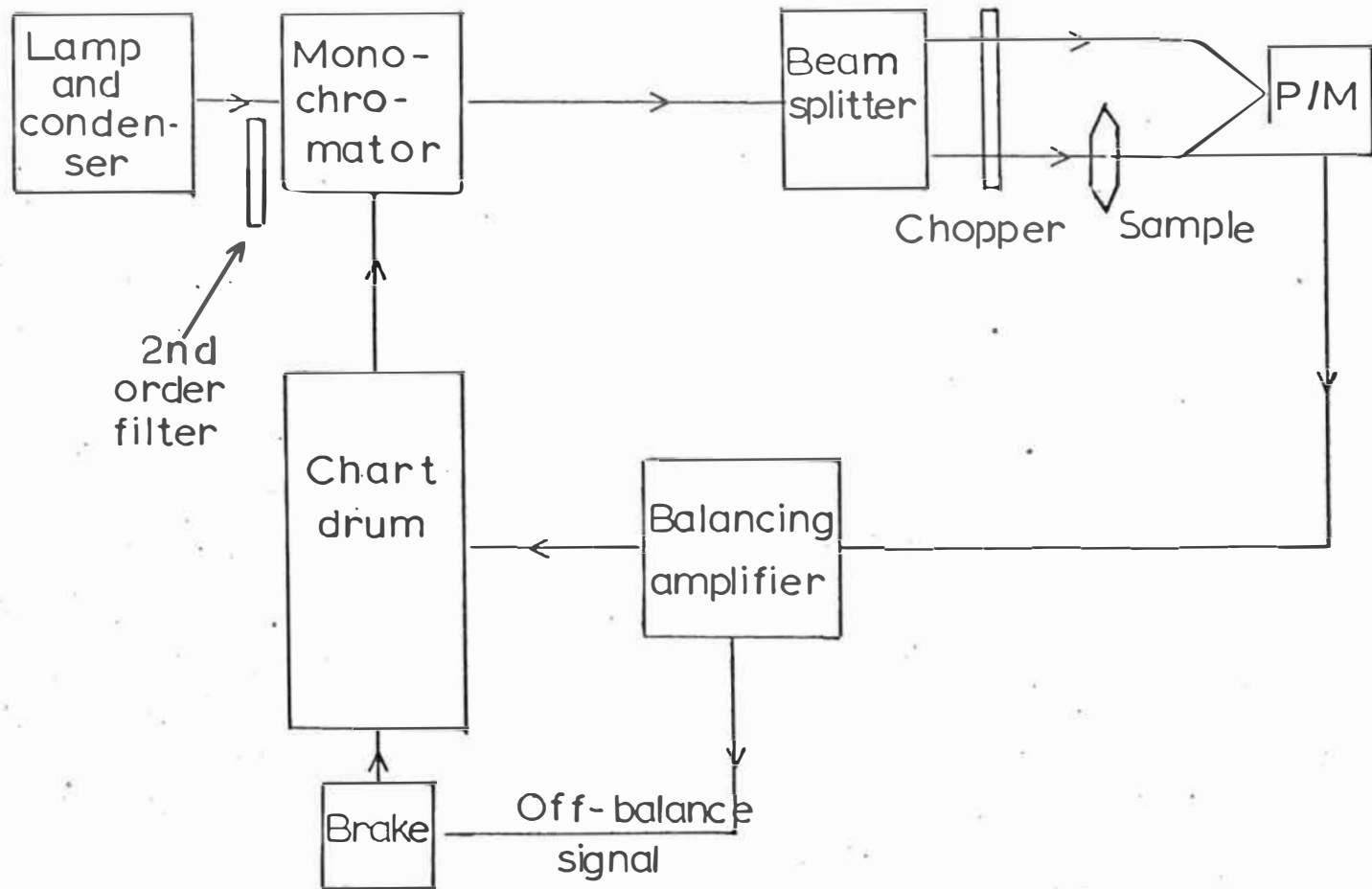
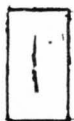


Figure 3-1 Bausch and Lomb Schematics

Figure 3-2

Bausch and Lomb
Sample focus

Mirror
Condenser



Lens
Condenser



Figure 3-3
Vibration effects

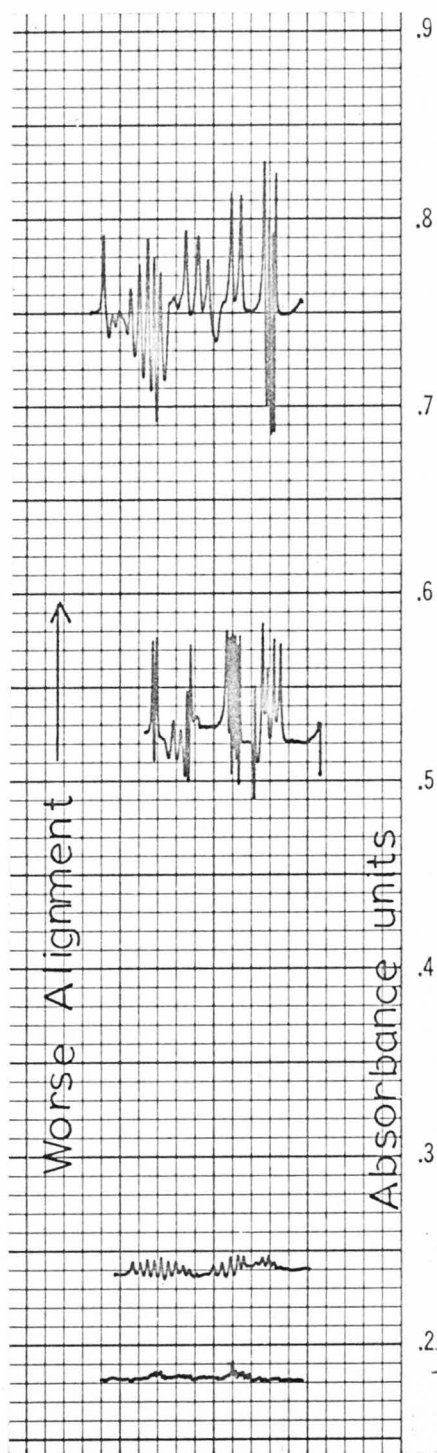


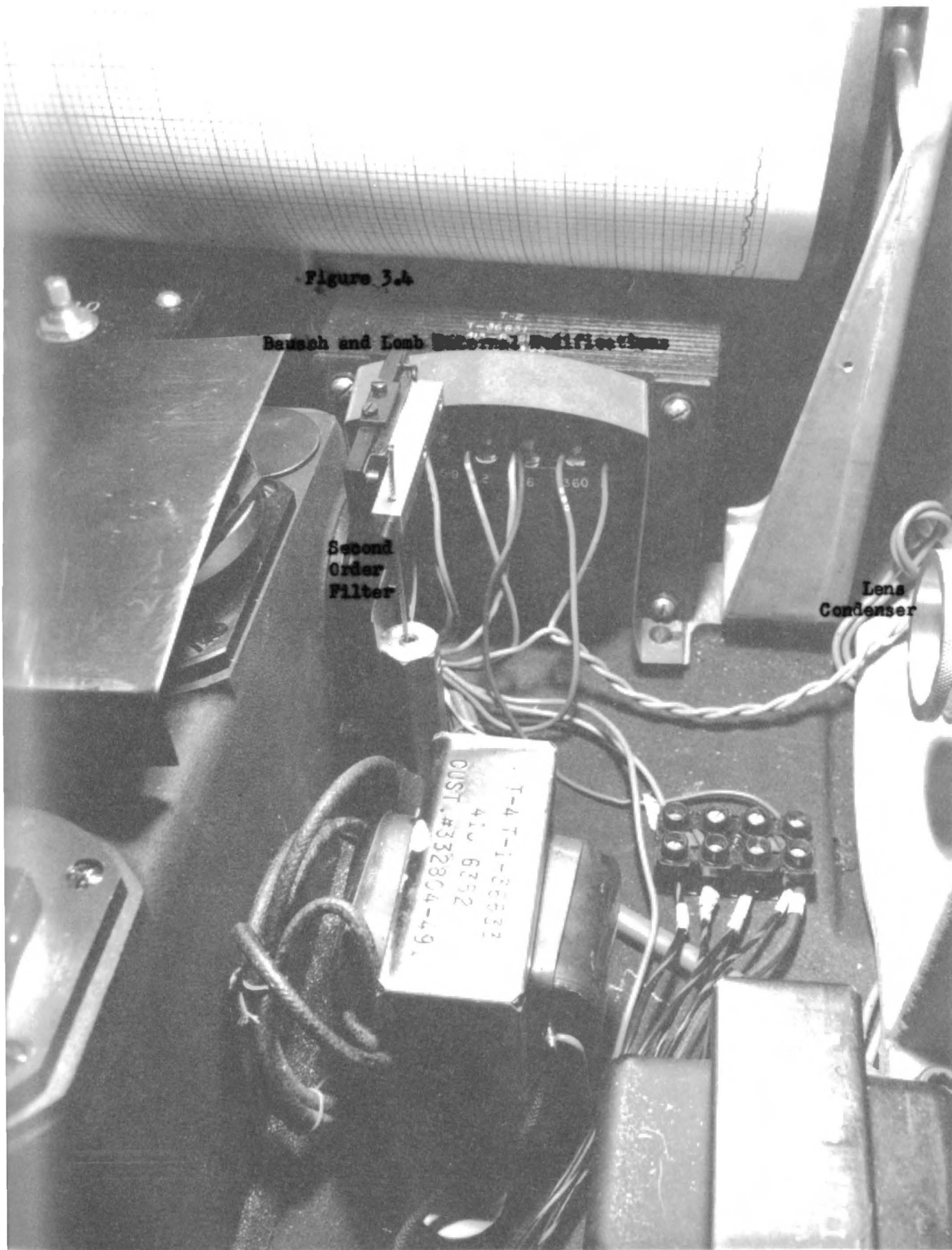
Figure 3.4

Bausch and Lomb ~~Internal Modifications~~

Second
Order
Filter

Lens
Condenser

T-4-T-1-36622
410 6752
CUST. #332804-49



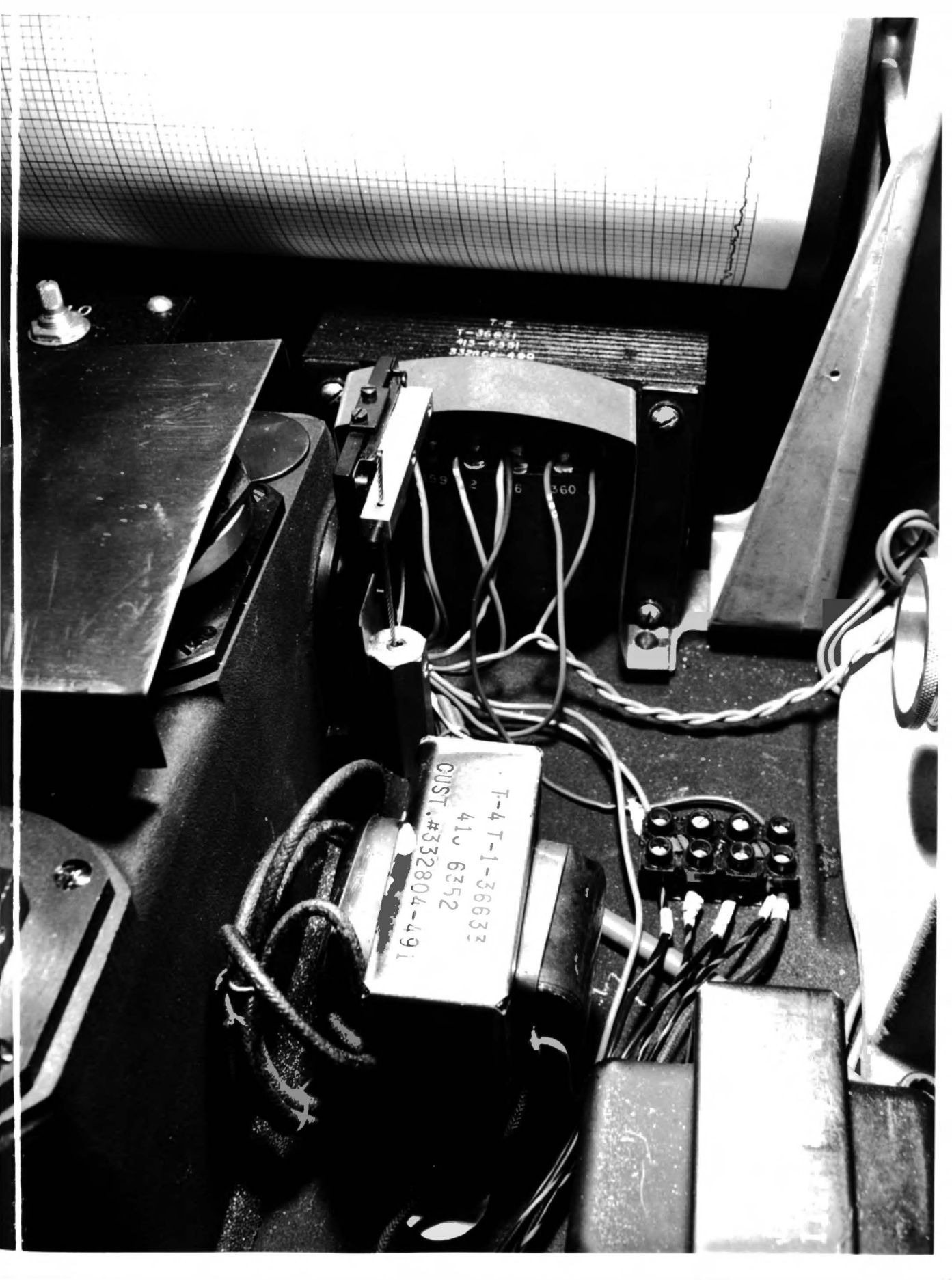


Figure 3-5

Reference beam Filter
Holder



Figure 3-6 Slit-limited Resolution

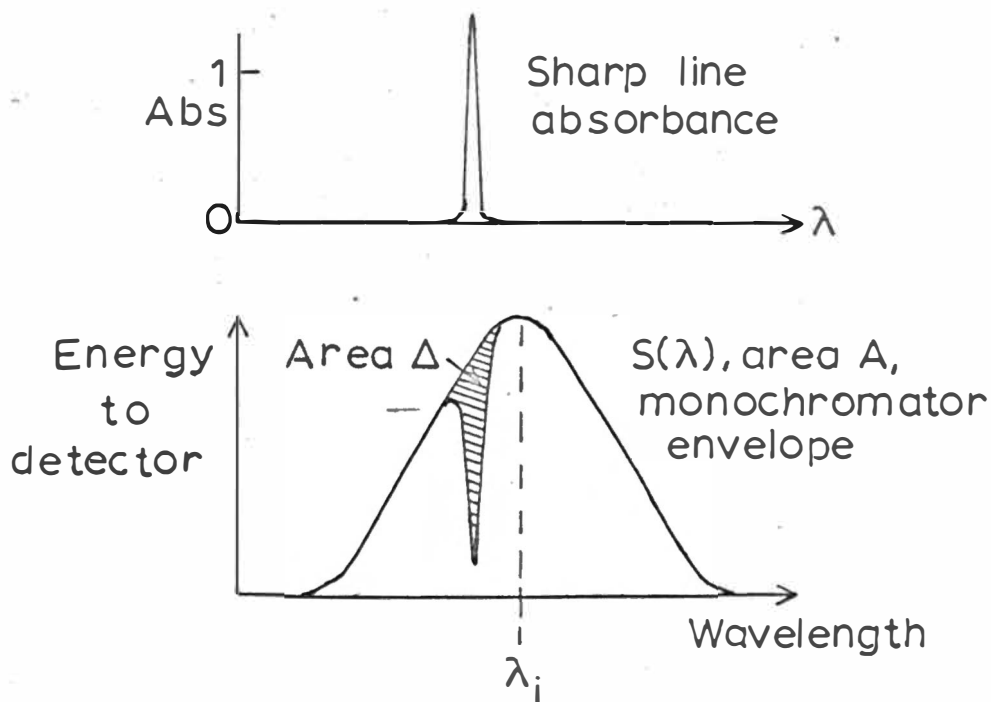


Figure 3-7 Quantitative Effect

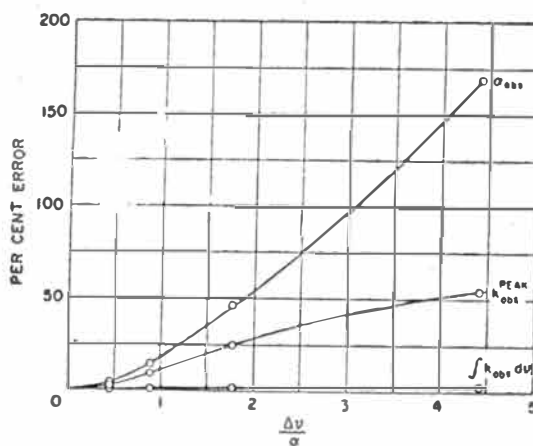


FIG. 1. Error made in direct measurement of line width, peak absorption coefficient, and line intensity as function of ratio of spectral slit width to line half-width for a single Lorentz line with 30% peak absorption and a Gauss slit function.

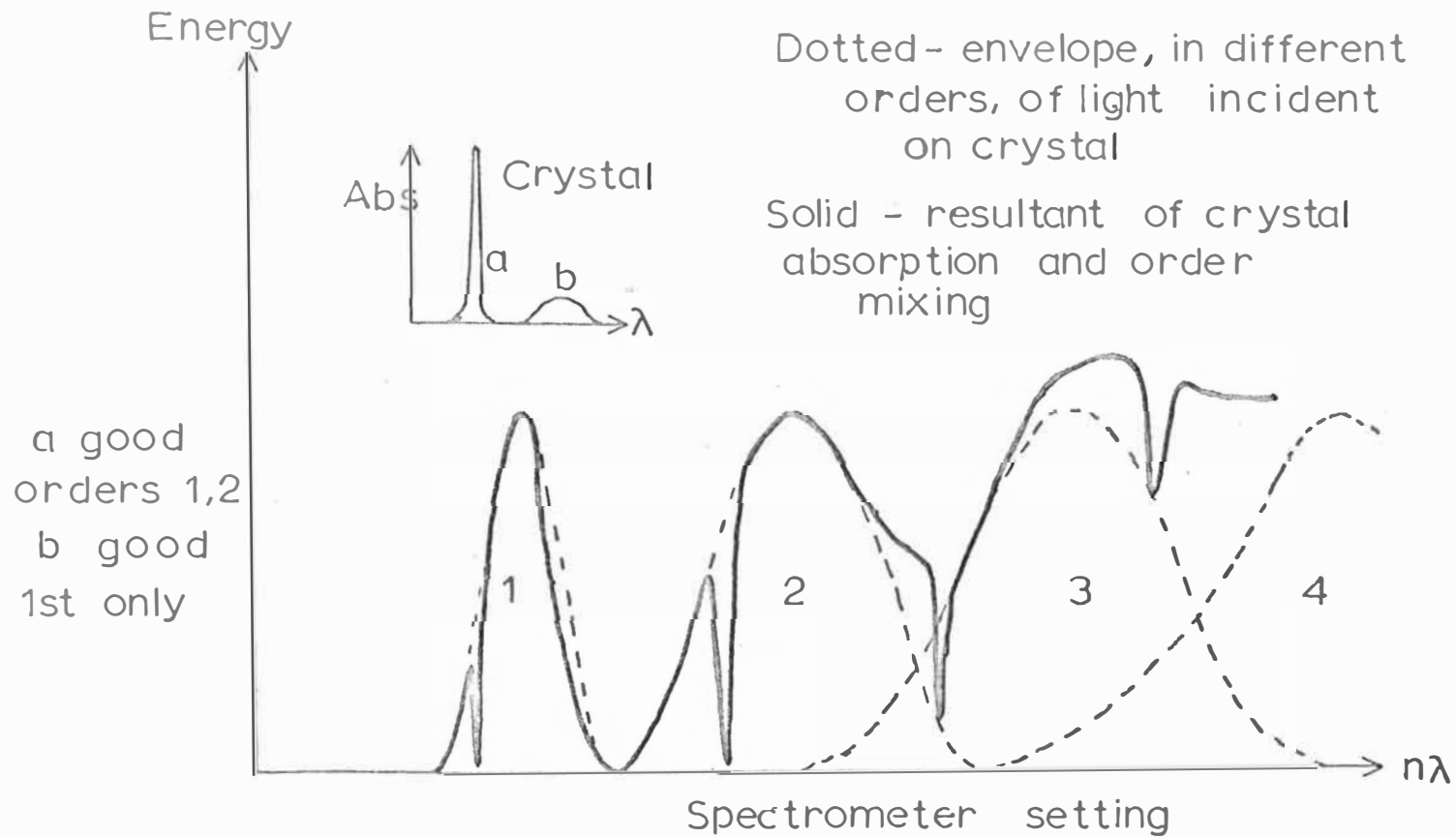


Figure 3-8 Overlapping Orders in Absorption

Figure 3-9 Ni - ZnO on Jarrell-Ash

Figure 3-9 a
Ni⁺⁺-ZnO
Raw Data

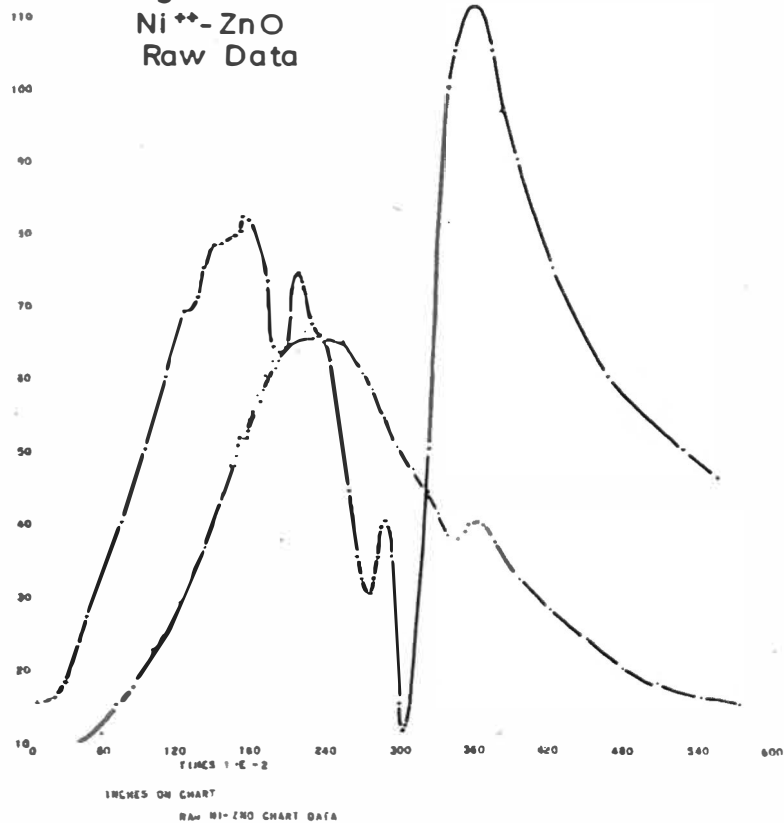
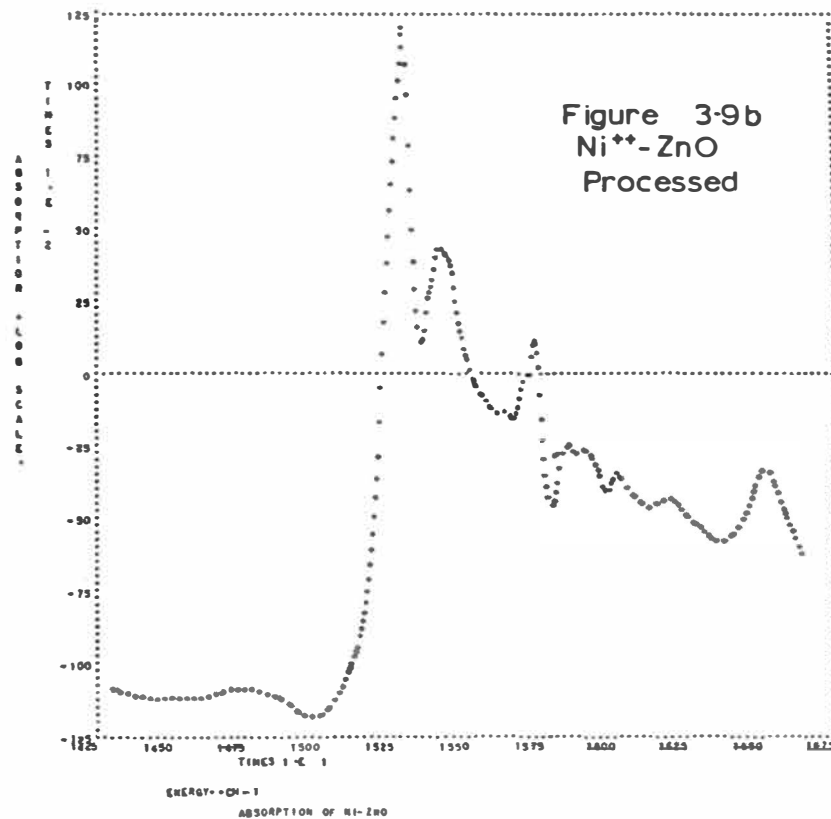


Figure 3-9 b
Ni⁺⁺-ZnO
Processed



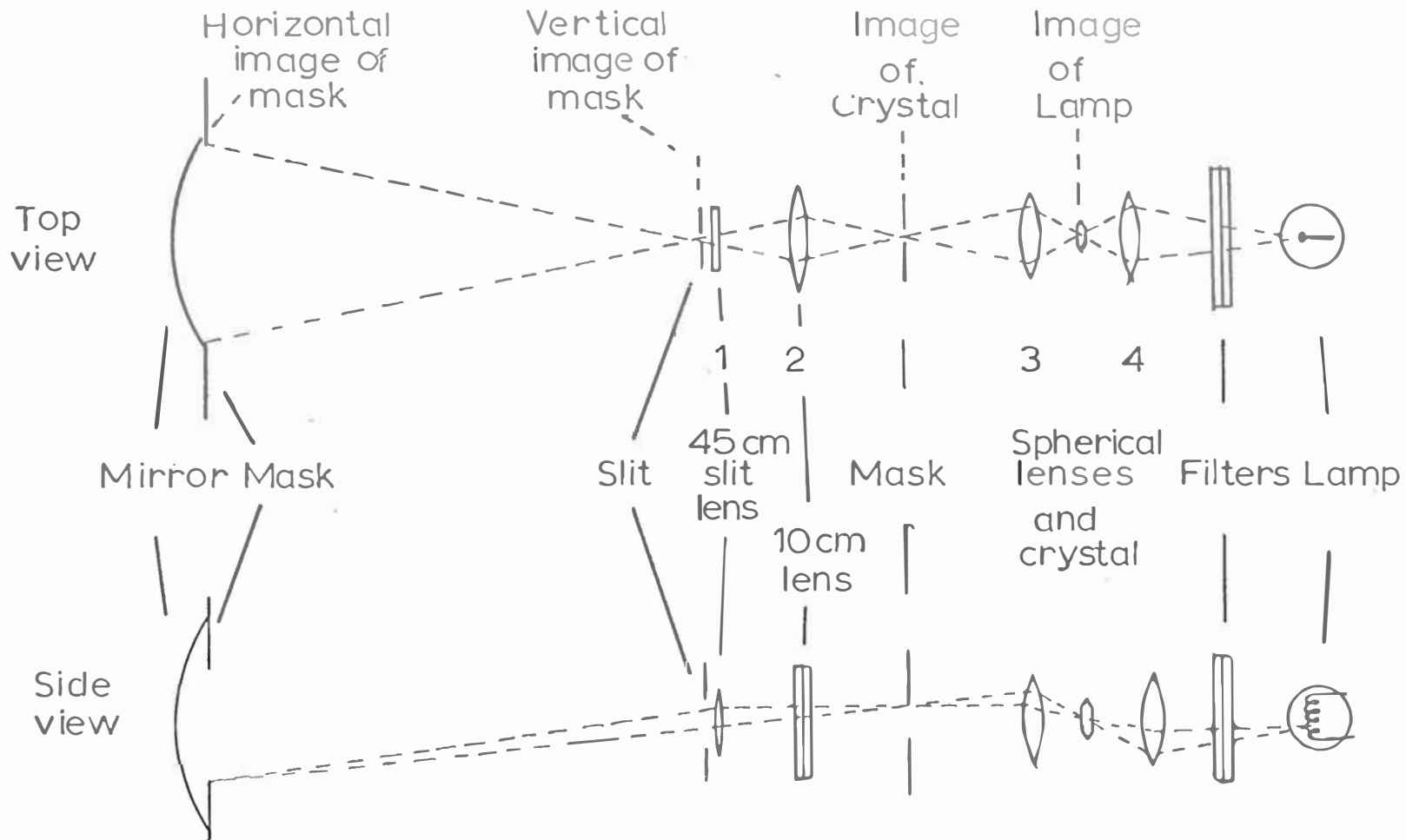


Figure 3-10 The Jarrell-Ash Condenser System

Figure 3-11 A Schematic Jarrell-Ash Chart

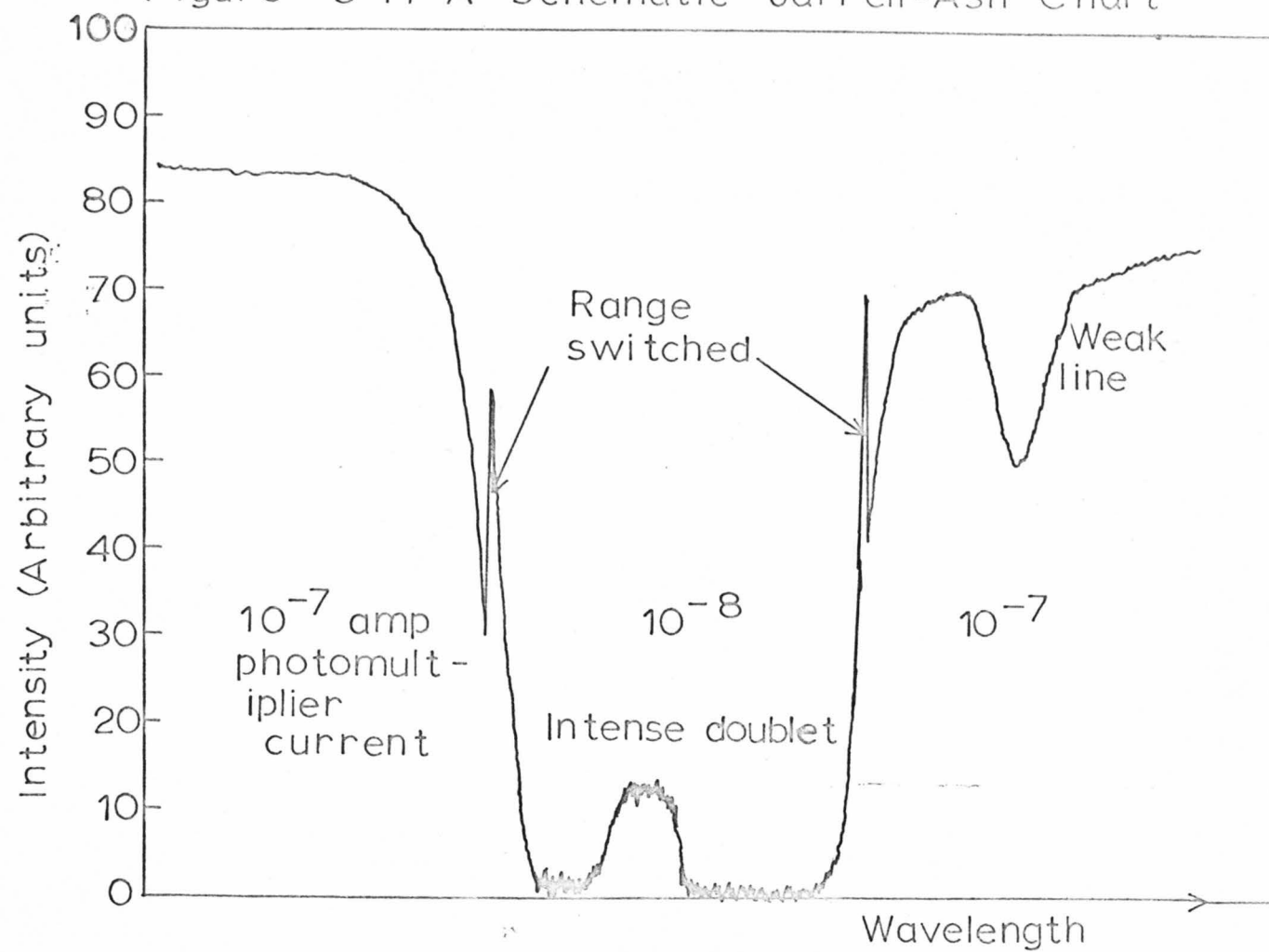
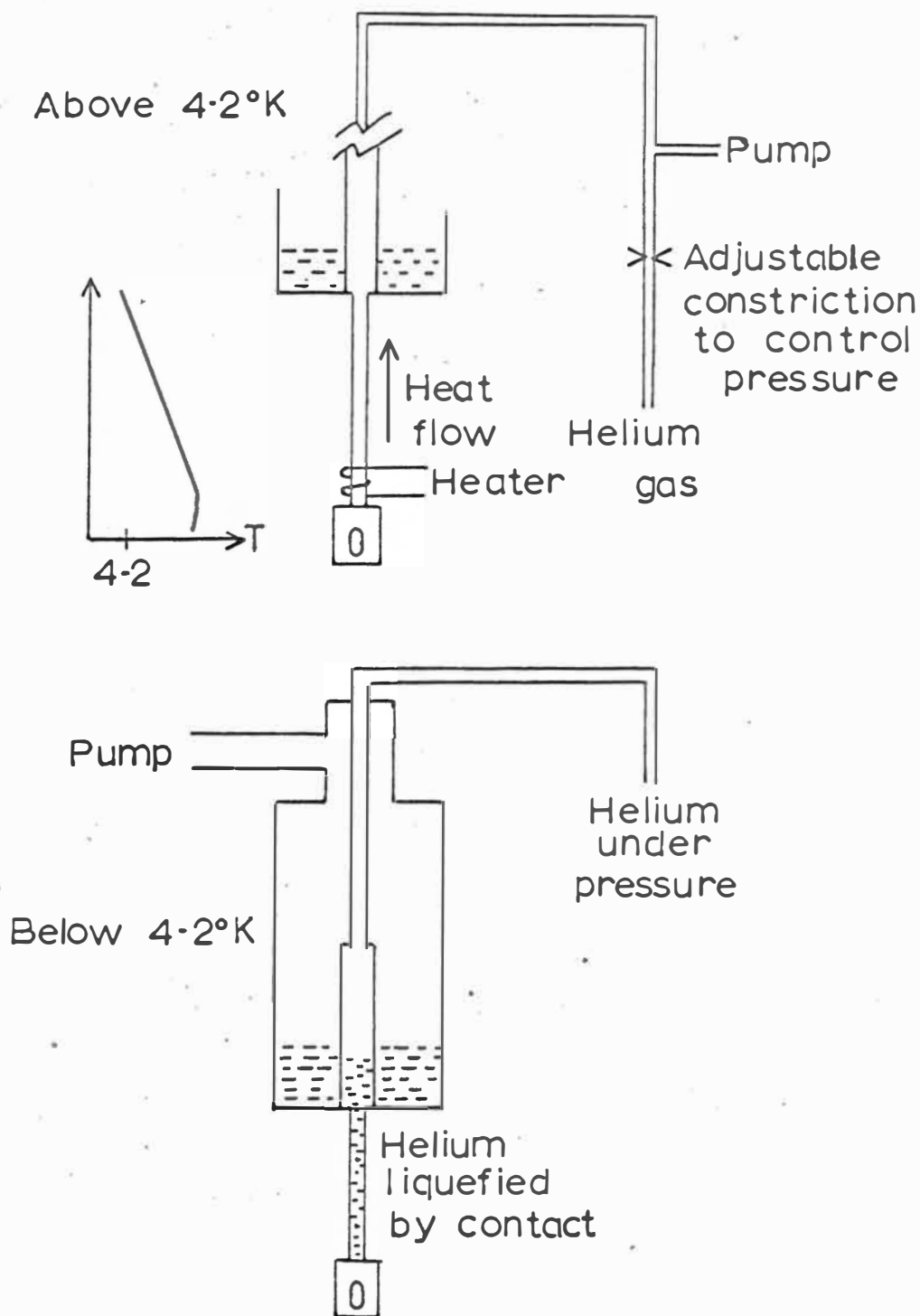


Figure 4-1 Andonian Dewar Operation



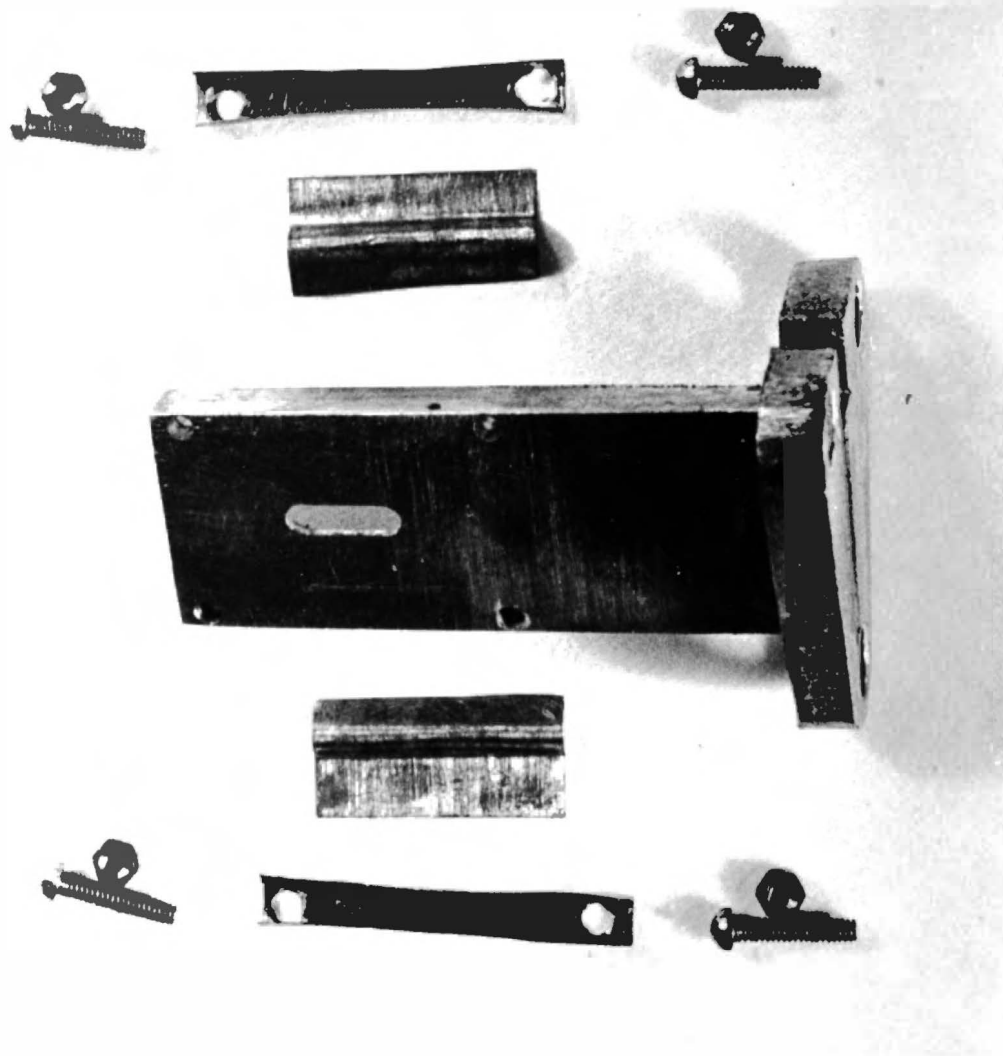


Figure 4-2
Sample holder disassembled

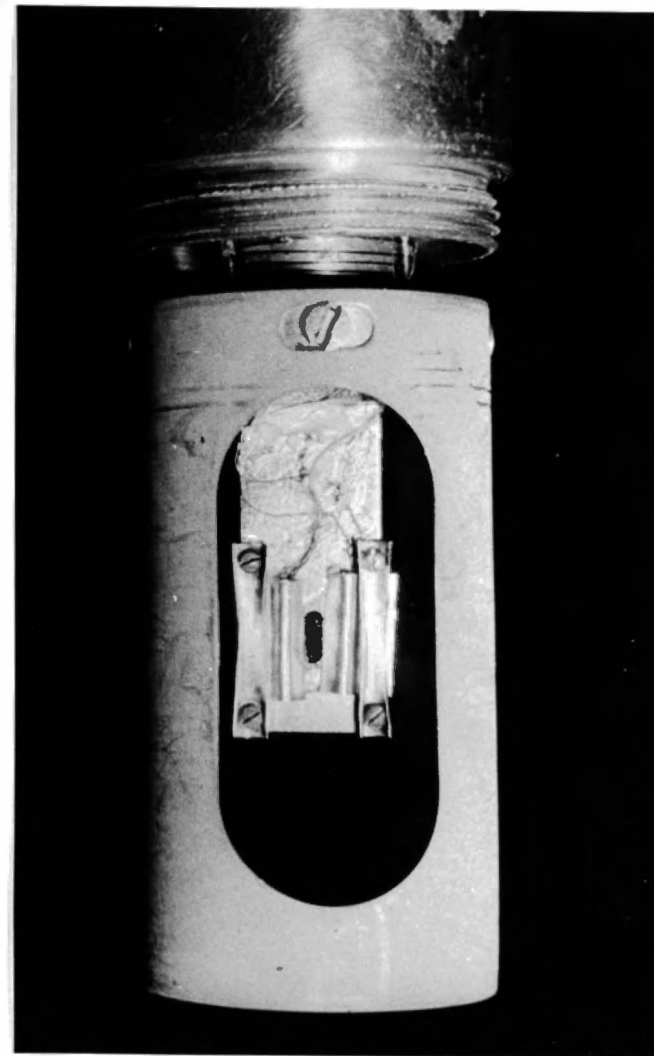
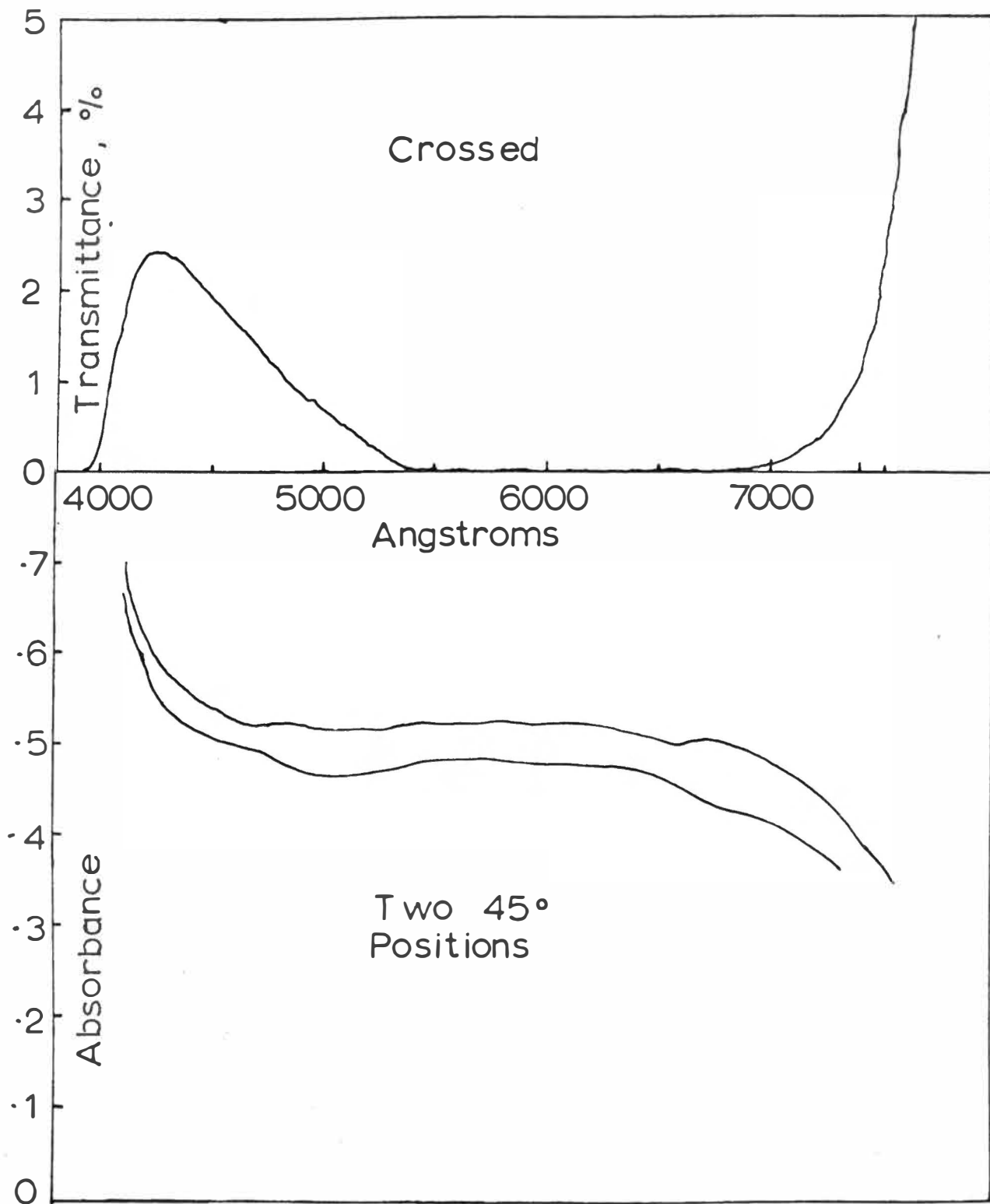


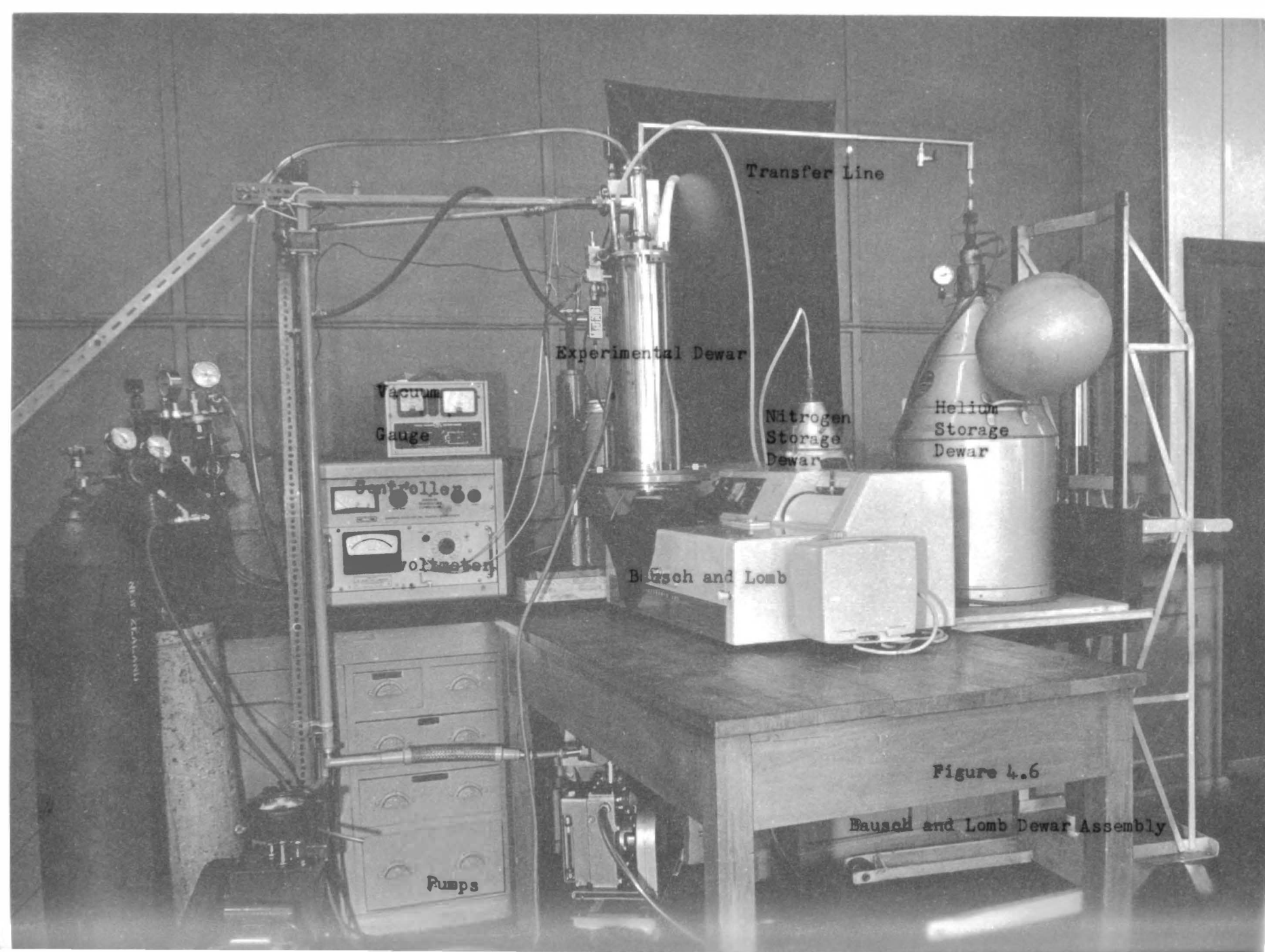
Figure 4-3
Sample holder in position

Figure 4.4
Polaroid slide for dewar



Figure 4-5 Polaroid Spectrum





Transfer Line

Experimental Dewar

Vacuum
Gauge

Nitrogen
Storage
Dewar

Helium
Storage
Dewar

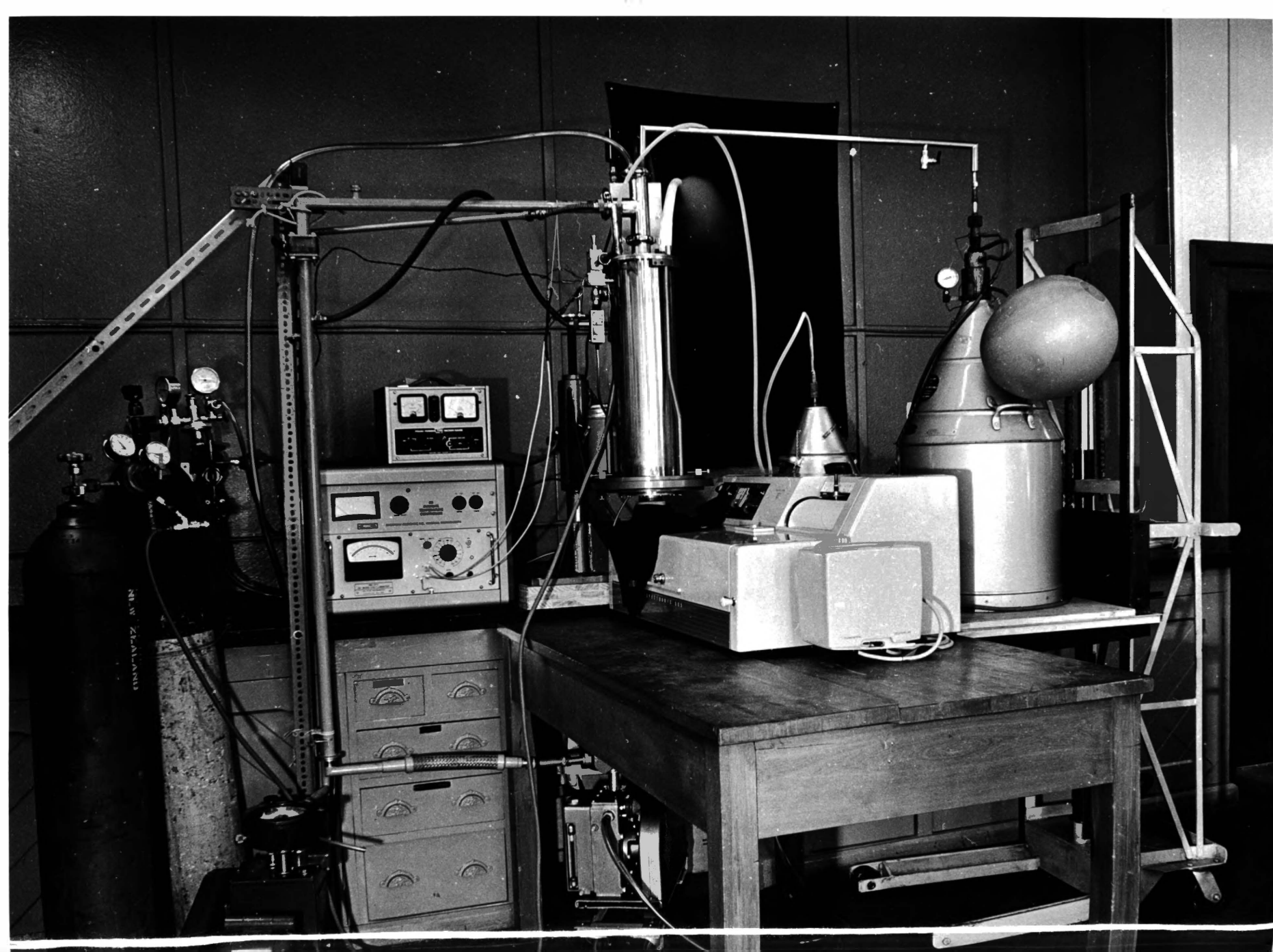
Controller
Voltmeter

Bausch and Lomb

Figure 4.6

Bausch and Lomb Dewar Assembly

Pumps



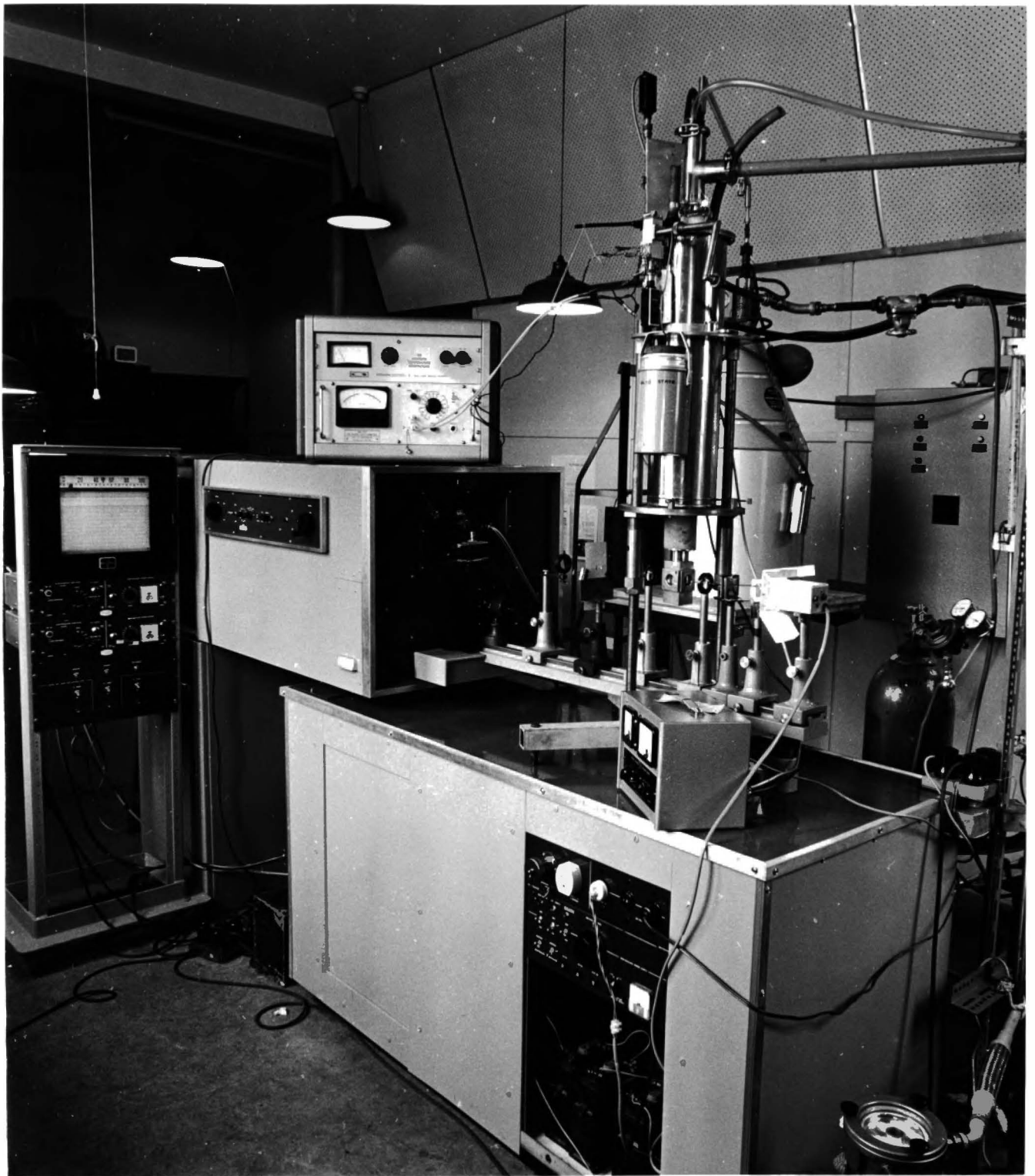


Figure 4-7 Jarrell-Ash Assembly

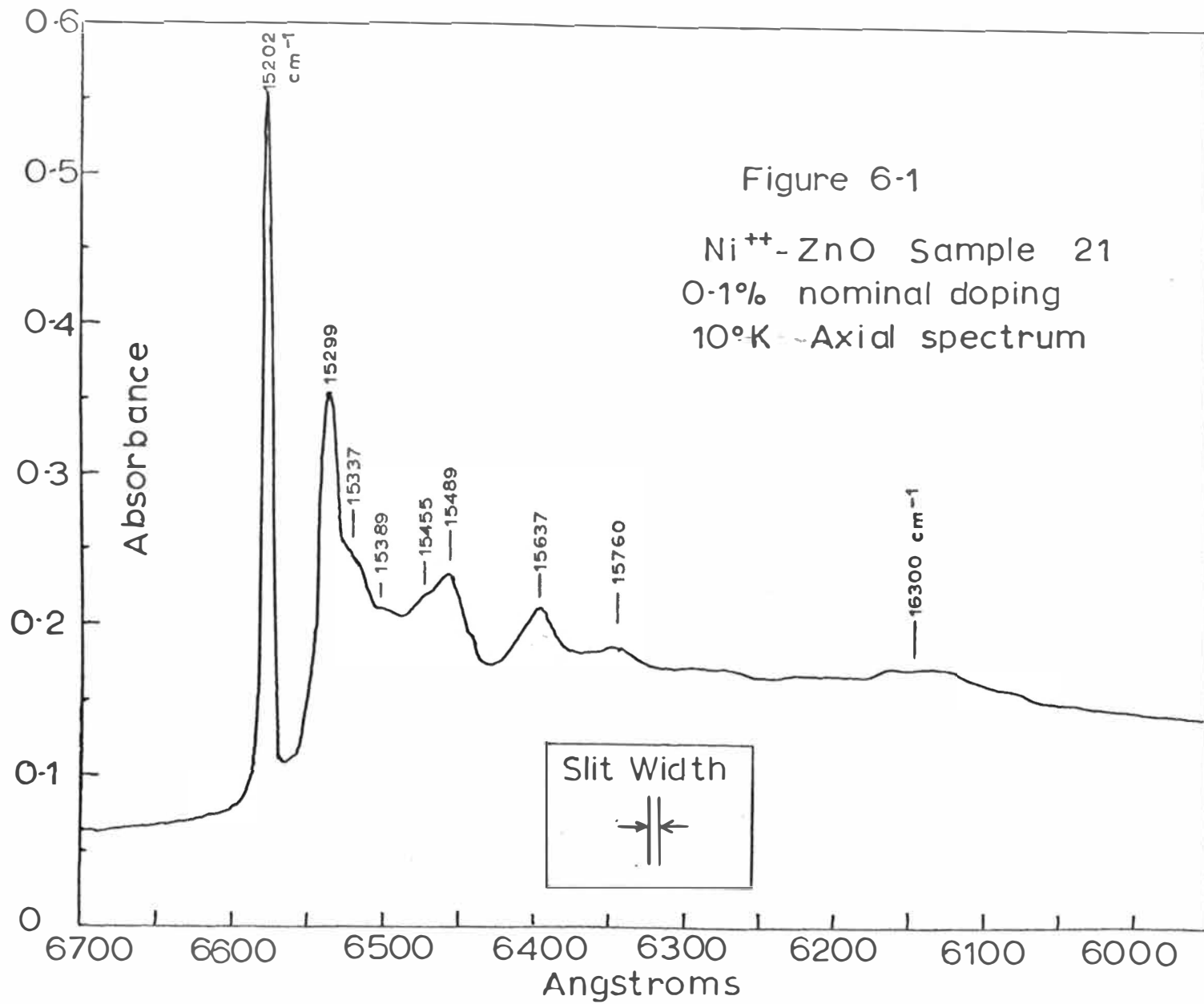
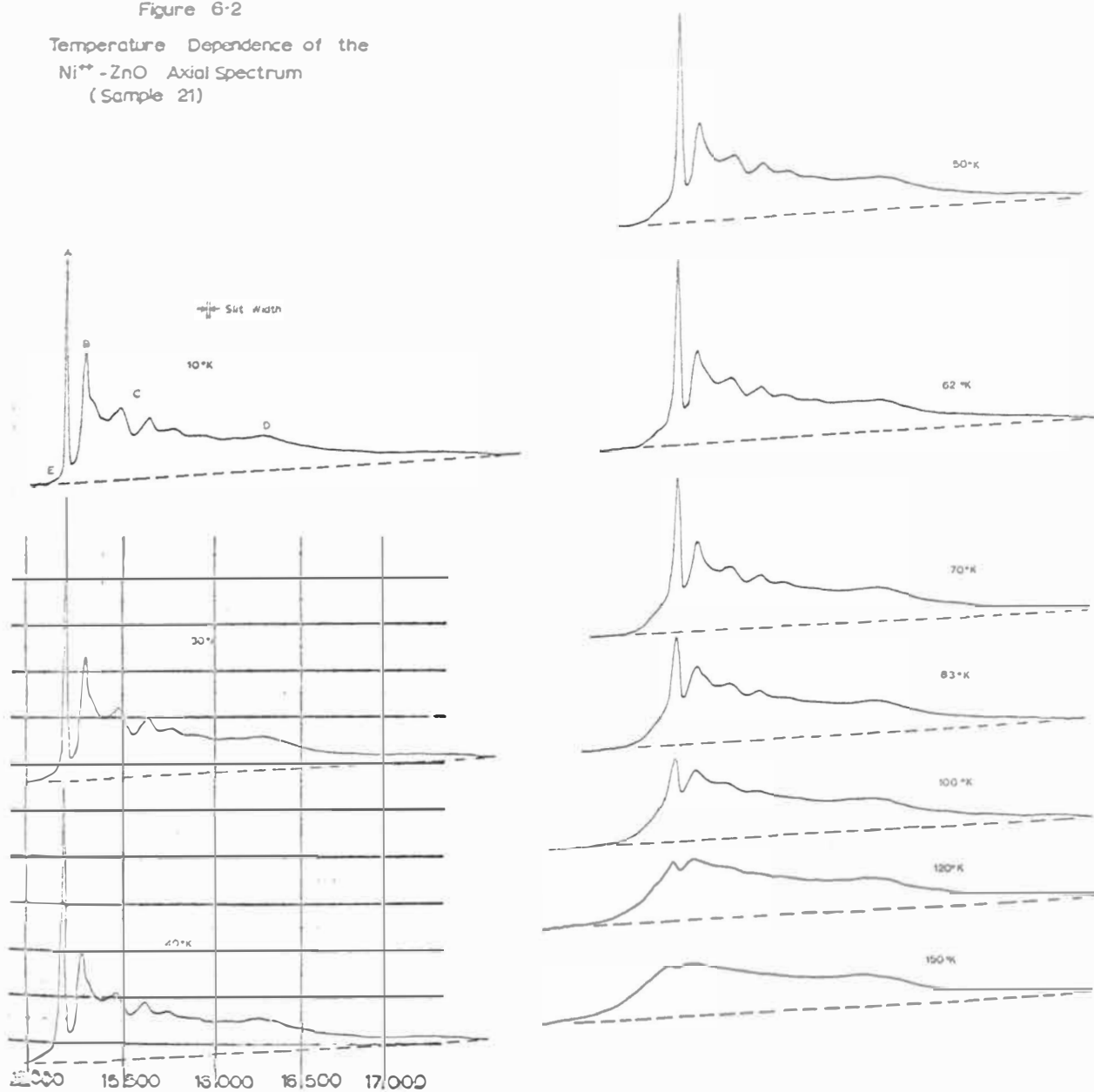
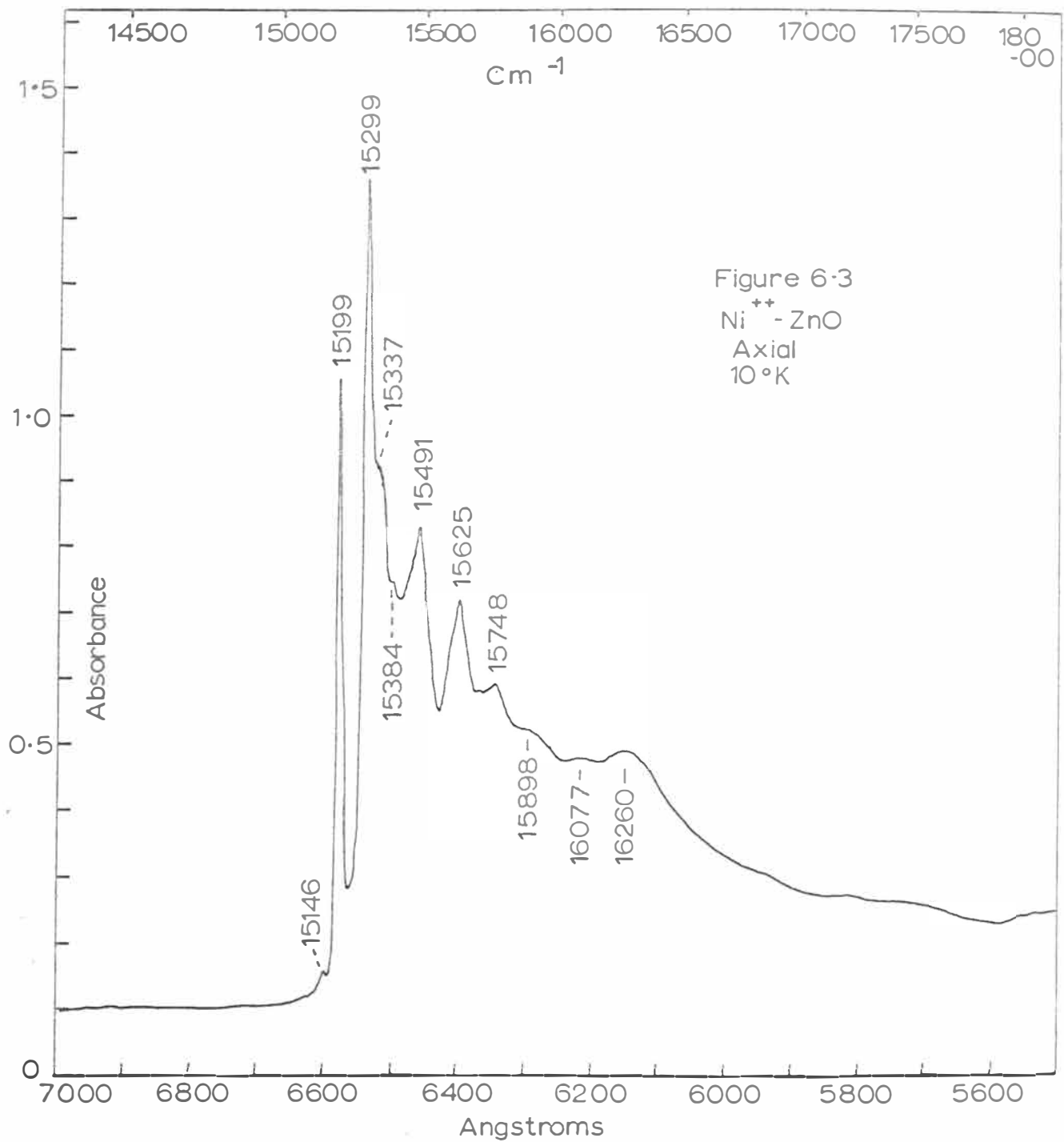


Figure 6-2

Temperature Dependence of the
Ni²⁺ - ZnO Axial Spectrum
(Sample 21)





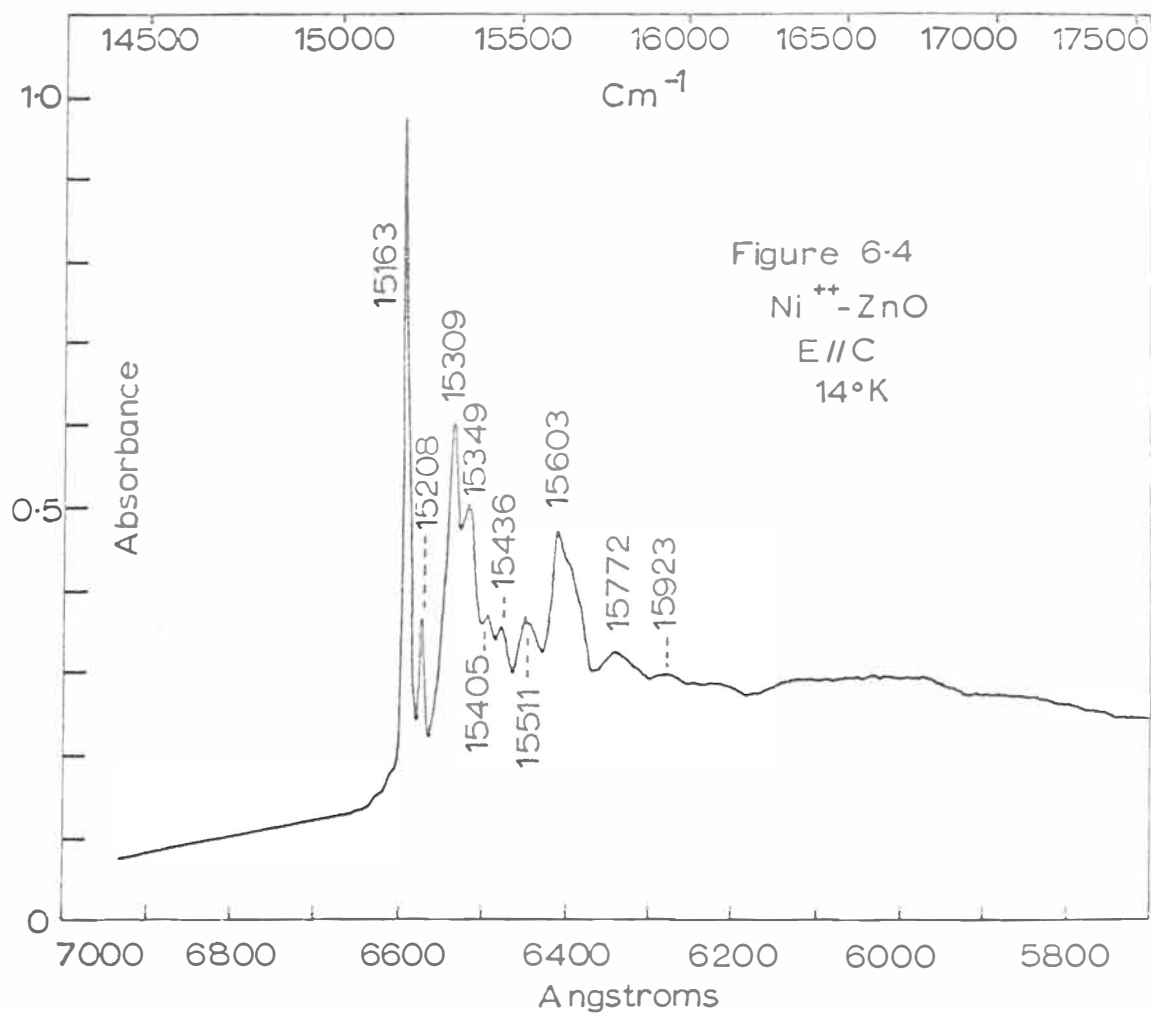


Figure 6-5

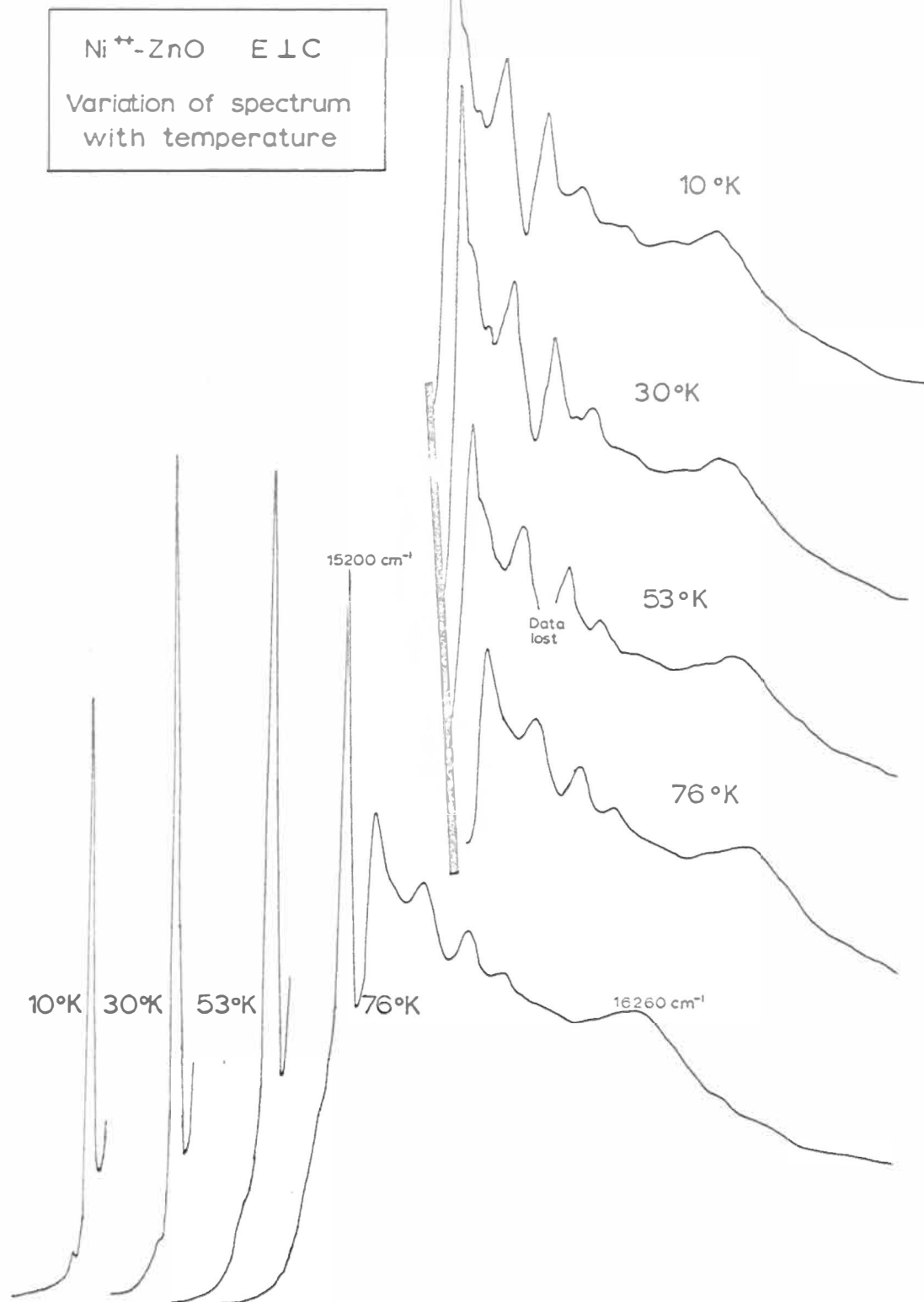
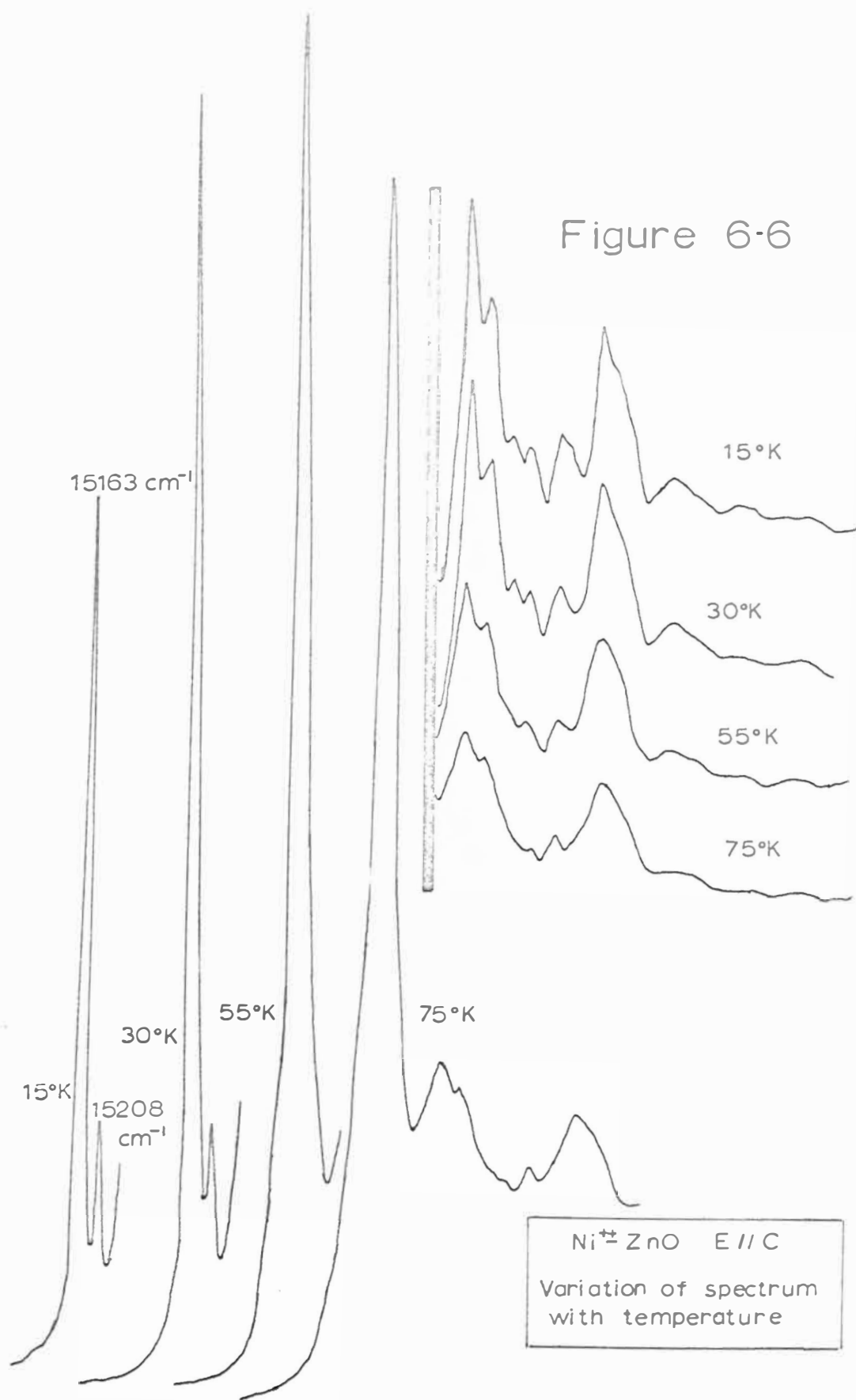


Figure 6-6



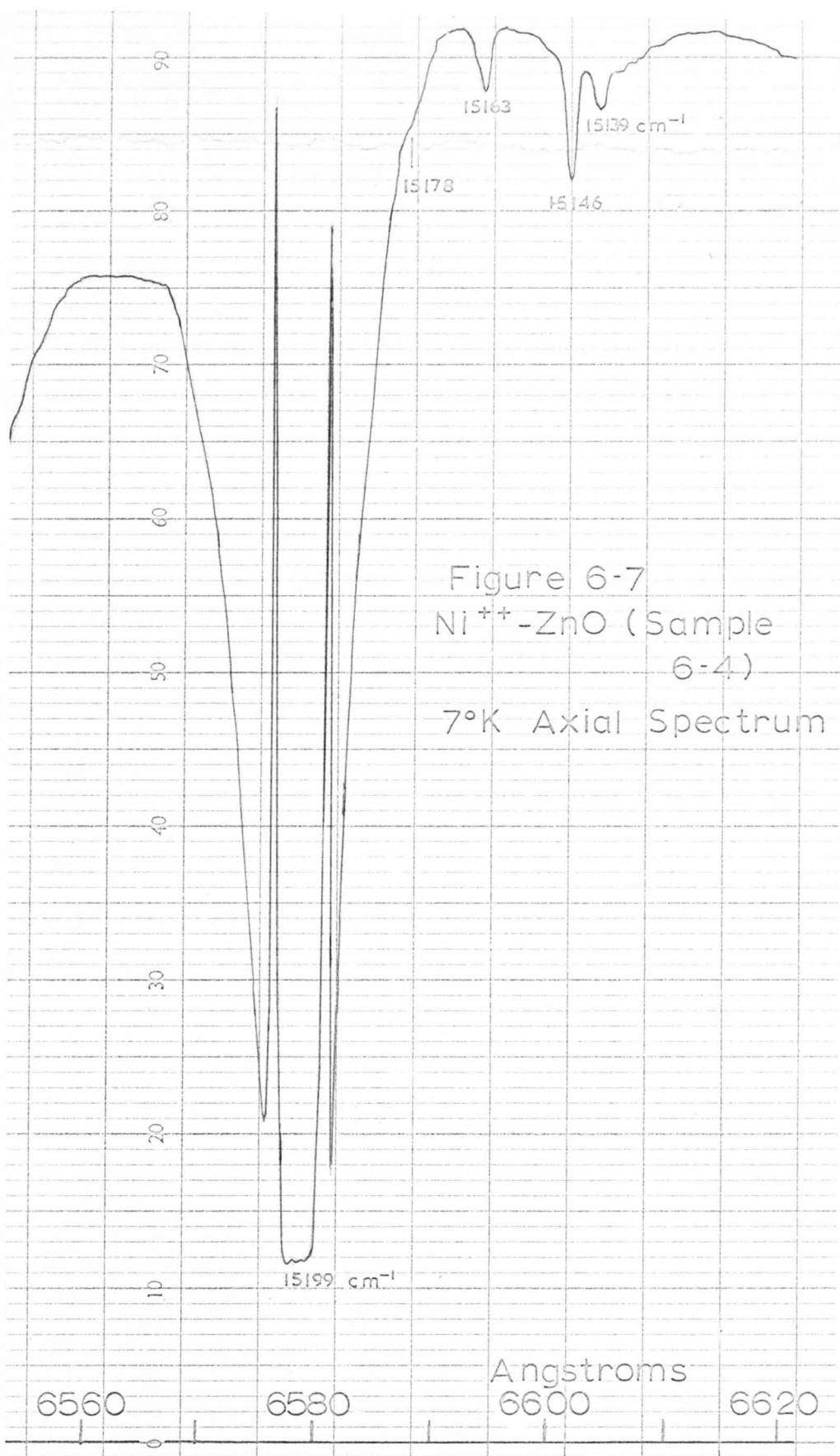
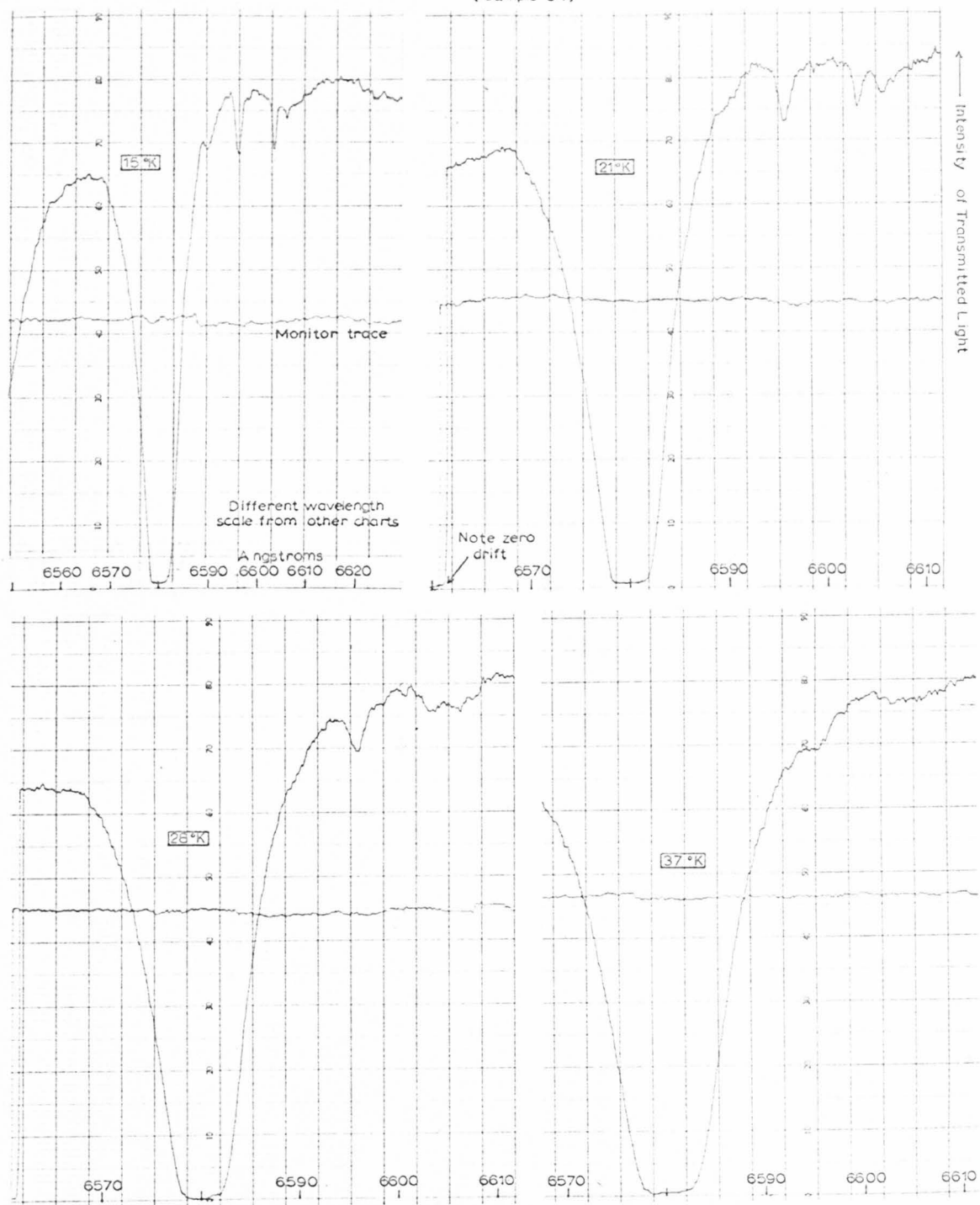


Figure 6-8 $\text{Ni}^{++}\text{-ZnO}$ Axial Spectrum (Jarrell-Ash)

(Sample 6-1)



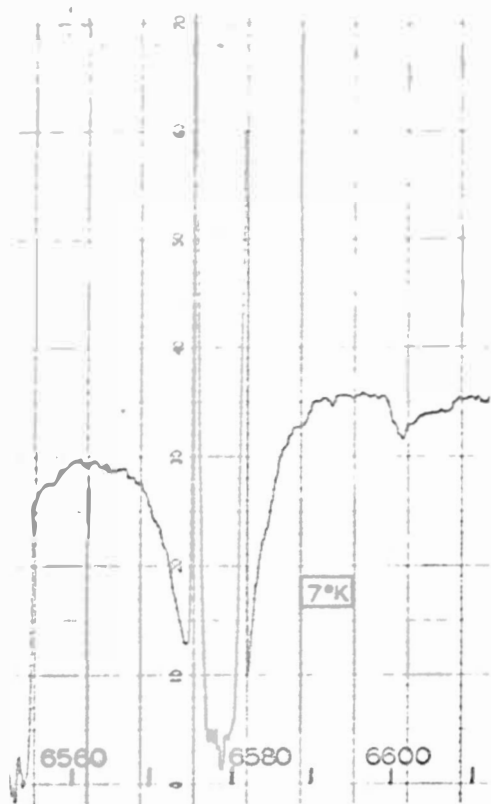


Figure 6-9 $\text{Ni}^{++}\text{-ZnO}$
J-A Sigma Spectrum

30°K trace on higher sensitivity

✚ Slit width

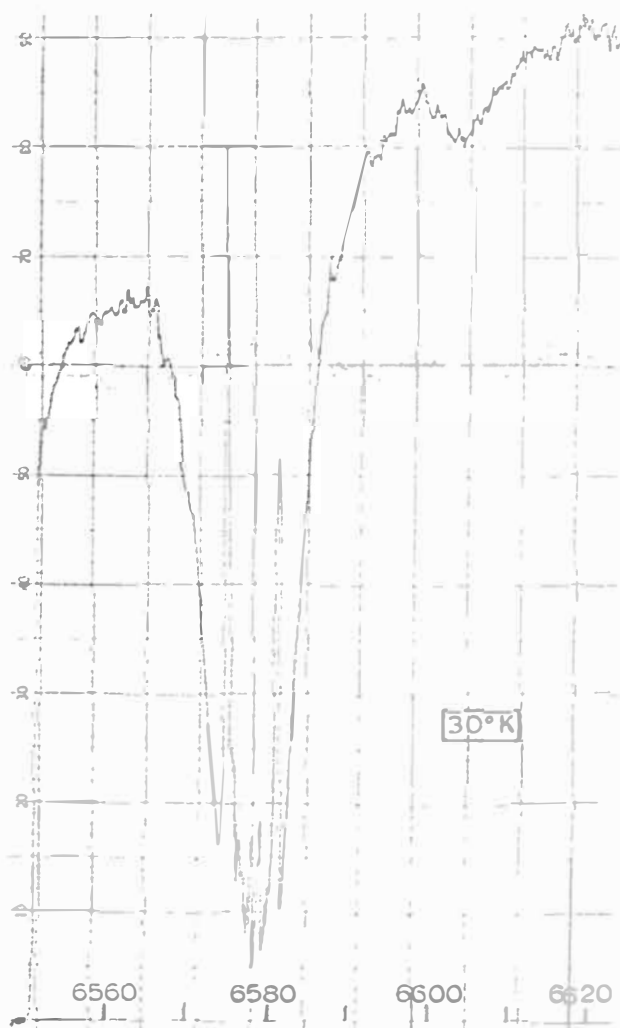
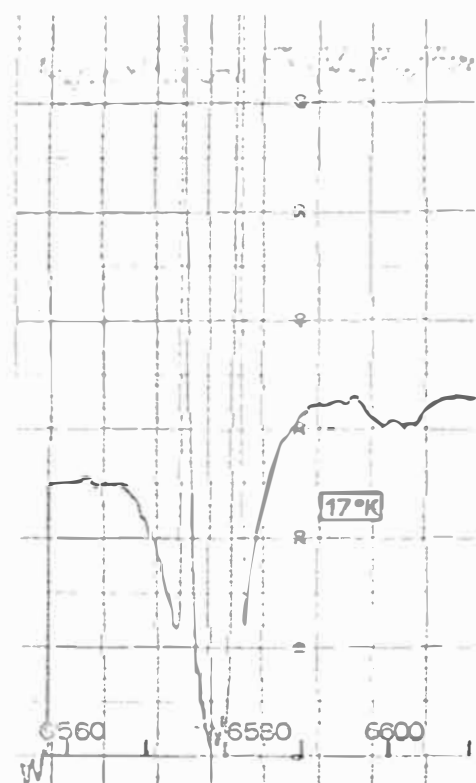


Figure 6-10 $\text{Ni}^{++}\text{-ZnO}$

J-A Pi Spectrum

9°K trace on lower sensitivity,
15207 cm^{-1} line not recorded

✚ Slit width

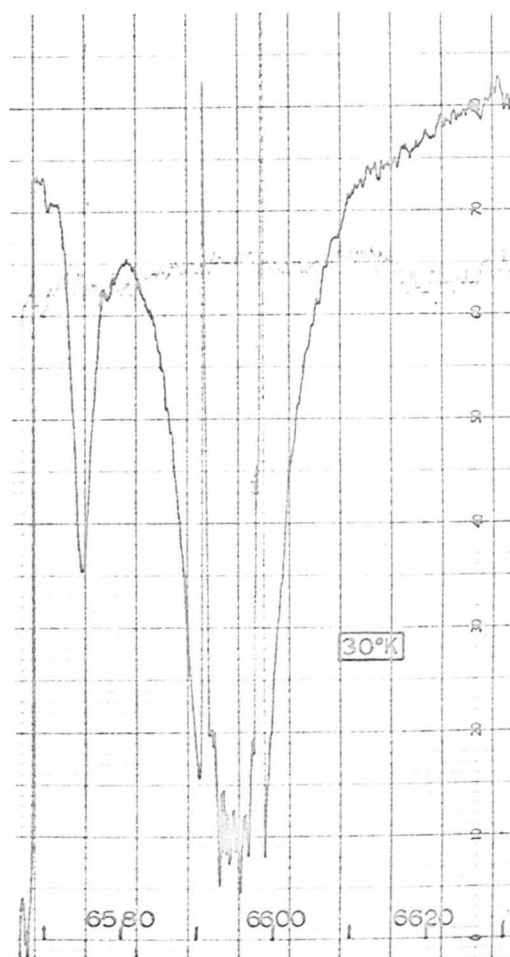
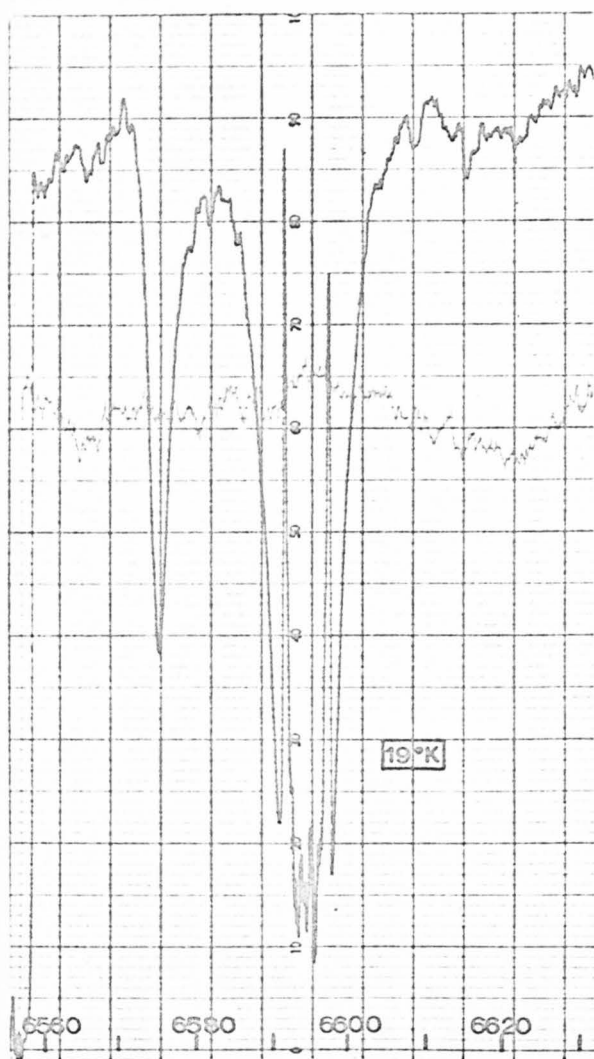
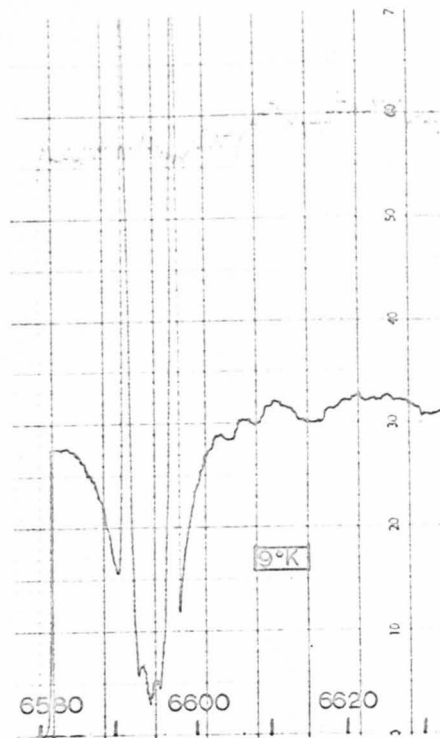


Figure 6-11 Histograms of Spectral Components
for two different Ni^{++} Dopings

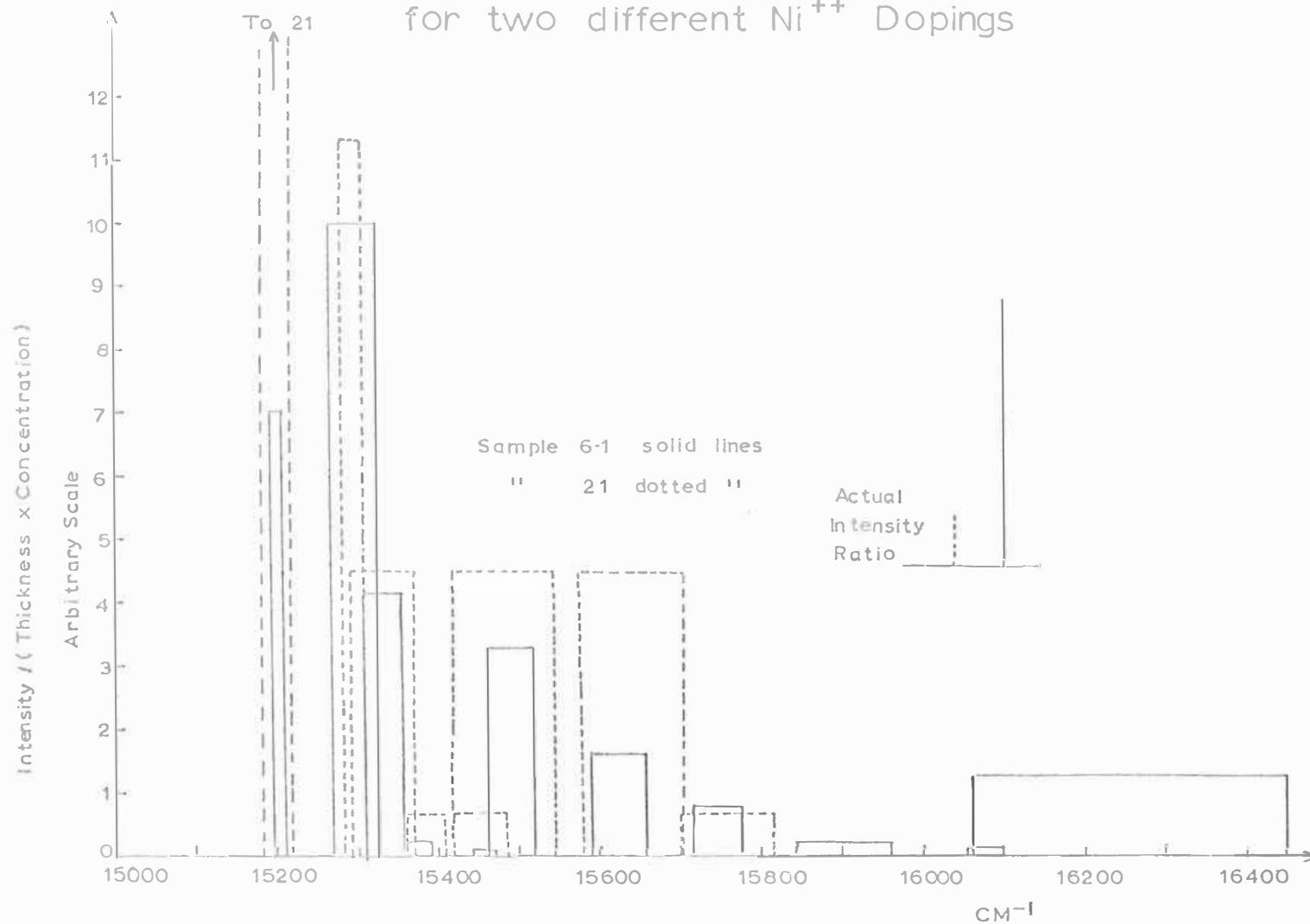


Figure 6-12 Concentration Dependence of
Weak Lines (Jarrell-Ash)

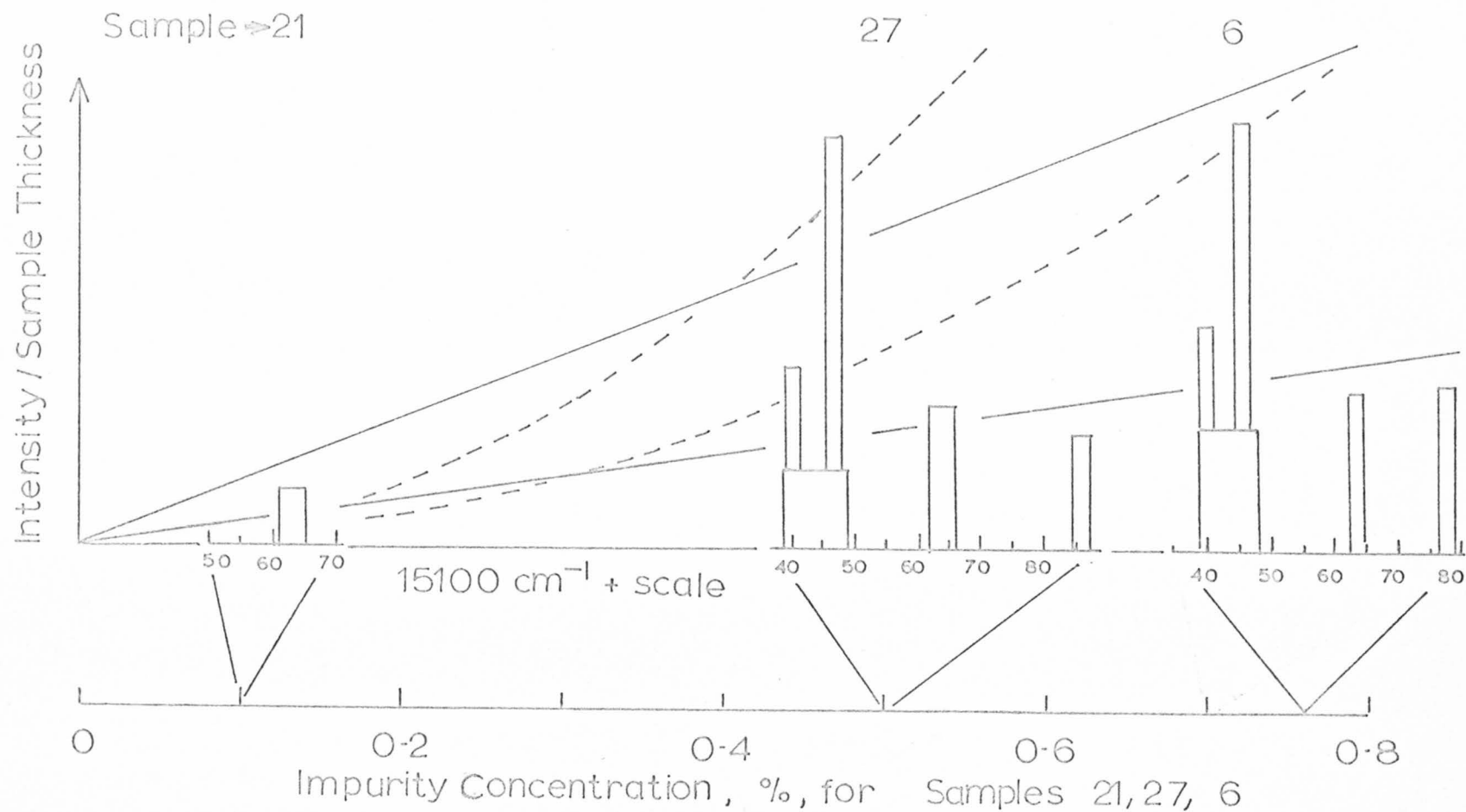


Figure 6-13 Sharp Line Temperature Dependence (J-A)

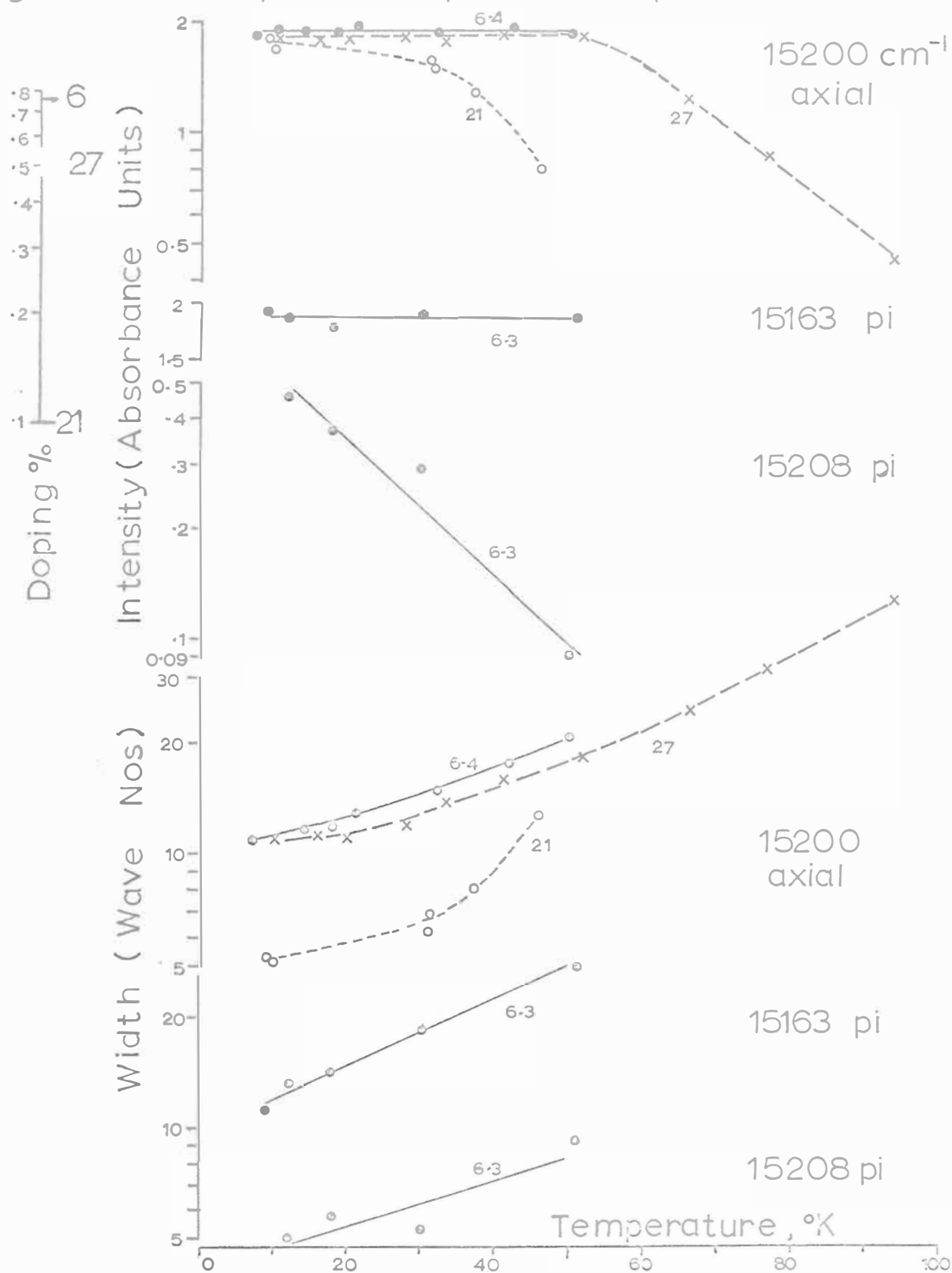


Figure 6-14 Temperature Dependence of Sharp Line Areas (J-A)

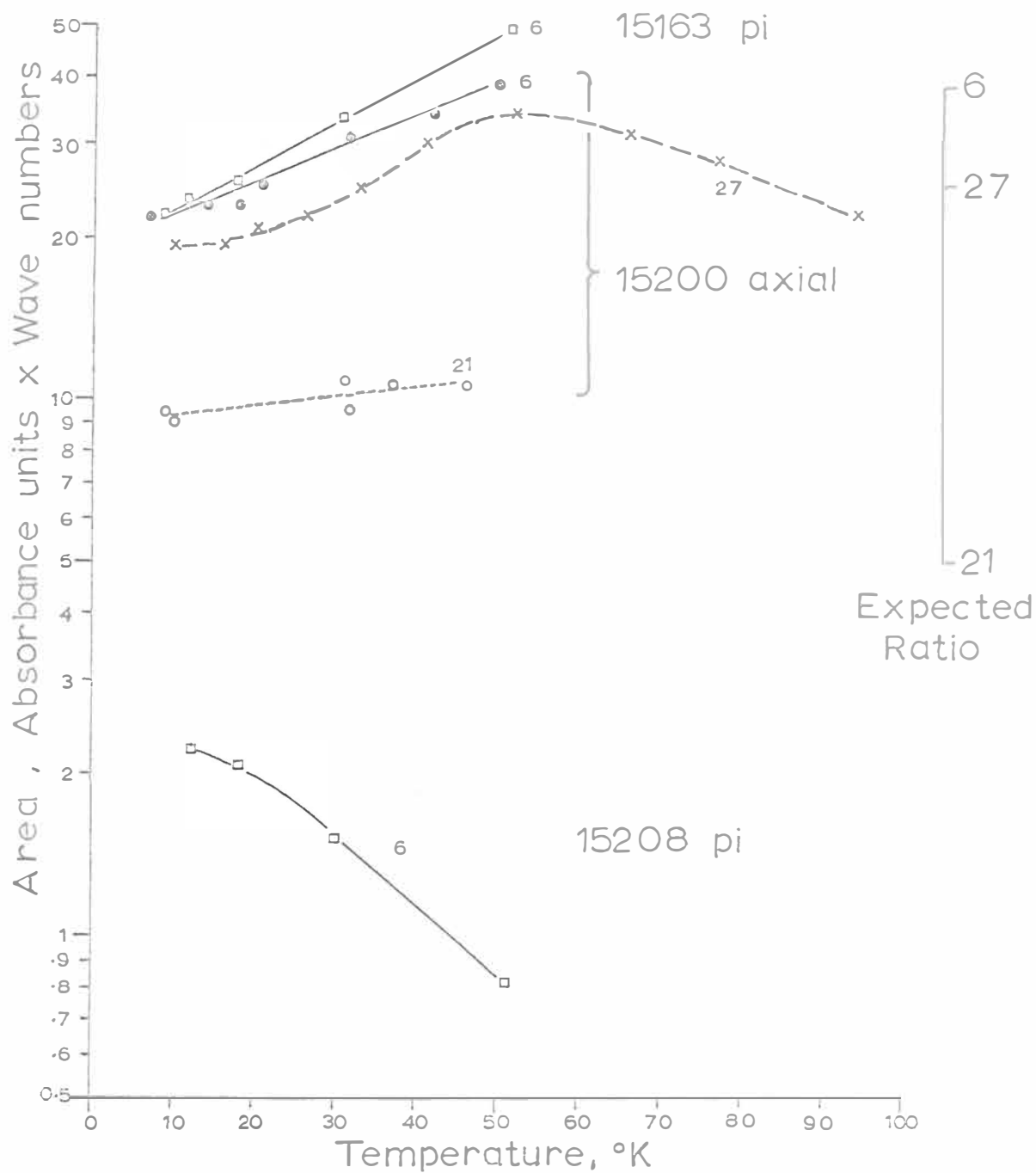


Figure 615 Total Integrated Absorption
of Ni^{++} -ZnO Visible Band

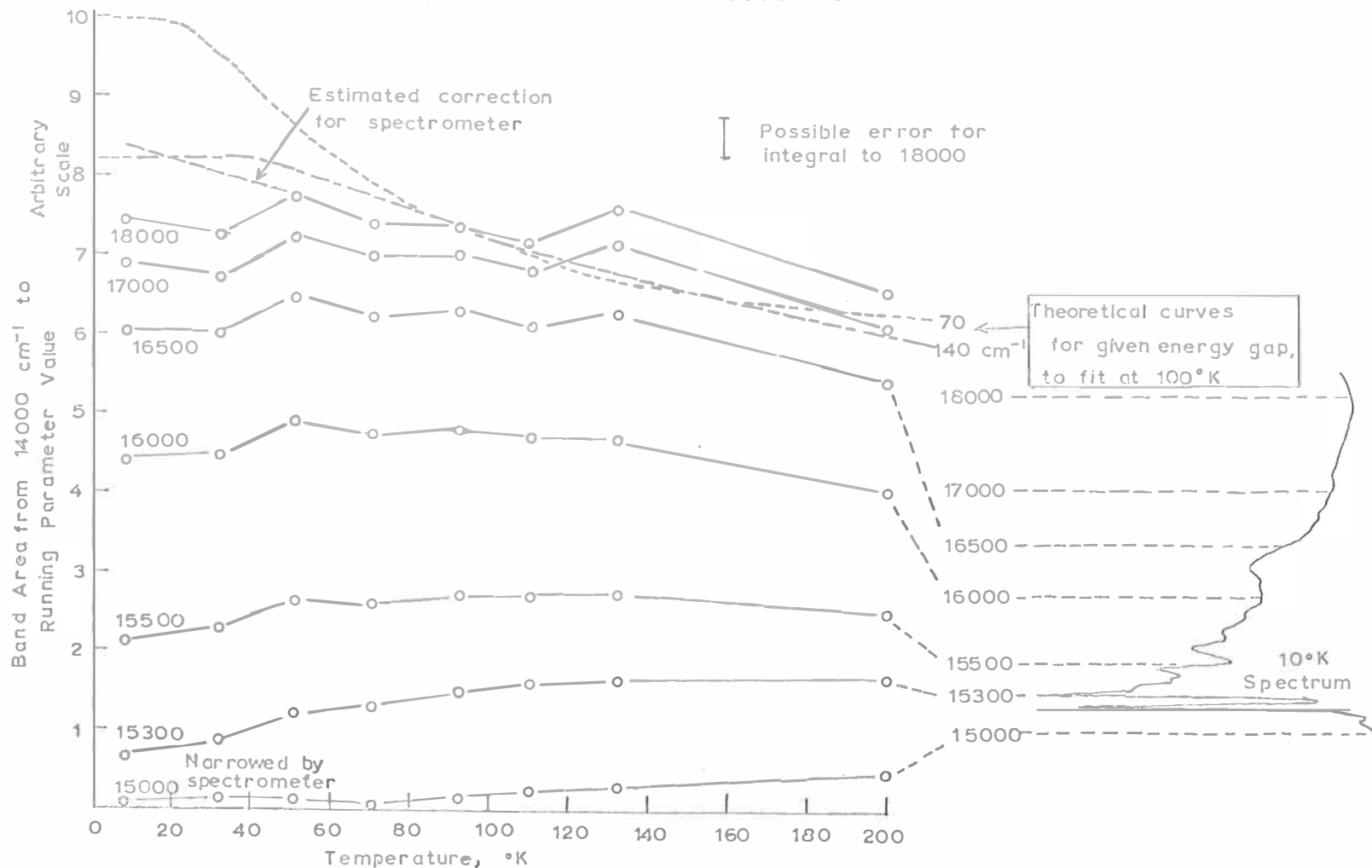


Figure 6-16 Band Shape Fitting Ni^{++} -ZnO Sigma

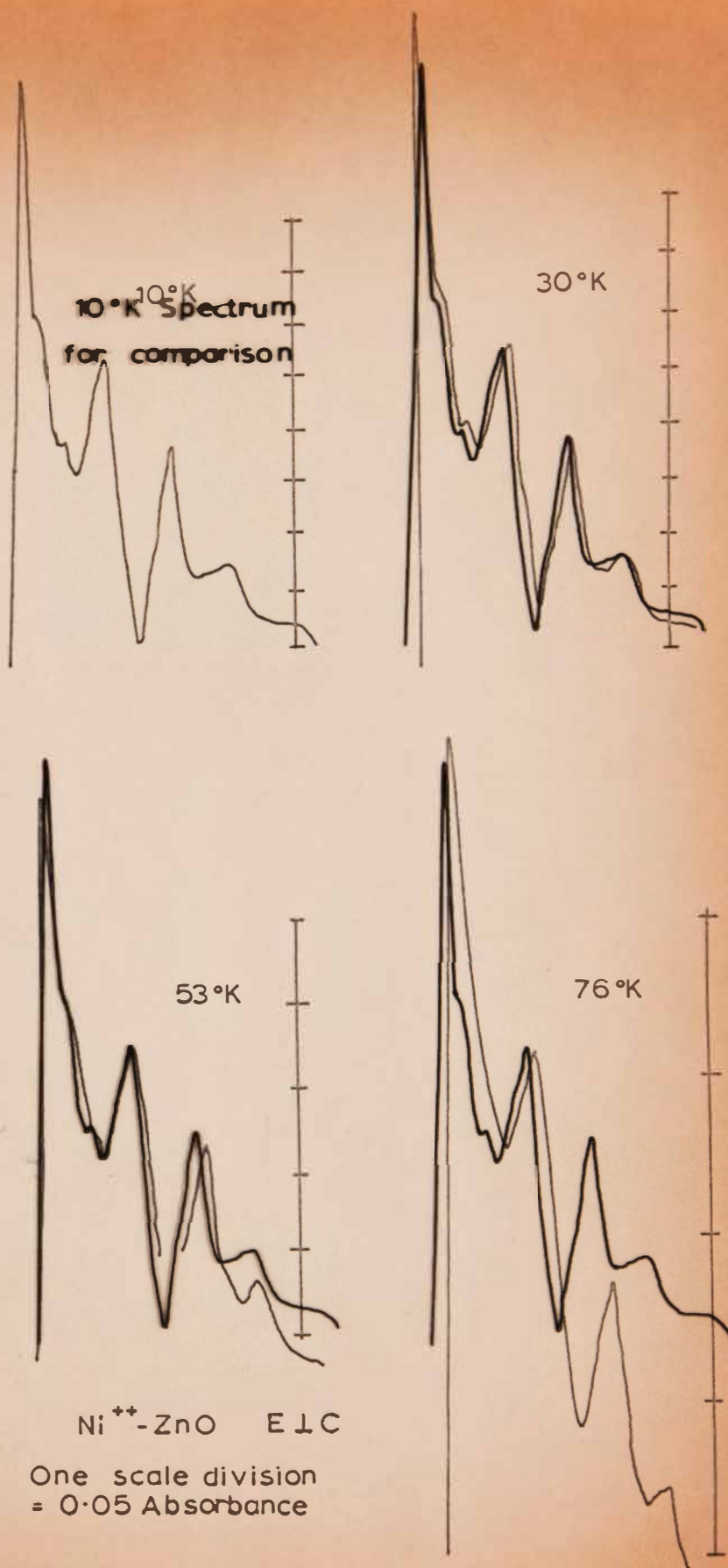
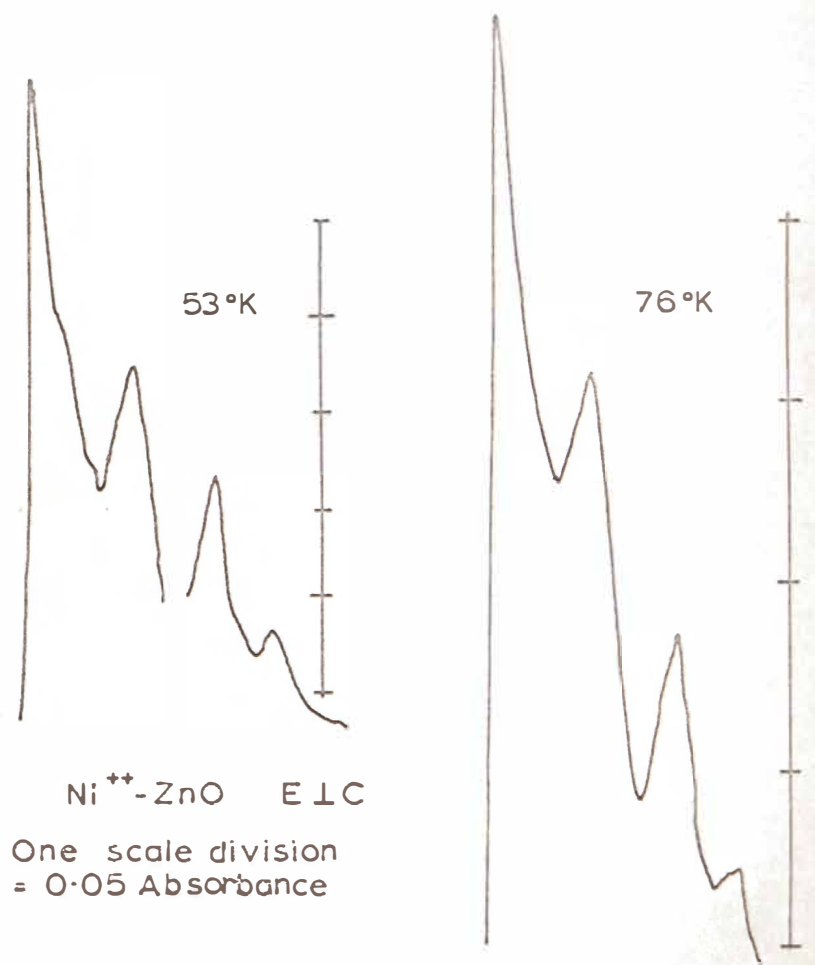
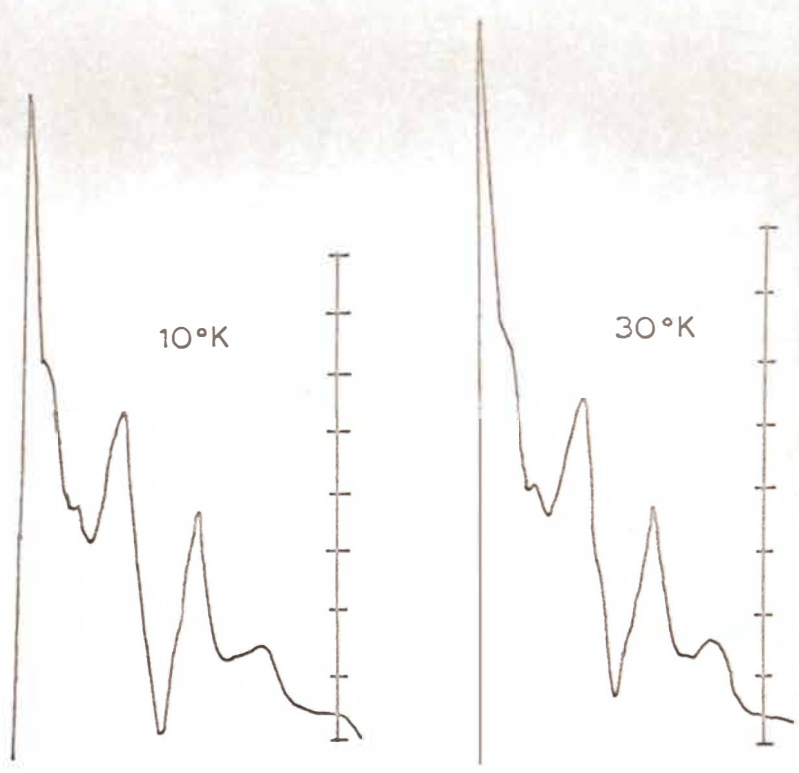
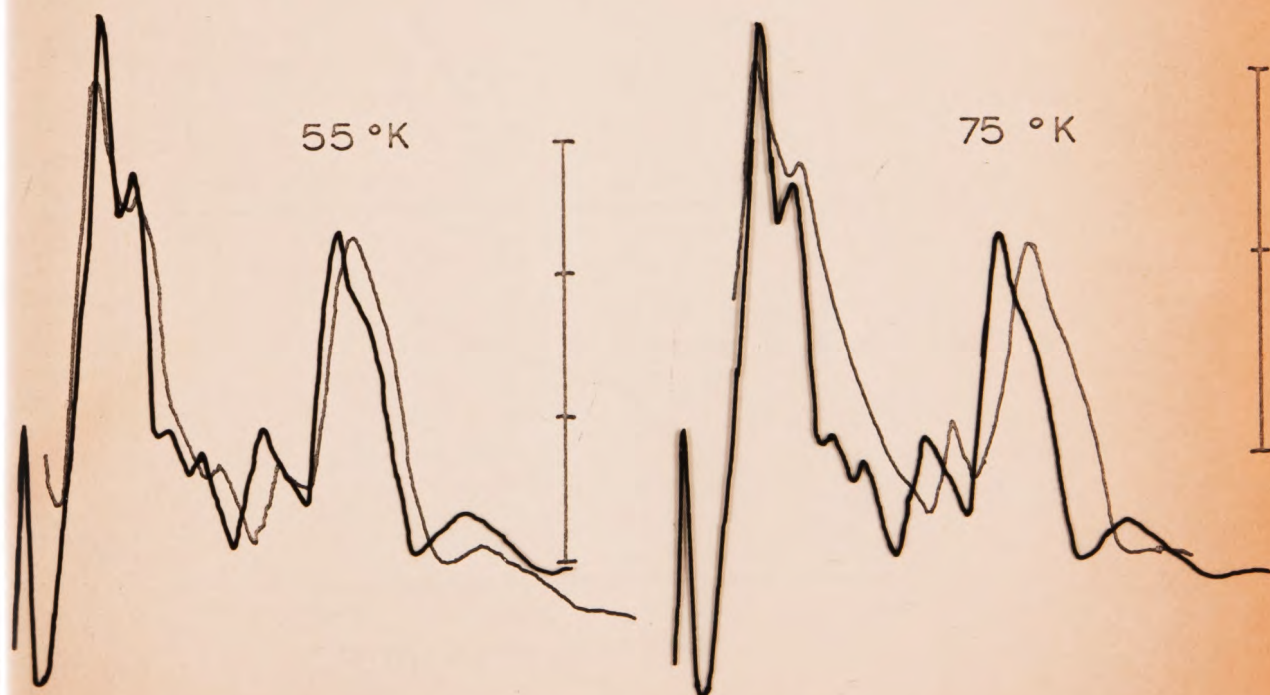
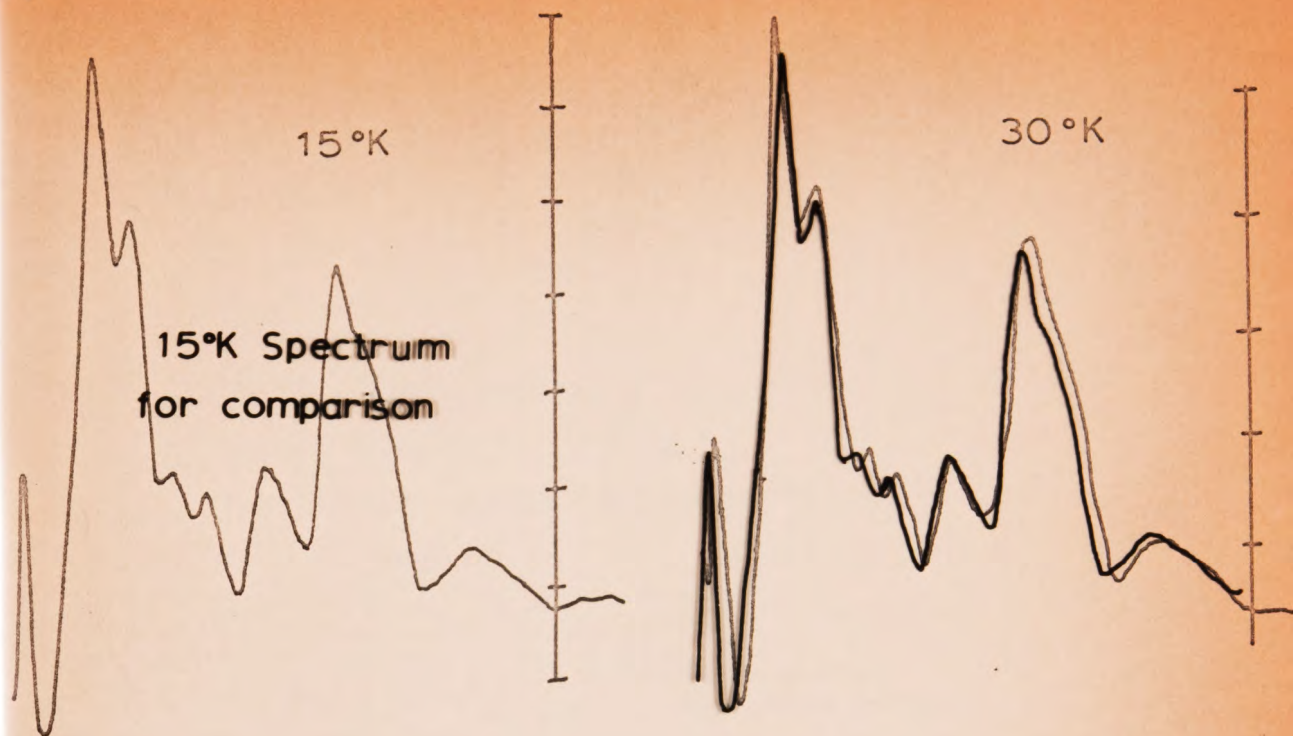


Figure 6-16 Band Shape Fitting $\text{Ni}^{++}\text{-ZnO}$ Sigma



$\text{Ni}^{++}\text{-ZnO}$ E.L.C.
 One scale division
 = 0.05 Absorbance

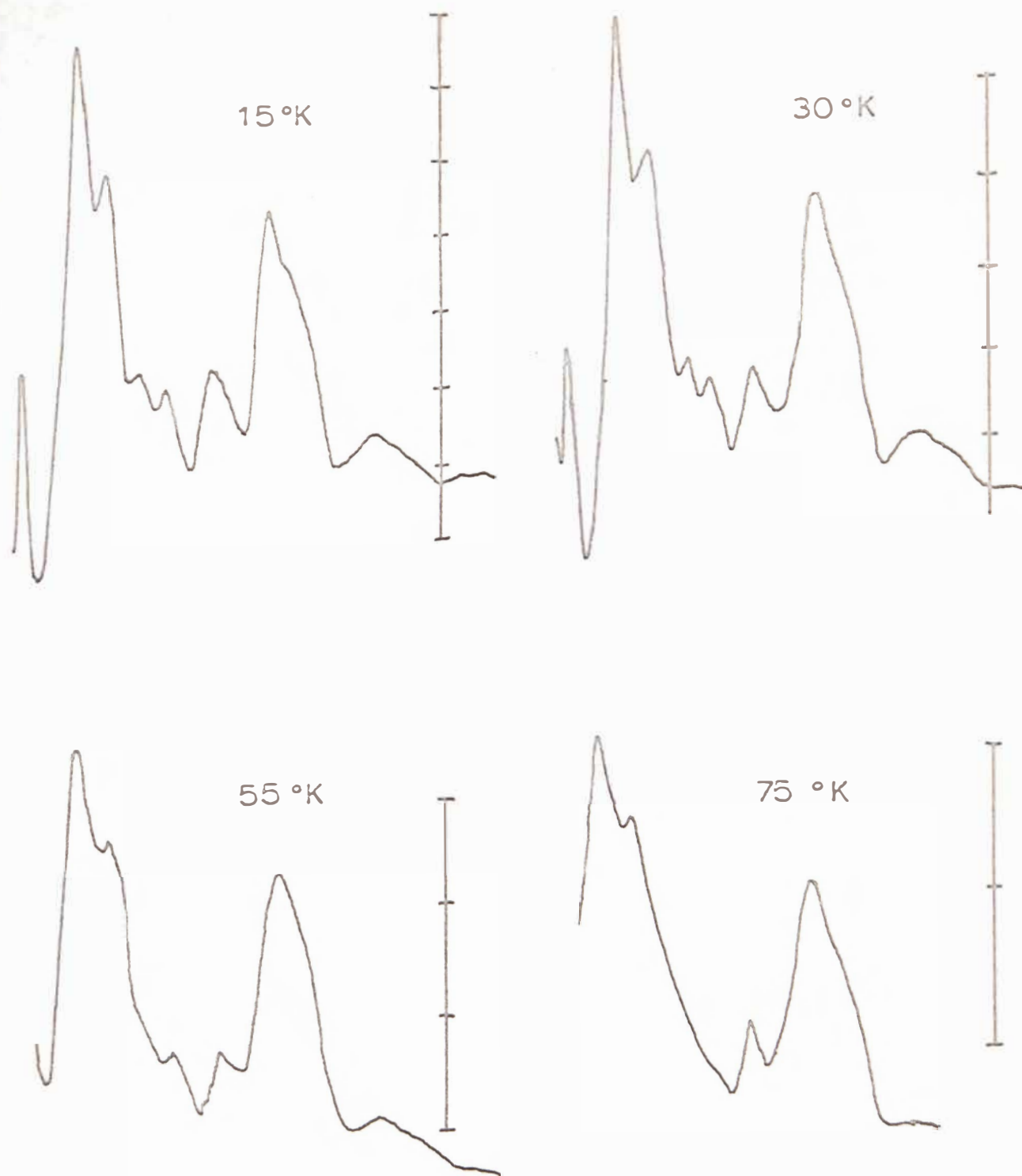
Figure 6-17 $\text{Ni}^{++}\text{-ZnO}$ Pi Band Shape Fitting



$\text{Ni}^{++}\text{-ZnO}$
E // C

One scale division
= 0.05 Absorbance

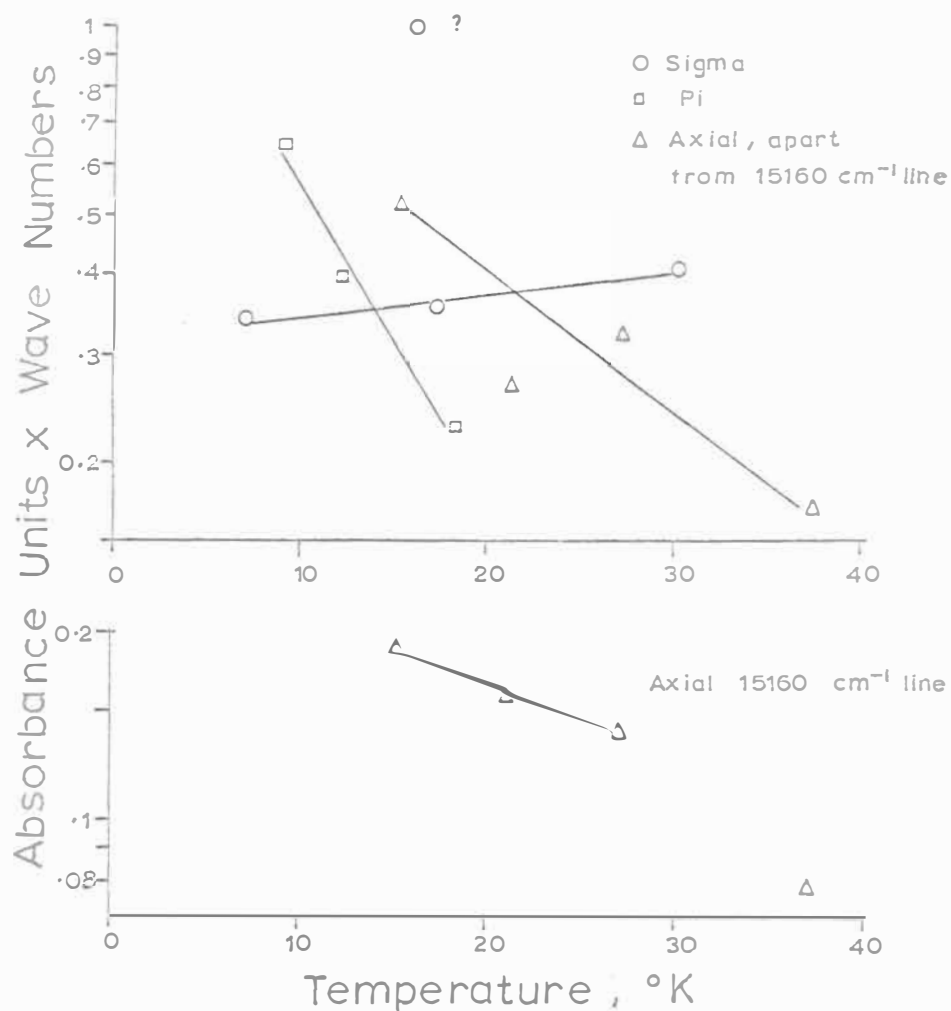
Figure 6-17 $\text{Ni}^{++}\text{-ZnO}$ Pi Band Shape Fitting



$\text{Ni}^{++}\text{-ZnO}$
E // C

One scale division
= 0.05 Absorbance

Figure 6-18 Temperature Dependence of
Weak Line Areas (J-A)
(For the whole weak structure)



d⁸ Under Decreasing Perturbations

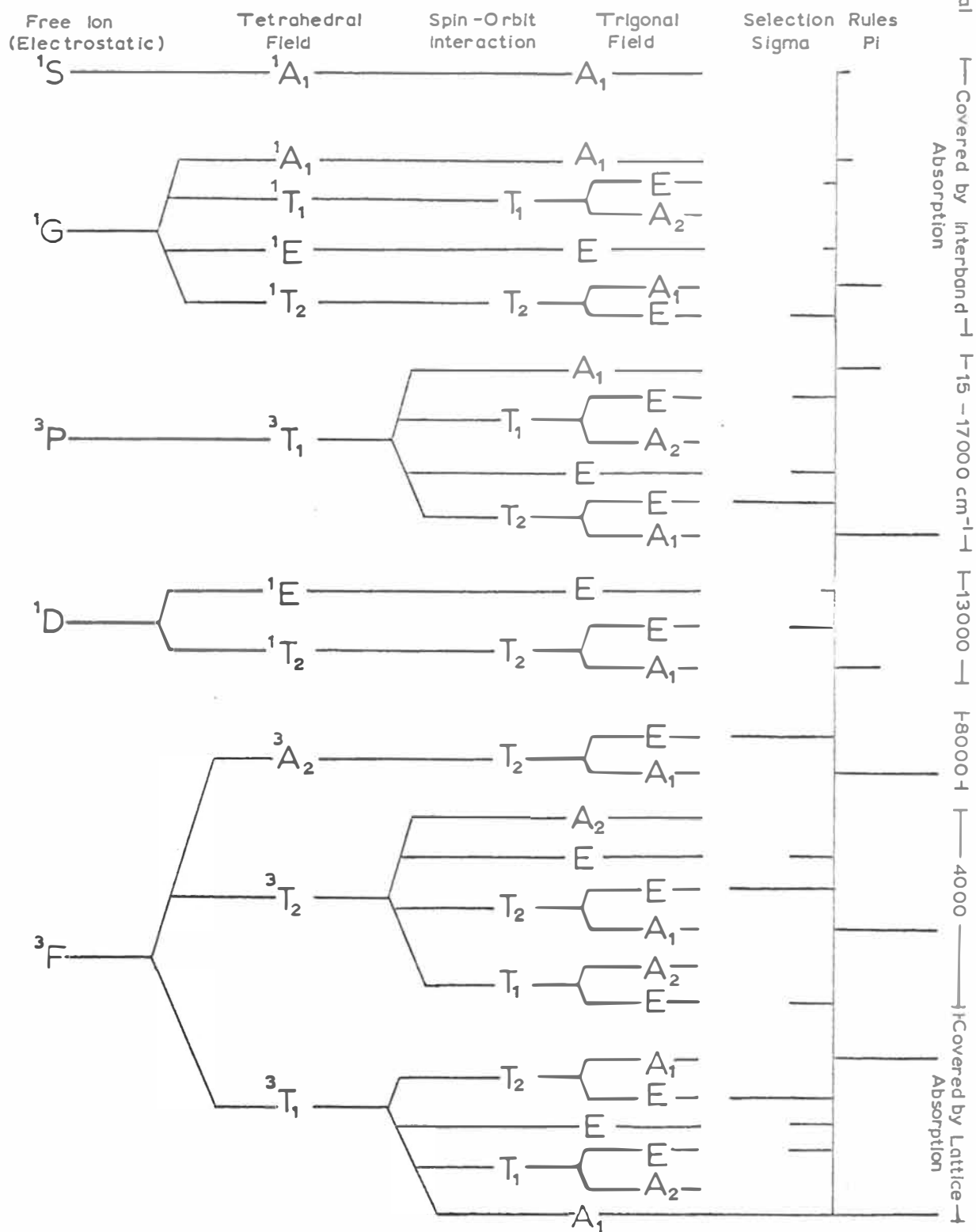


Figure 7-2 Pairs in Ni-ZnO

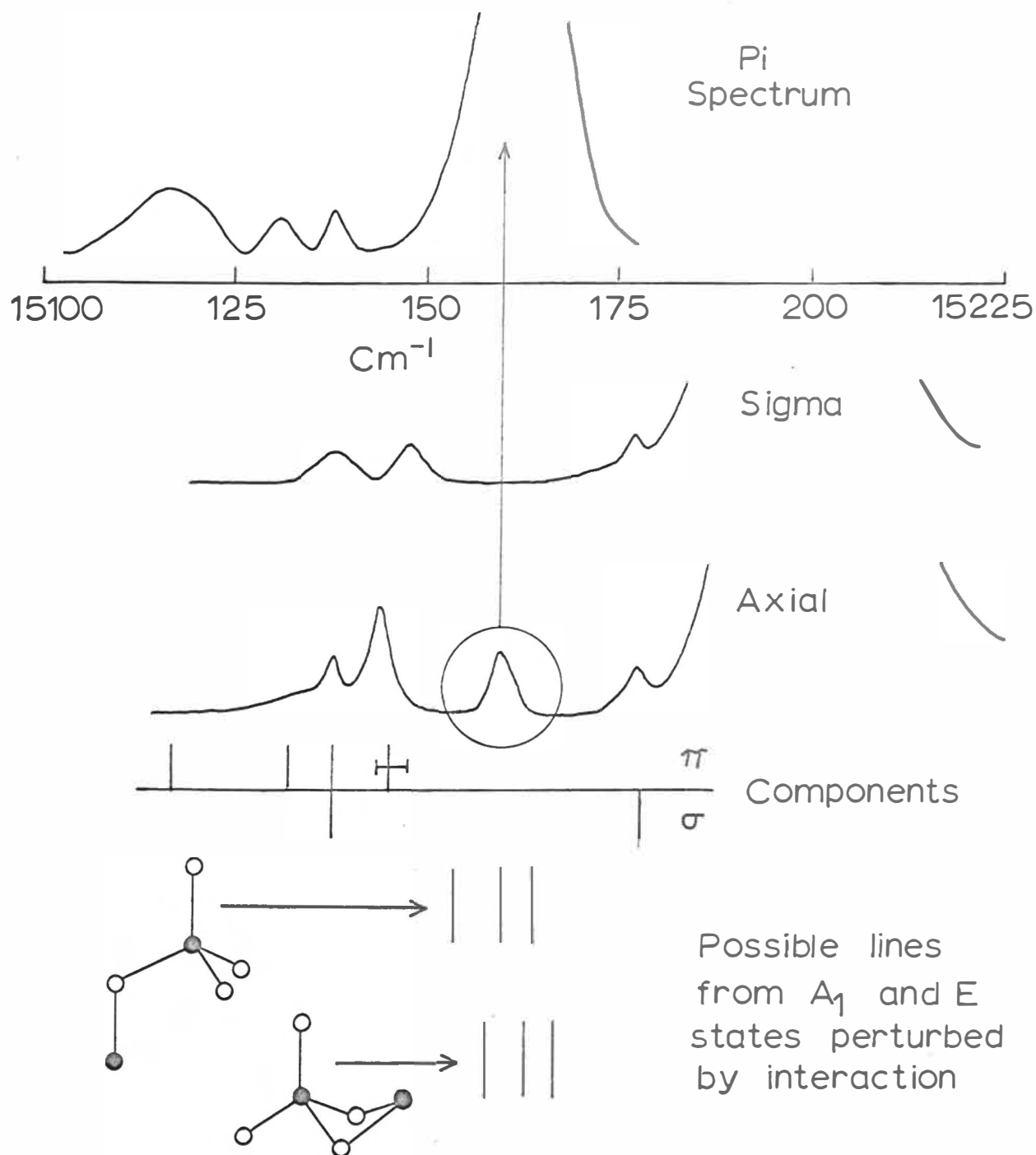


Figure 7-3 d^2 Cubic Field

Trigonal and cubic field representations and the main multiplet component are given for each level. The first line gives parameter values, the body of the table gives parameter dependence.

ENERGY	STATE		A40 -7027.944	A43 8400.000	A20 0.000	DELTA 4199.99	V 0.00	VPRIME 0.00	ZETA -500.	B 770.	C 3700.
47024	A1	1 S	-.0497	.1190	0.0000	.321	0.000	0.000	-.18846	13.73065	6.86017
22942	E	1 G	-.1582	.3783	0.0000	1.021	0.000	0.000	-.14961	2.04830	1.99317
21128	A1	1 G	-.0123	.0294	0.0000	.079	0.000	0.000	-.06443	4.25256	2.12524
20958	A2	1 G	-.1193	0.0000	.1194	.199	-.332	0.000	-.05134	3.99181	1.99855
20958	E	1 G	.0132	.1109	-.0597	.199	.166	0.000	-.05135	3.99181	1.99855
19356	A1	1 G	-.0888	-.0854	-.0740	-.022	-.109	-.671	-.13803	3.10199	1.99102
19356	E	1 G	.0495	.0303	.0370	-.022	.054	.335	-.13803	3.10199	1.99102
15646	A1	3 P	-.0120	.0287	0.0000	.077	0.000	0.000	-.76688	6.83448	.01327
15454	A2	3 P	-.0066	.0352	-.1428	.081	.183	-.455	-.48399	6.81091	.00012
15454	E	3 P	-.0156	.0277	.0714	.081	-.091	.227	-.48399	6.81092	.00012
15251	E	3 P	.0047	-.0114	0.0000	-.030	0.000	0.000	-.56330	5.60024	.31424
15148	A1	3 P	.0106	.0176	.1214	.017	-.116	.471	-.21746	6.13035	.16784
15148	E	3 P	-.0093	.0008	-.0607	.017	.058	-.235	-.21746	6.13035	.16784
13330	E	1 D	.0783	-.1872	0.0000	-.505	0.000	0.000	.97656	.10986	1.68455
12873	A1	1 D	.2311	-.0534	-.0277	-.493	.365	.612	.38863	-1.54714	1.81299
12873	E	1 D	-.0008	-.2475	.0138	-.493	-.182	-.306	.38863	-1.54714	1.81299
8582	A1	3 F	-.1769	.4344	.0023	1.164	.004	.024	-.27505	-7.95999	.01506
8582	E	3 F	-.1822	.4299	-.0011	1.164	-.002	-.012	-.27505	-7.95999	.01506
4555	A2	3 F	-.0309	.0740	0.0000	.199	0.000	0.000	-.50000	-8.00000	0.00000
4361	E	3 F	-.0229	.0549	0.0000	.148	0.000	0.000	-.47018	-7.96999	.00429
4331	E	3 F	-.0449	.0643	.0321	.203	-.067	.047	.13208	-7.95369	.01086
4331	A1	3 F	-.0048	.0978	-.0643	.203	.134	-.095	.13209	-7.95369	.01086
4235	E	3 F	-.0004	.0924	-.0248	.185	.090	.045	.03470	-7.99186	.00046
4235	A2	3 F	-.0853	.0214	.0497	.185	-.181	-.090	.03470	-7.99186	.00046
1028	E	3 F	.1569	-.2039	-.0211	-.670	.139	.170	-.39016	-7.77149	.00219
1028	A1	3 F	-.0021	-.3370	.0423	-.670	-.278	-.340	-.39016	-7.77149	.00219
878	E	3 F	.0981	-.2345	0.0000	-.633	0.000	0.000	.20654	-7.78842	.00371
311	E	3 F	.0338	-.3052	.0131	-.667	-.165	-.272	1.00064	-7.81086	.00086
311	A2	3 F	.2423	-.1308	-.0263	-.667	.330	.545	1.00064	-7.81087	.00085
0	A1	3 F	.1051	-.2513	0.0000	-.678	0.000	0.000	1.51978	-7.81769	.00130

Figure 7-4 Depopulation and Band Intensity

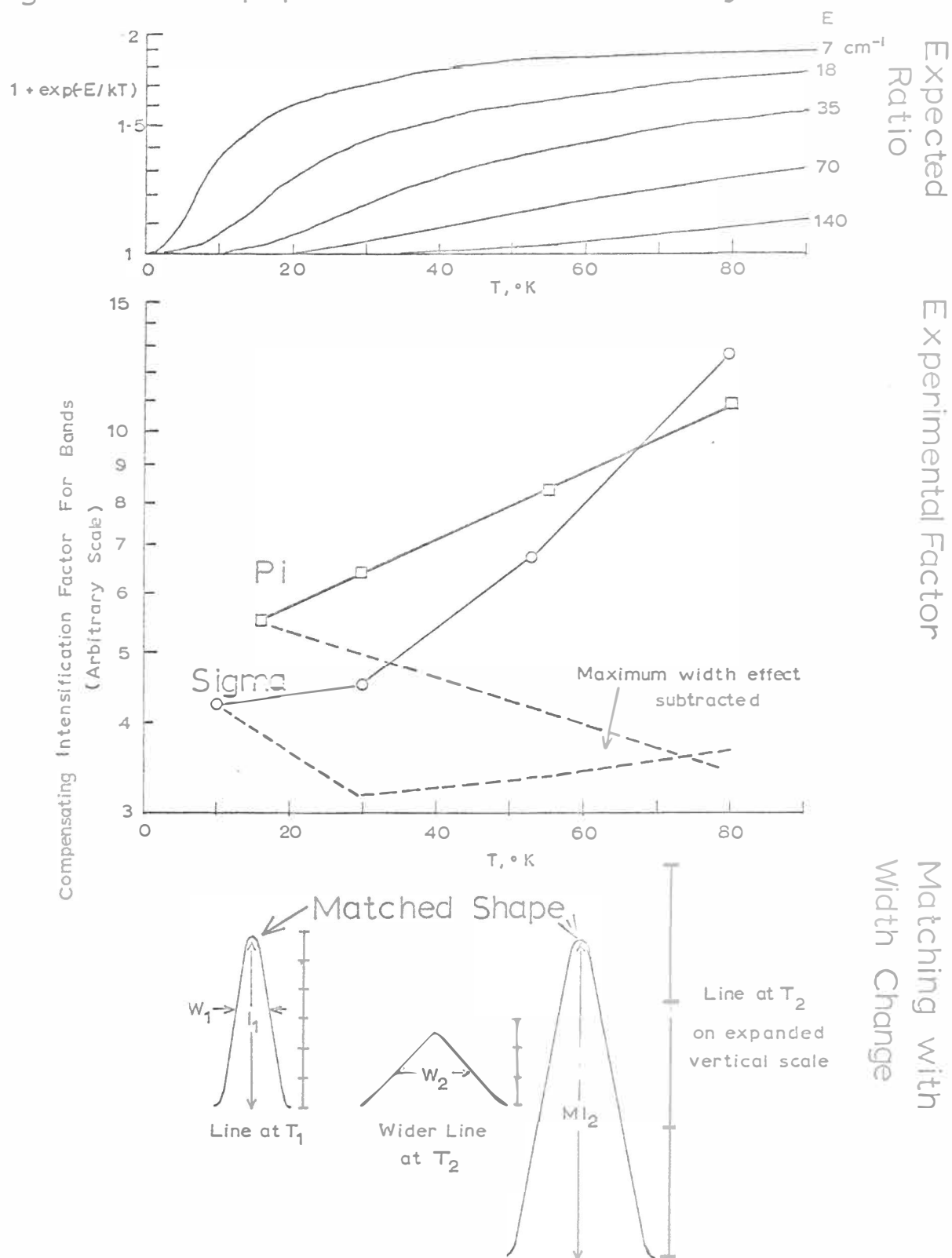


Figure 7-5

Parameter Dependence of
d⁸ First Excited State
Relative to A₁ Ground State

A₀² dependence in brackets

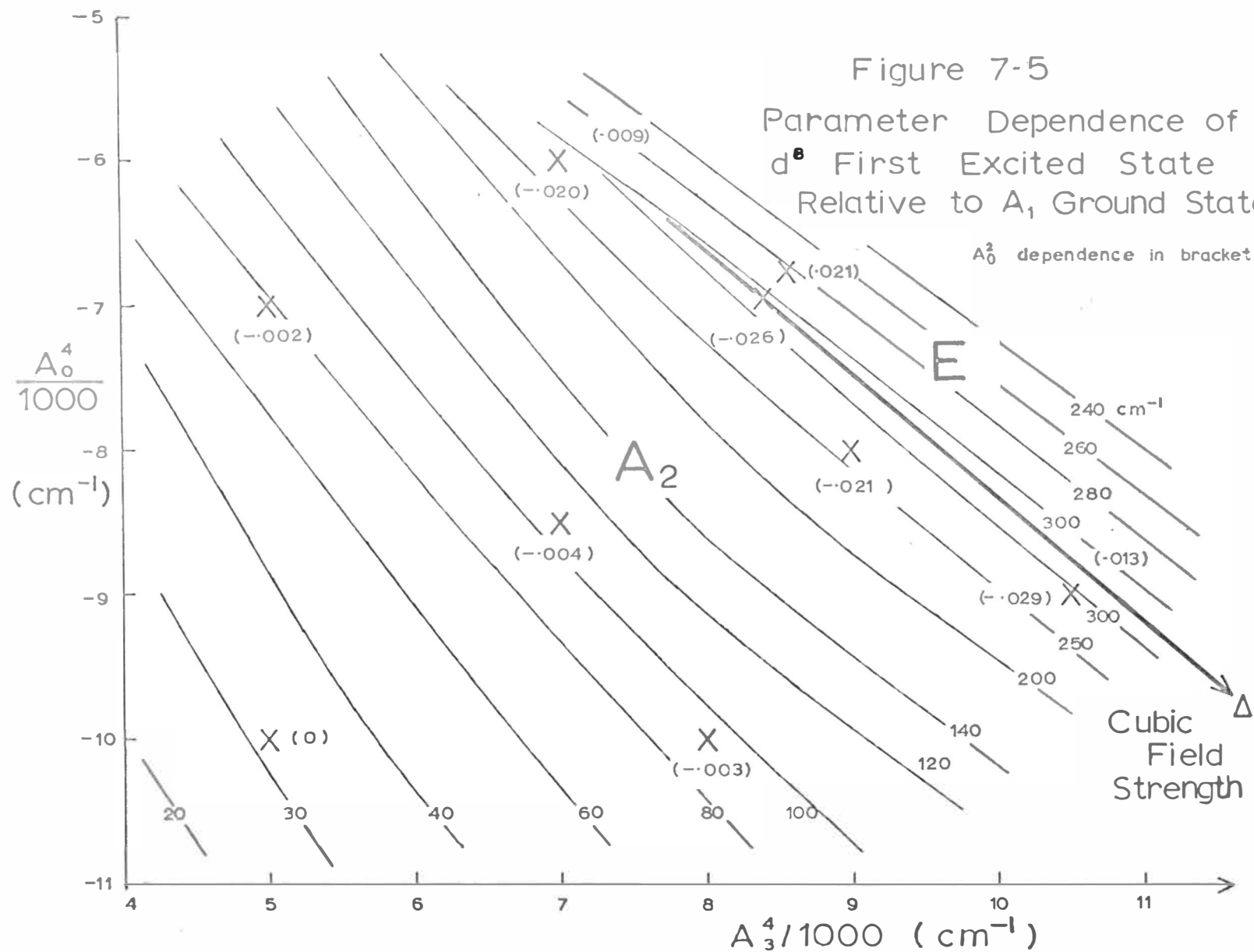


Figure 7-6 V and V' Dependence
of Splittings

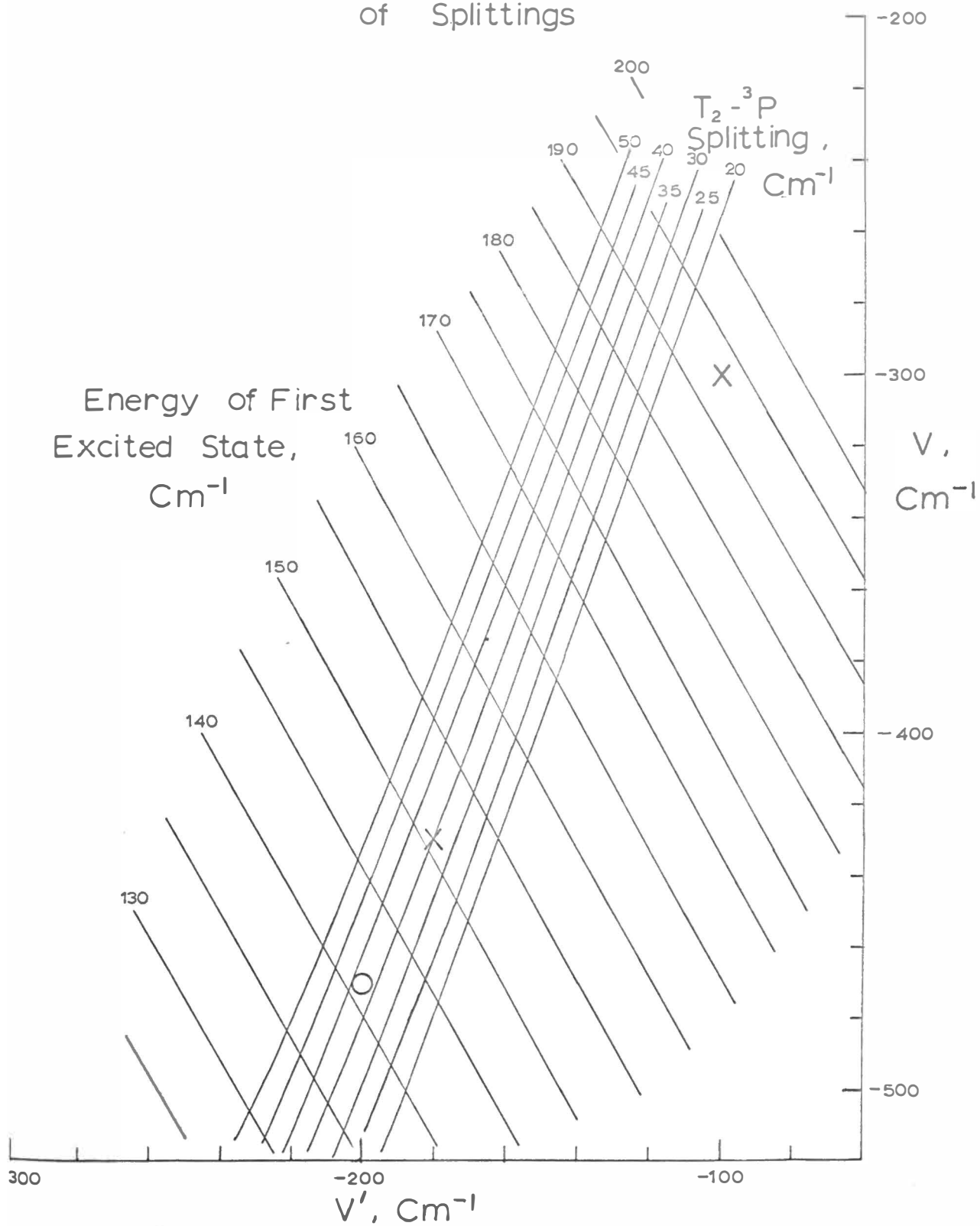


Figure 7-7 Trigonal Field Levels

Parameters are chosen to fit the energies of the first excited state and the two components of T_2 (3P)

ENERGY	STATE		DELTA 4199.99	V -469.99	VPRIME -199.99	ZETA -500.	B 770.	C 3700.	Energy for B = 765.5	No-Phonon Lines
47136	A1	1 S	.291	-.014	-.052	-.19069	13.77263	6.88109	47039	
23079	E	1 G	1.010	-.001	-.329	-.14817	2.06364	1.99328	23035	
21255	A1	1 G	.108	-.055	.005	-.06158	4.20062	2.09951	21201	
21218	A2	1 G	.199	-.332	0.000	-.05021	3.99214	1.99862	21165	
20962	E	1 G	.206	.109	.161	-.05422	3.95731	1.99835	20929	
19628	A1	1 G	-.008	-.060	-.606	-.13879	3.02790	1.99590	19579	
19354	E	1 G	-.028	.087	.380	-.13788	3.15434	1.99070	19304	
15756	A1	3 P	.078	-.003	-.047	-.76582	6.82460	.01330	15689	
15566	A2	3 P	.078	.169	-.453	-.48722	6.82210	.00009	15499	
15563	E	3 P	.084	-.099	.173	-.48115	6.78785	.00020	15496	
15381	E	3 P	-.041	-.128	.035	-.61843	5.42727	.34698	15321	
15264	E	3 P	.012	.148	-.367	-.24377	6.11033	.17603	15201	15200
15226	A1	3 P	.040	-.137	.384	-.08828	6.29705	.12070	15163	15163
13543	E	1 D	-.473	-.301	-.265	.99514	-.00418	1.65115	13540	
12992	E	1 D	-.502	.163	.098	.47126	-1.27521	1.80760	12989	
12668	A1	1 D	-.519	.439	.590	.20739	-1.70527	1.85488	12665	
8680	E	3 F	1.163	-.002	.085	-.29032	-7.94286	.01373	8680	
8669	A1	3 F	1.159	.004	.124	-.23913	-7.91115	.01885	8669	8343
4694	A2	3 F	.199	-.157	.003	-.42280	-7.99891	.00006	4694	
4598	E	3 F	.170	-.322	-.043	-.19270	-7.95787	.00696	4598	
4414	A2	3 F	.178	-.024	-.159	-.07374	-7.98178	.00036	4414	
4399	A1	3 F	.188	.130	-.160	.06252	-7.93376	.01237	4399	4248
4375	E	3 F	.180	.152	-.043	-.11131	-7.96224	.00701	4375	4217
4259	E	3 F	.186	.177	0.000	.05077	-7.98741	.00107	4259	
1421	A1	3 F	-.667	-.485	-.628	-.19040	-7.74327	.00206	1421	
1295	E	3 F	-.650	-.477	-.601	.16492	-7.75657	.00276	1295	
863	E	3 F	-.657	.281	.382	-.19665	-7.79601	.00275	863	
372	E	3 F	-.661	.212	.332	.79253	-7.81839	.00134	372	
141	A2	3 F	-.656	.345	.607	1.03399	-7.83355	.00084	141	(140)
0	A1	3 F	-.671	.222	.390	1.40480	-7.82934	.00128	0	

Figure 7-8 Wurtzite $\underline{k} = 0$ Modes

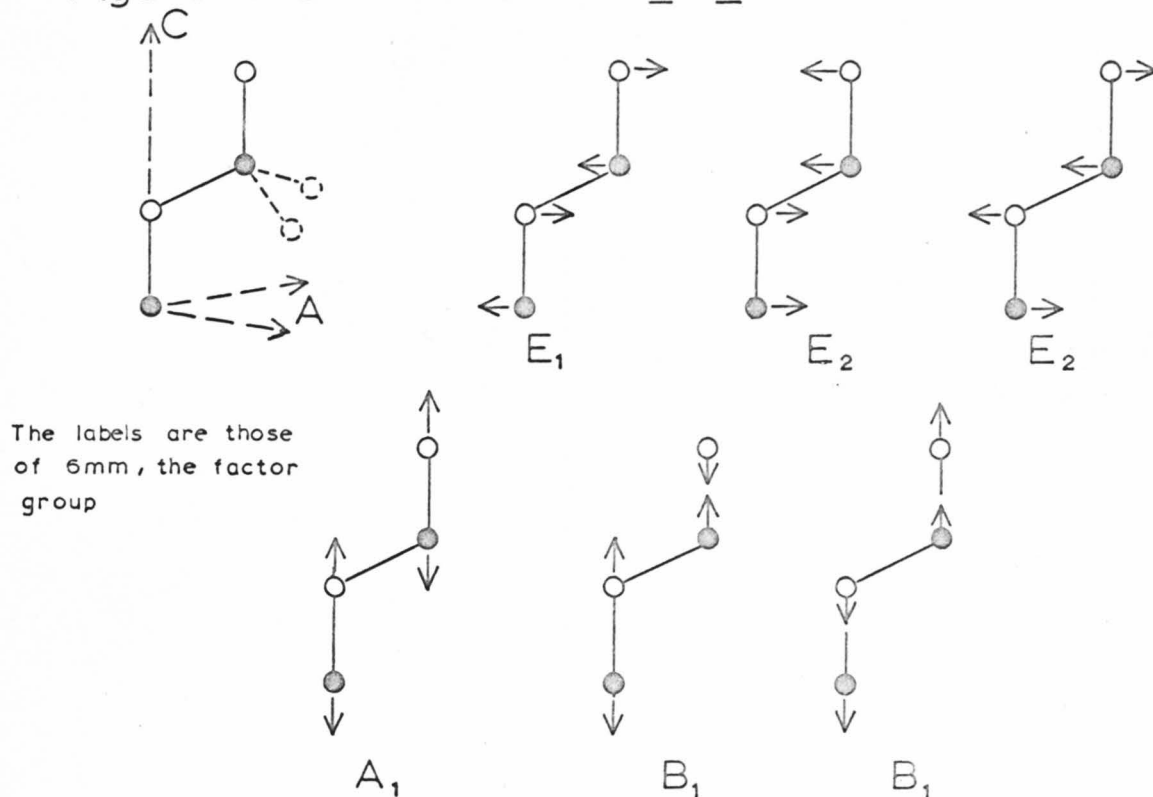


Figure 7-9 Peaks in the ZnO Phonon Distribution

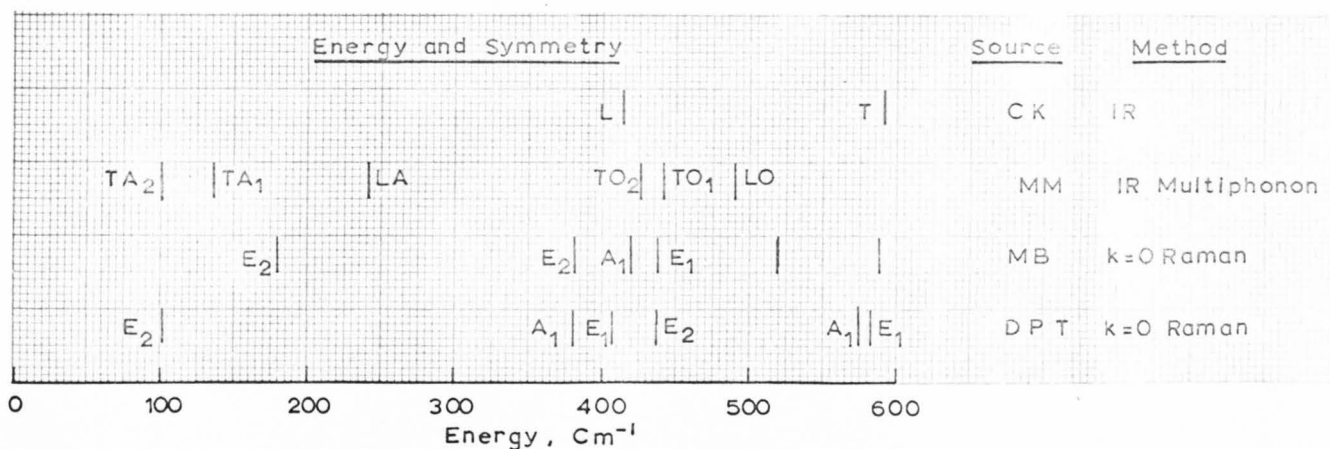
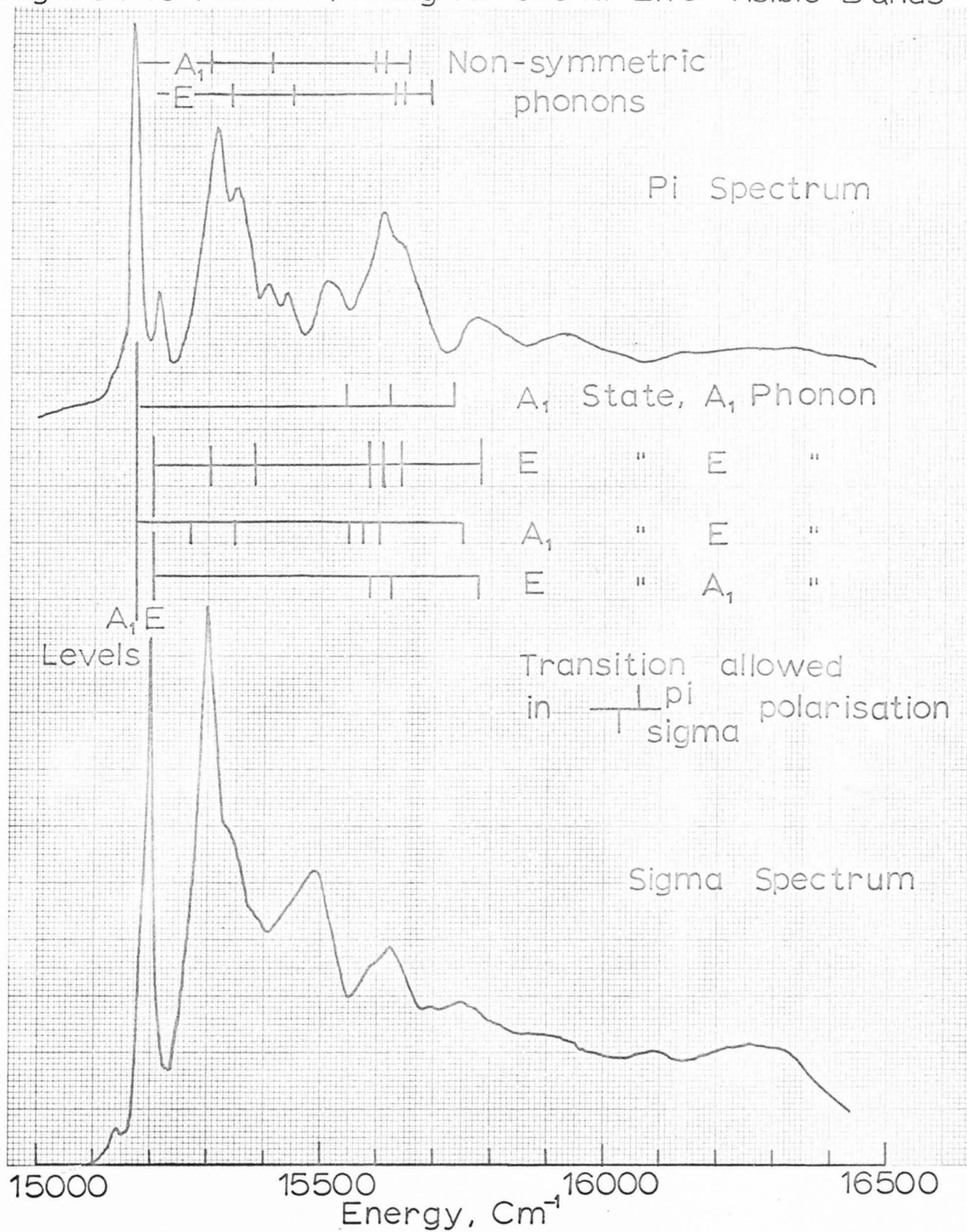
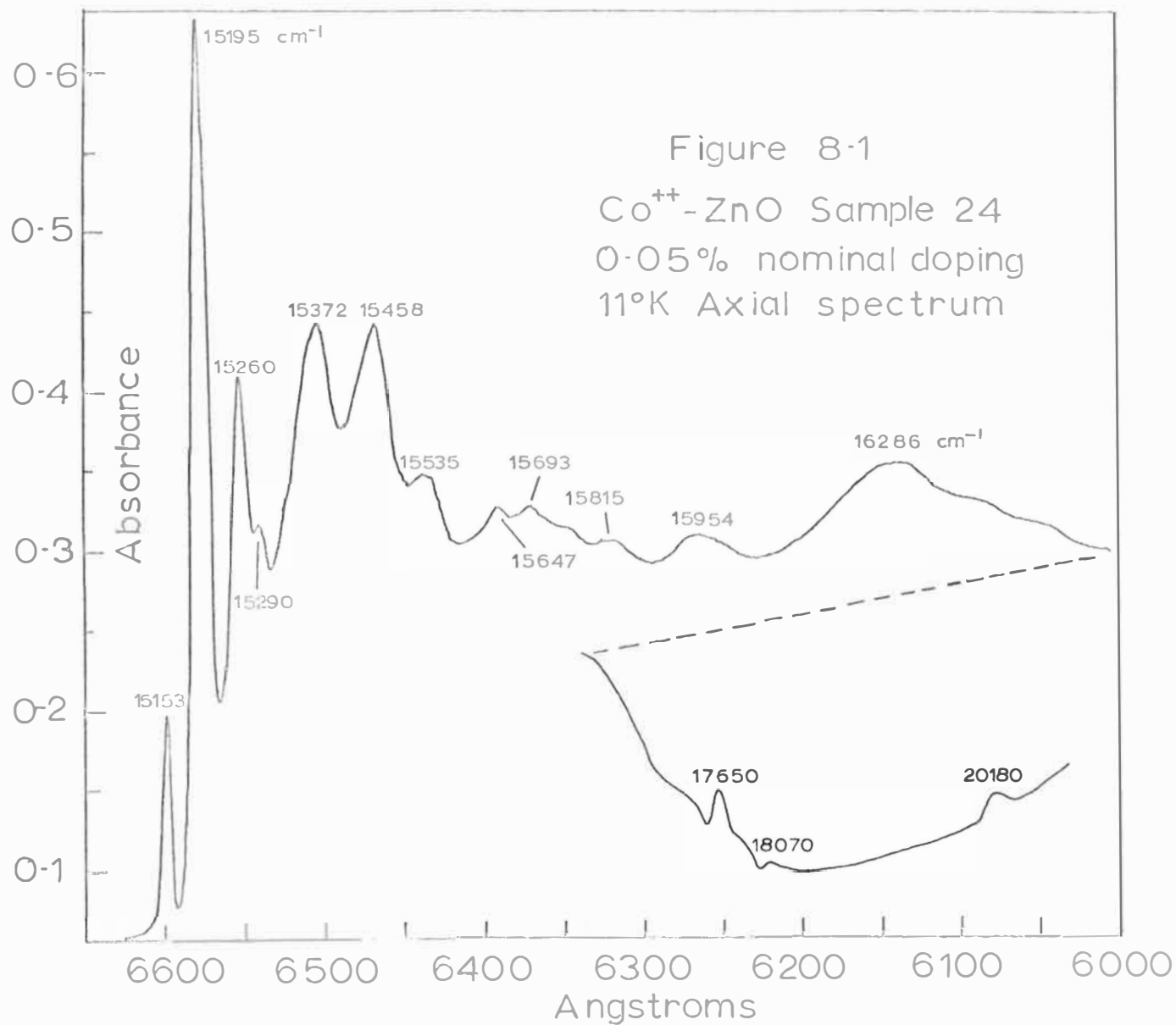


Figure 7-10 Phonon Fitting for the Ni-ZnO Visible Bands





Absorbance

Figure 8-2

Co⁺⁺-ZnO Sample 22
13°K Axial spectrum

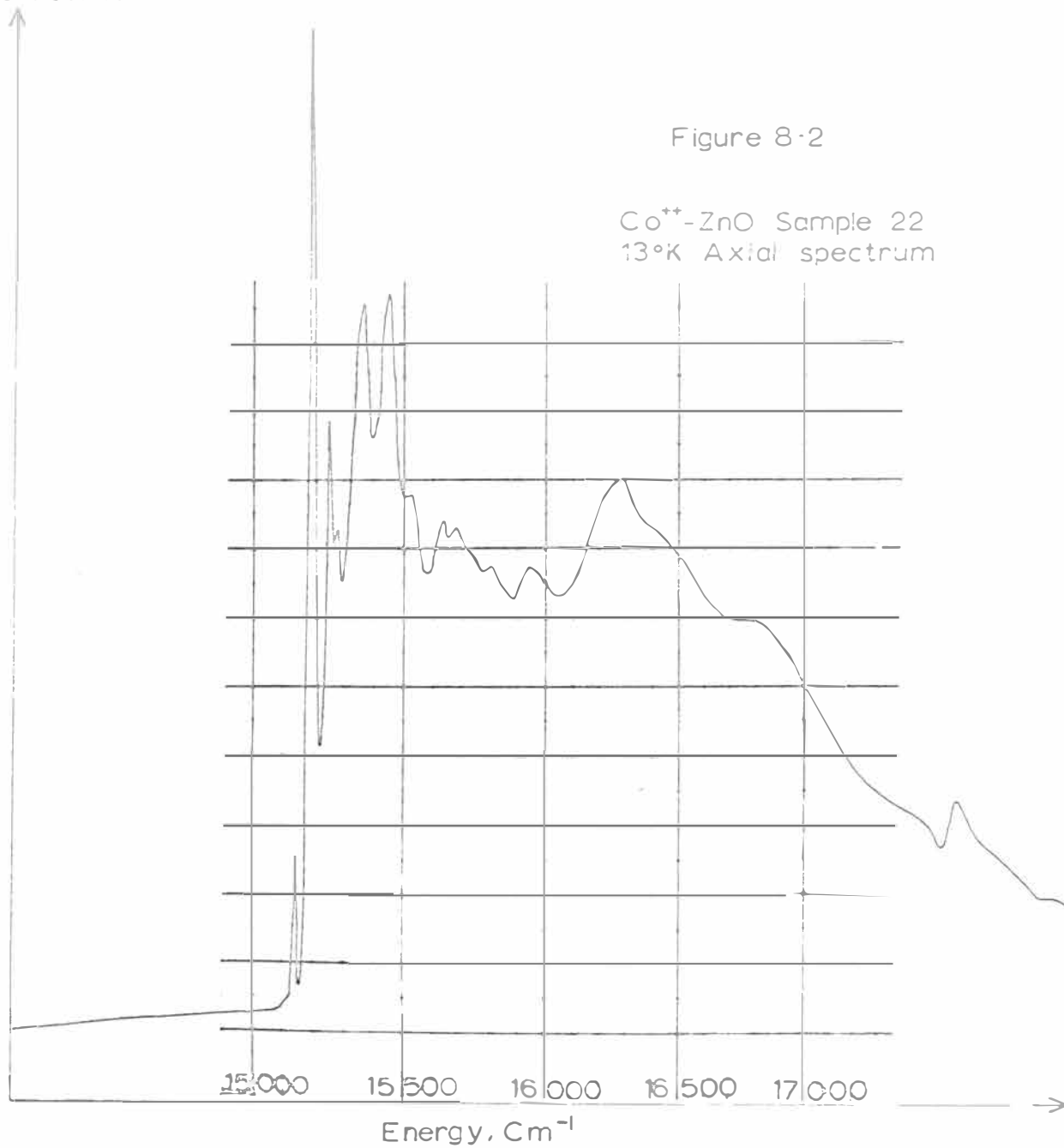


Figure 8-3
Co⁺⁺-ZnO Sample 24
Temperature Dependence
of Axial Spectrum

Absorbance

11°K

32

40

60

80

93

130°K

210°K

Energy

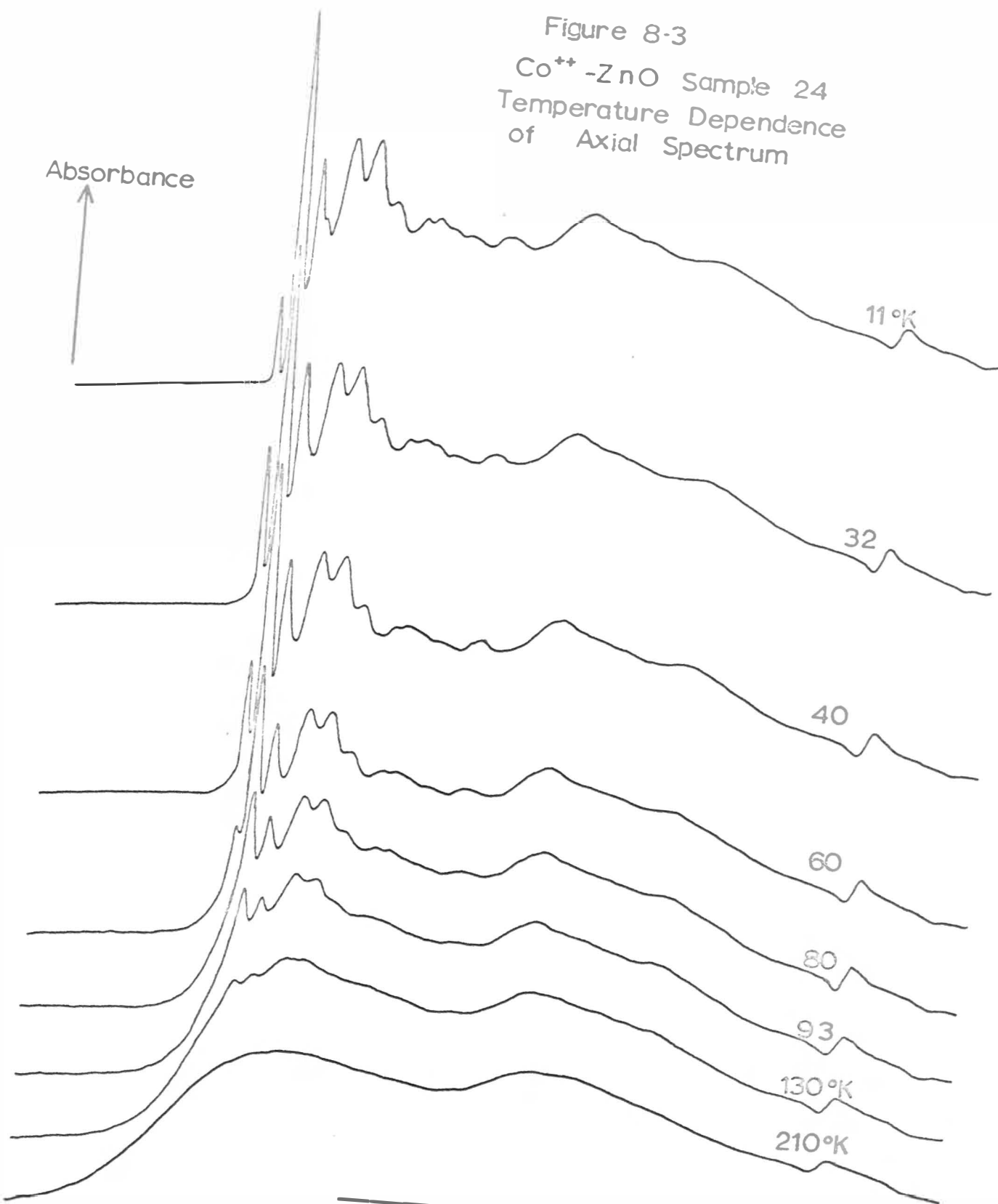


Figure 8.4 Co^{++} -ZnO Axial Spectrum (J-A)

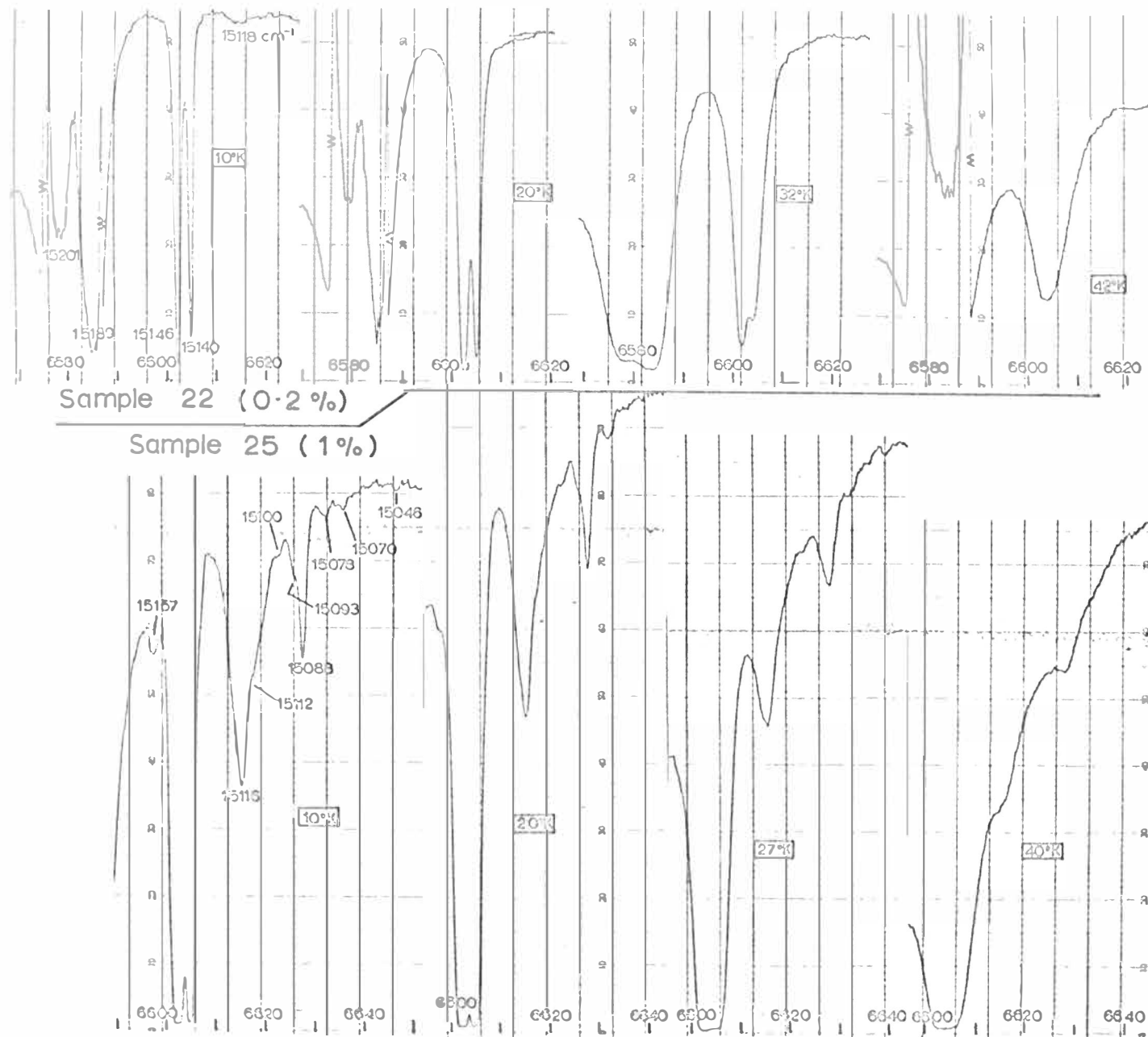


Figure 8-5 Co^{++} -ZnO Pi Spectrum (J-A)

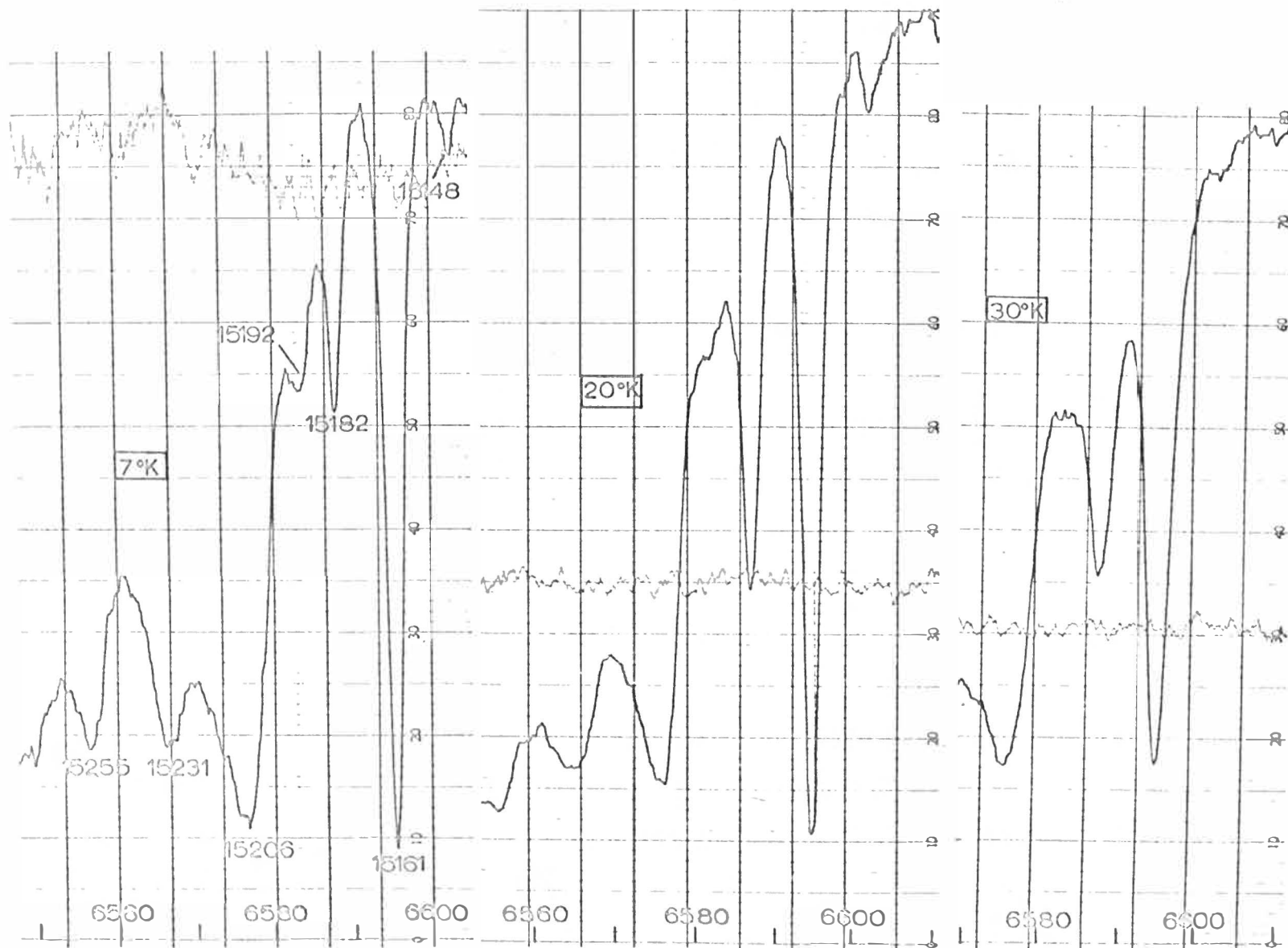


Figure 8-6 Concentration Dependence of Co-ZnO Weak Lines

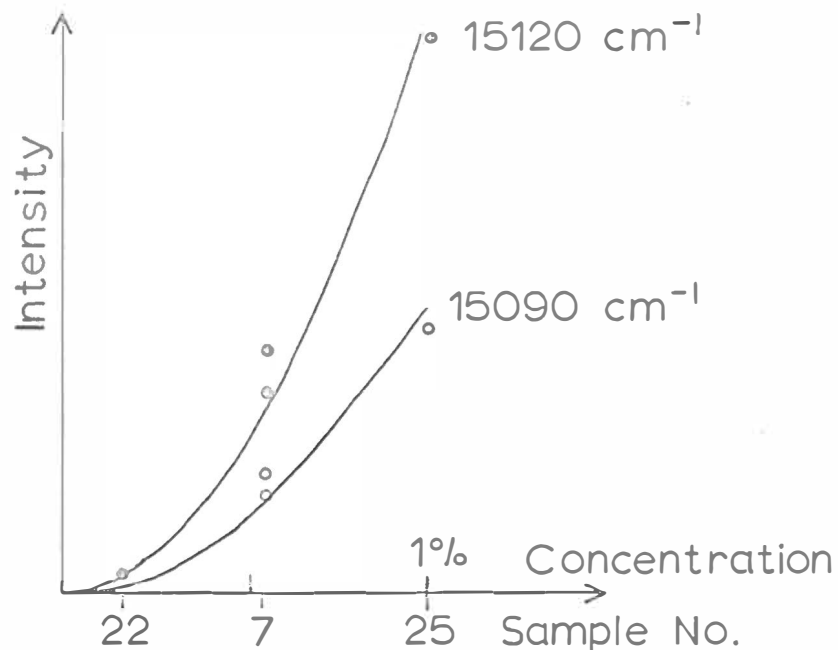


Figure 8-7 The No-Phonon Lines

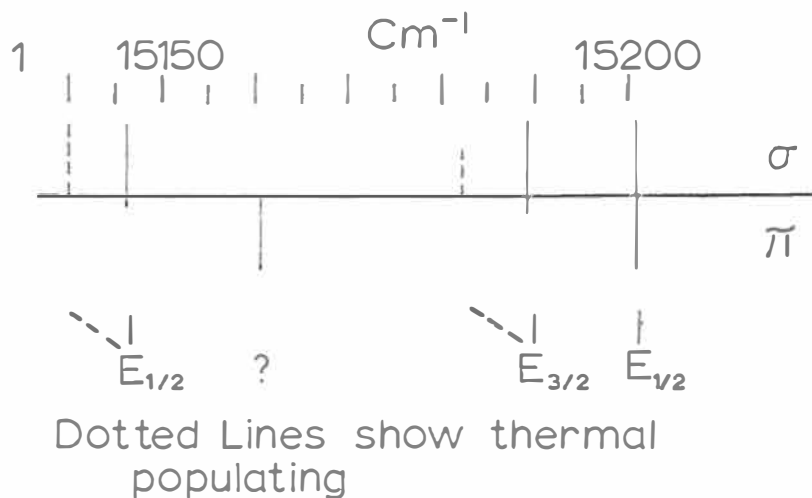


Figure 8-8 Phonon Fitting for the
Co-ZnO Axial Spectrum

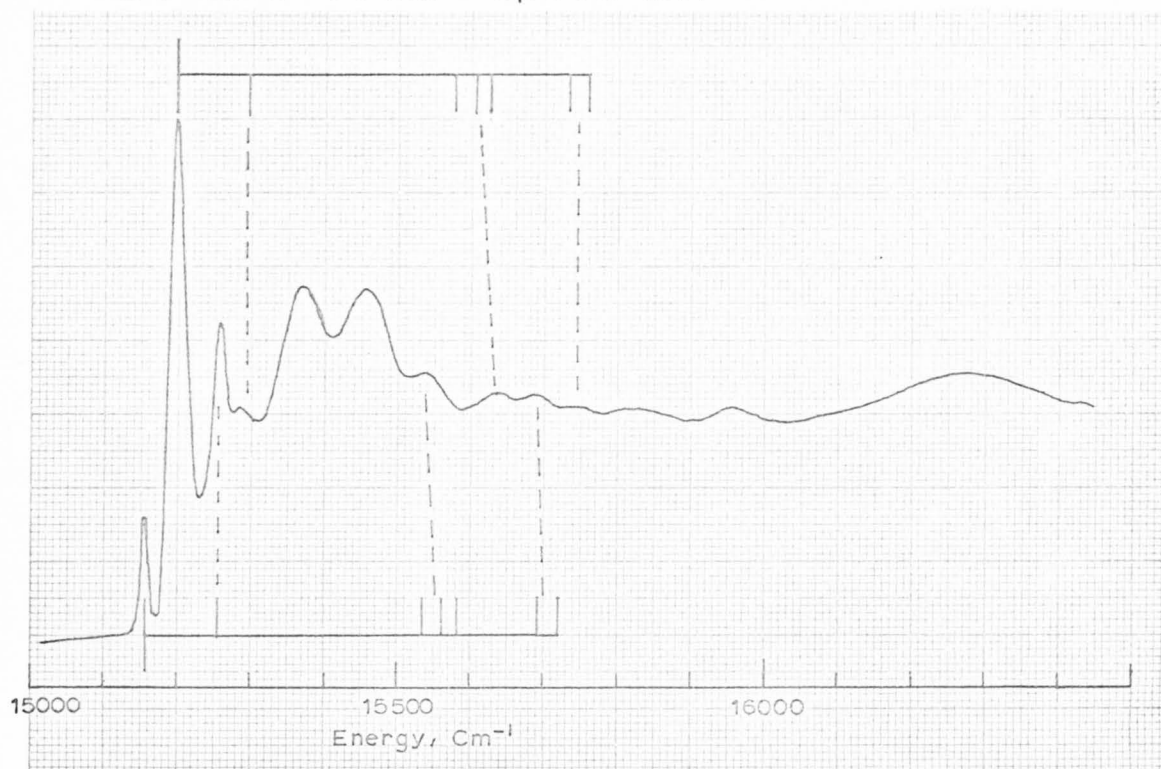


Figure A1
Correction to Apparent
Absorbance for a
Crystal Wedge

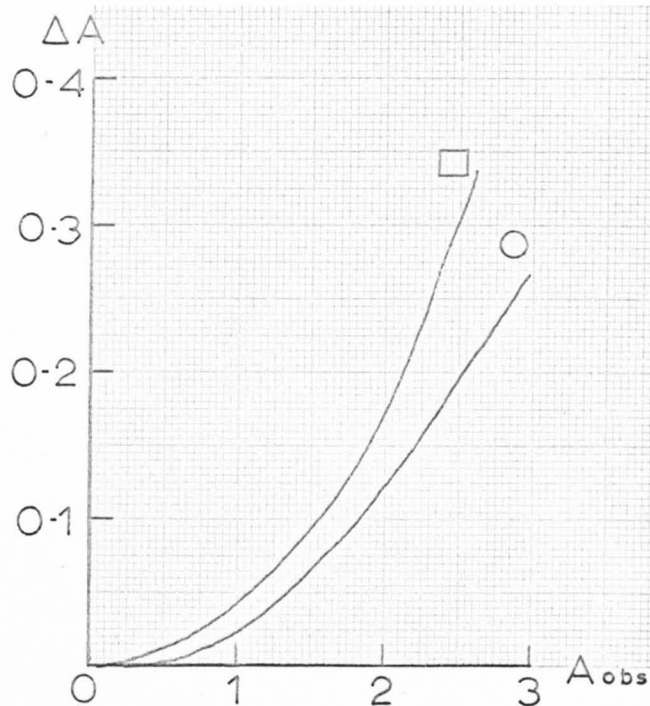
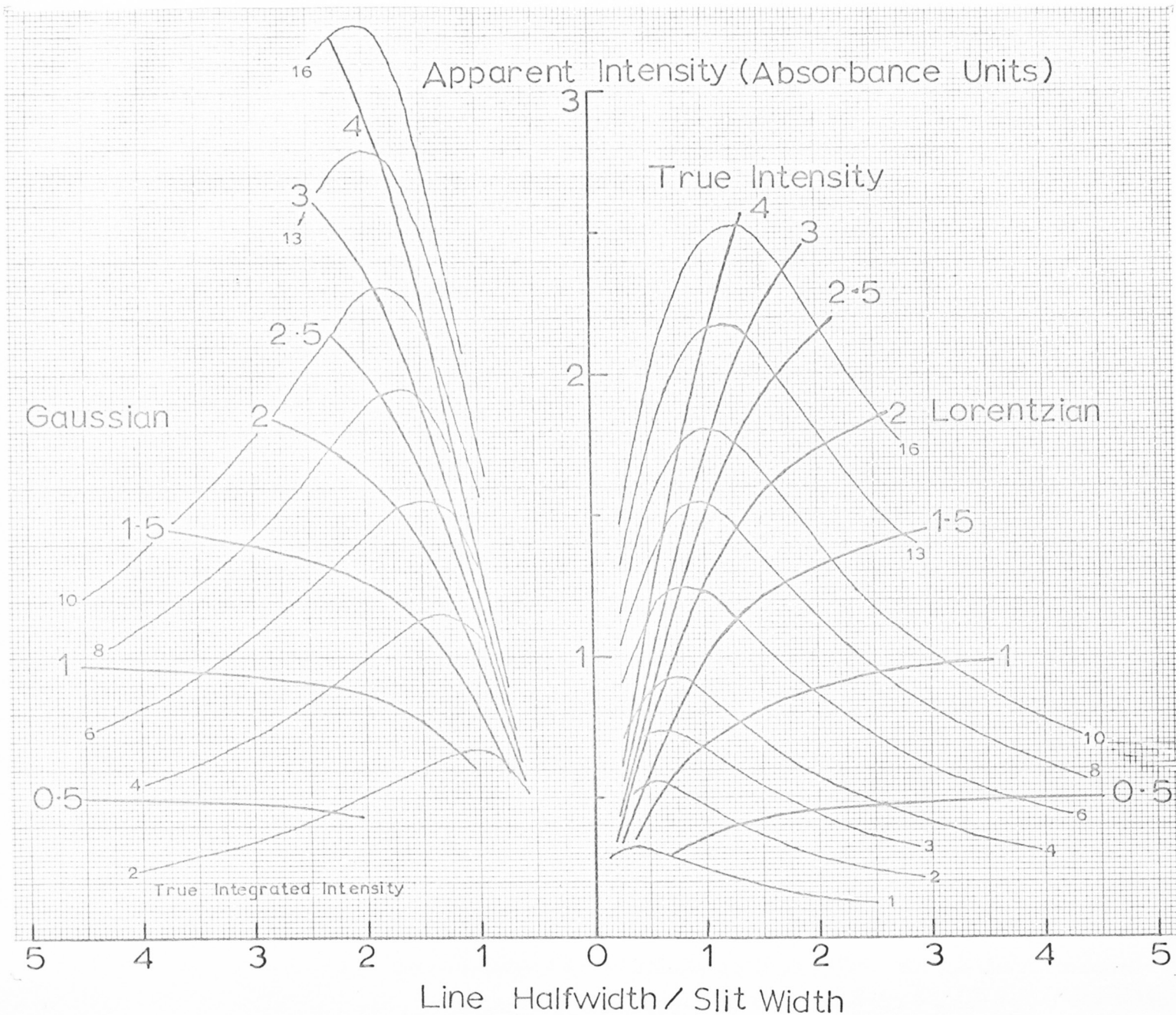


Figure A2 Apparent Intensity of Slit-limited Absorption Lines as a Function of Width



APPENDIX ONE

HEAT FLOW IN THE SAMPLE HOLDER AND SAMPLE

The heat input to the sample holder will be from two sources.

1 Black body radiation from the nitrogen shield and through the windows.

2 Energy absorbed from the light beam.
For both, take a worst possible case.

1 The nitrogen shield had two windows of 3 cm² area. Assume that all the radiation from a black body at 300°K passing through these windows is absorbed by the holder. Then heat flow in

$$\begin{aligned} W &= A \sigma T^4 \\ &= 6 \times 5.7 \times 10^{-12} \times 300^4 \text{ watts} \\ &= 0.28 \text{ watts.} \end{aligned}$$

The holders were electropolished, giving an emissivity⁶² of say 0.02, so this can be reduced to 6 mw.

2 The lamp filament is imaged onto the crystal by the condenser system. For a final image 2 mm high produced by rays in 0.6 sterad of solid angle, 0.3% of the light from an 8 mm filament is used. Assuming the lamp is 1% efficient, radiating 1 watt of visible light, 3 mw is incident on the sample. This is less than the previous power, and so does not affect the sample holder, but being incident directly on the crystal, which has low thermal conductivity, it may raise its temperature above that of the

holder.

Now assuming a 1 cm path length between crystal and dewar base, with heat flow across a 0.2 cm^2 area, we have

$$W = k A \frac{\Delta T}{l}$$

$$\Delta T = \frac{W}{k} \frac{l}{A}$$

Taking $k = 1 \text{ watt/cm deg K}$ at 10 degrees, for commercial copper,

$$\Delta T = 1.5 \text{ degrees K for } 0.3 \text{ watts.}$$

The lowest temperature actually observed was 7°K , i.e.

$\Delta T = 2.8 \text{ degrees}$. The extra could have occurred across the Indium gasket or be due to poor thermocouple contact.

For temperature gradients across the crystal, consider 3 mw flowing from a line image in the crystal, through an area of typically 1 mm^2 , for 1 mm distance. Then from $\Delta T = Wl/(kA)$, we have $\Delta T = \frac{3}{100k}$, with T in degrees and k in watts/cm $^\circ\text{K}$. Since k will certainly be higher than 0.01, ΔT will be less than 3°K , and may be much less. The actual differential will of course vary with sample and sample mounting.

APPENDIX TWO

ABSORBANCE OF A WEDGE-SHAPED CRYSTAL

Consider a homogeneous beam of monochromatic light of intensity I incident on an area of crystal for which the thickness is a linear function of one co-ordinate x , with the origin as the crystal centre,

$$t = ax + t_0,$$

and optical density α .

Then light transmitted

$$= I \int e^{-\alpha t(x,y)} dx dy$$

$= I A e^{-\alpha t_0} K$, where A is the area observed and K depends on a , α , and the geometry. If A is a rectangular area aligned to the axes, and of x dimension $2d$,

$$K = \frac{\sinh(\alpha ad)}{2\alpha ad}.$$

If A is a circular area of radius r , the result is

$$K = \frac{2 I_1(\alpha ad)}{\alpha ad}$$

where I_1 is the modified Bessel function of the first kind, of first order.

The correction appropriate absorbance is $\ln(K)$.

Figure A1 shows this as a function of apparent absorbance for parameters appropriate to sample 6.3 and its holder and the correction for a square hole of the same diameter.

APPENDIX THREEINSTRUMENTAL EFFECTS IN SPECTRA

The two effects observed in the spectra of Chapter Six, namely slit limiting on the Bausch and Lomb and intensity cutoff on the Jarrell-Ash, will be discussed here.

Intensity Limiting of Absorption Lines

The spectra showed a cutoff of intensity at absorbance 2 which could not be accounted for by errors in the zero level, and was below the expected noise limit. The limiting must therefore have been caused by stray light passing the crystal by some means and reaching the detector.

Polarised light was used, and since the two strong lines observed were at different wavelengths, any light of incorrect polarisation would be passed by the crystal. The expected transmittances were 0.06% due to polarisation impurity and 0.2% for incorrect alignment. Transmittances are additive to give the final intensity reaching the detector.

It was found that due to an internal reflection in the quartz plate in the Jarrell-Ash used to direct energy to the monitor phototube, a ghost spectrum was formed at the exit slit displaced 1 mm from the main spectrum. With dispersion 3.3 A/mm, this was sufficient to partially clear the strong lines and give a transmittance estimated at 0.2% at the line peaks.

The three contributions add to give transmittance 0.5%, corresponding to absorbance 2.3, which is near the observed limit. Some of the errors may be underestimated, or other

effects may be significant. McClure³¹ found that accurate readings were only obtained after small cracks in the crystals were filled to stop residual transmission.

Slit-Limiting of Absorption Lines

The calculations of Kostkowski and Bass³² do not cover many cases, and Kyle and Green³³ give figures only for the transmittance and halfwidth of Lorentzian lines. It was decided to perform similar calculations for Gaussian and Lorentzian lines for results in absorbance units. The slit function was taken as Gaussian for convenience.

The integrations to find apparent line intensity were done for lines of constant true integrated area and varying width, using a computer program. From the plots of the results, curves showing apparent intensity as a function of width for lines of constant real intensity can also be drawn, as in Figure A2. The curves of constant integrated intensity are of interest to the present spectra, since no-phonon lines sharpen as temperature decreases. With the width axis relabelled as temperature, the constant area curves show temperature dependence very similar to that of the sharp line of Figure 6.5.

The Lorentzian line, having wider wings, should show less loss of intensity when narrow and strong than the Gaussian. It can be seen that the true intensity curves fall closer to the Intensity axis for the Lorentzian case, verifying that of two lines showing the same intensity reduction, the

Lorentzian is narrower. The apparently high integrated intensity curves for the Gaussian are deceptive, since the wings of a Lorentzian contribute to its area, with apparent reduction in intensity for the constant area curve.

```

A1(D2) A40 TRIG      3      1
 1000000  1000000  1040400
10000000.E-01 00000000.E-99
10202000.E-01 00000000.E-99 13659754.E-08
10404000.E-01 29814237.E-08-25453450.E-08 10244815.E-08
 1040403  1040403  1040403
10404030.E-01-11952285.E-08
 3010000  3010000  3030403
30100000.E-01 00000000.E-99
30102000.E-01 00000000.E-99 00000000.E-99
30302000.E-01 00000000.E-99-12777530.E-08-12521442.E-08
30303030.E-01 00000000.E-99 00000000.E-99 00000000.E-99-19920475.E-09
30304000.E-01-12171612.E-08 61475922.E-09 98580787.E-09 00000000.E-99
-15367224.E-08
30304030.E-01 00000000.E-99 00000000.E-99 00000000.E-99 17251636.E-08
00000000.E-99 17928428.E-08
A1(D2) A43 TRIG      2      1
 1000000  1000000  1040403
10000000.E-01 00000000.E-99
10202000.E-01 00000000.E-99 00000000.E-99
10404000.E-01 00000000.E-99 00000000.E-99 00000000.E-99
10404030.E-01 42163700.E-08 12598815.E-08-16903084.E-08 00000000.E-99
 3010000  3010000  3030403
30100000.E-01 00000000.E-99
30102000.E-01 00000000.E-99 00000000.E-99
30302000.E-01 00000000.E-99 00000000.E-99 00000000.E-99
30303030.E-01 00000000.E-99-15811388.E-08 30988988.E-08 00000000.E-99
30304000.E-01 00000000.E-99 00000000.E-99 00000000.E-99-24397499.E-08
00000000.E-99
30304030.E-01-17213258.E-08-30429030.E-09-48794999.E-09 00000000.E-99
25354626.E-08 00000000.E-99
A1(D2) A20 TRIG      3      1
 1000000  1000000  1040400
10000000.E-01 00000000.E-99
10202000.E-01 40000000.E-08 10244815.E-08
10404000.E-01 00000000.E-99 18326484.E-08-34149388.E-08
 1040403  1040403  1040403
10404030.E-01 11952285.E-08
 3010000  3010000  3030403
30100000.E-01 00000000.E-99
30102000.E-01-23664318.E-08 16733200.E-08
30302000.E-01 25298220.E-08-51110121.E-09-81958532.E-09
30303030.E-01 00000000.E-99 00000000.E-99 00000000.E-99 89642139.E-09
30304000.E-01 00000000.E-99 26557599.E-08 11829694.E-09 00000000.E-99
-85373466.E-09
30304030.E-01 00000000.E-99 00000000.E-99 00000000.E-99-51754913.E-09
00000000.E-99 29880714.E-09

```

```

E(D2)  A40 TRIG      4      1
1020201  1020201  1040402
10202010.E-01-91065029.E-09
10202020.E-01 00000000.E-99 22766258.E-09
10404010.E-01-69707141.E-09 00000000.E-99 51224082.E-09
10404020.E-01 00000000.E-99 29574236.E-08 00000000.E-99-62607211.E-09
10404040.E-01 79681906.E-09
3010101  3010101  3030402
30101010.E-01 00000000.E-99
30102010.E-01 00000000.E-99 00000000.E-99
30102020.E-01 00000000.E-99 00000000.E-99 00000000.E-99
30302010.E-01 00000000.E-99 85183538.E-09 00000000.E-99 83476282.E-09
30302020.E-01 00000000.E-99 00000000.E-99-21295884.E-09 00000000.E-99
-20869070.E-09
30303010.E-01 59761429.E-09 99602375.E-09 00000000.E-99-19521227.E-08
00000000.E-99-66401588.E-10
30303020.E-01 00000000.E-99 00000000.E-99-62994076.E-09 00000000.E-99
12346308.E-08 00000000.E-99 46481111.E-09
30304010.E-01 11785112.E-08 16835873.E-09 00000000.E-99 26997460.E-09
00000000.E-99-15152286.E-08 00000000.E-99-76836123.E-09
30304020.E-01 00000000.E-99 00000000.E-99-71428571.E-09 00000000.E-99
-11454052.E-08 00000000.E-99-11293848.E-08 00000000.E-99 93910811.E-09
3030404  3030404  3030404
30304040.E-01-11952285.E-08
E(D2)  A43 TRIG      2      1
1020201  1020201  1040404
10202010.E-01 00000000.E-99
10202020.E-01 13468699.E-08 00000000.E-99
10404010.E-01 00000000.E-99 24743582.E-08 00000000.E-99
10404020.E-01-29160589.E-08 00000000.E-99 47619047.E-09 00000000.E-99
10404040.E-01-30860669.E-08 00000000.E-99-12598815.E-08 00000000.E-99
00000000.E-99
3010101  3010101  3030404
30101010.E-01 00000000.E-99
30102010.E-01 00000000.E-99 00000000.E-99
30102020.E-01 00000000.E-99 00000000.E-99 00000000.E-99
30302010.E-01 00000000.E-99 00000000.E-99-12598815.E-08 00000000.E-99
30302020.E-01 00000000.E-99-12598815.E-08 00000000.E-99-12346308.E-08
00000000.E-99
30303010.E-01 00000000.E-99 00000000.E-99 11785112.E-08 00000000.E-99
23097828.E-08 00000000.E-99
30303020.E-01 11180339.E-08-37267796.E-09 00000000.E-99 73041747.E-09
00000000.E-99 24845198.E-09 00000000.E-99
30304010.E-01 00000000.E-99 00000000.E-99-59761429.E-09 00000000.E-99
95831479.E-09 00000000.E-99 18898223.E-08 00000000.E-99
30304020.E-01-98601324.E-09 70429514.E-09 00000000.E-99 11293848.E-08
00000000.E-99-84515422.E-09 00000000.E-99-71428571.E-09 00000000.E-99
30304040.E-01 74535595.E-09 74535595.E-09 00000000.E-99 11952285.E-08
00000000.E-99 22360679.E-08 00000000.E-99 18898223.E-08 00000000.E-99
00000000.E-99

```

```

E(D2) A20 TRIG      4      1
1020201 1020201 1040402
10202010.E-01 51224082.E-09
10202020.E-01 00000000.E-99-10244815.E-08
10404010.E-01 16729713.E-08 00000000.E-99-29026979.E-08
10404020.E-01 00000000.E-99 11829694.E-08 00000000.E-99-13659754.E-08
1040404 1040404 1040404
10404040.E-01 47809143.E-08
3010101 3010101 3030402
30101010.E-01 83666002.E-09
30102010.E-01 25099800.E-08 83666002.E-09
30102020.E-01 00000000.E-99 00000000.E-99-16733200.E-08
30302010.E-01 17888543.E-08-25555060.E-09 00000000.E-99-40979265.E-09
30302020.E-01 00000000.E-99 00000000.E-99 51110121.E-09 00000000.E-99
81958532.E-09
30303010.E-01 19123656.E-08 95618284.E-09 00000000.E-99-38332592.E-09
00000000.E-99-53785286.E-09
30303020.E-01 00000000.E-99 00000000.E-99 15118578.E-08 00000000.E-99
-60609148.E-09 00000000.E-99 00000000.E-99
30304010.E-01 00000000.E-99 24243659.E-08 00000000.E-99 10798984.E-09
00000000.E-99-25253811.E-09 00000000.E-99-72567449.E-09
30304020.E-01 00000000.E-99 00000000.E-99 17142857.E-08 00000000.E-99
76360352.E-10 00000000.E-99-45175393.E-09 00000000.E-99-34149388.E-09
3030404 3030404 3030404
30304040.E-01 11952285.E-08

```

```

A2(D2) A40 TRIG      3      1
1040403 1040403 1040403
10404030.E-01-11952285.E-08
3010100 3010100 3030300
30101000.E-01 00000000.E-99
30303000.E-01-97589999.E-09-39840952.E-09
3030303 3030303 3030403
30303030.E-01-19920475.E-09
30304030.E-01 17251636.E-08 17928428.E-08
A2(D2) A43 TRIG      2      1
1040403 1040403 1040403
10404030.E-01
3010100 3010100 3030403
30101000.E-01 00000000.E-99
30303000.E-01 00000000.E-99 00000000.E-99
30303030.E-01-91287088.E-09 74535595.E-09 00000000.E-99
30304030.E-01-15811388.E-08 12909944.E-08 00000000.E-99 00000000.E-99
A2(D2) A20 TRIG      3      1
1040403 1040403 1040403
10404030.E-01 11952285.E-08
3010100 3010100 3030300
30101000.E-01-16733200.E-08
30303000.E-01 23421599.E-08-71713715.E-09
3030303 3030303 3030403
30303030.E-01 89642139.E-09
30304030.E-01-51754913.E-09 29880714.E-09

```

S-0 (D2)
 3 1 0 3 1 0 1 4 4 100
 3 1 0 -1.
 3 1 1 -0.5
 3 1 2 0.5
 3 3 2 -2.
 3 3 3
 -0.5
 3 3 4
 1.5
 1 0 0 -2.449489742
 1 2 2 1.449137674 -1.549193338
 1 4 4
 1.0
 B (D2)
 3 3 3 3 1 0 10000
 3 3 -8.
 3 1 7.
 1 4 4.
 1 2 -3.
 1 0
 14.
 C (D2)
 1 4 1 4 1 0 10000
 1 4 2.
 1 2 2.
 1 0 7.

PARAMETER TRANSFORMATIONS

$$\begin{bmatrix} \Delta \\ v \\ v' \end{bmatrix} = \begin{bmatrix} -0.15493704 & 0.37037037 & 0.0 \\ 0.26560636 & 0.22222222 & -0.35856868 \\ 0.09390603 & 0.07856742 & 0.16903085 \end{bmatrix} \begin{bmatrix} A_0^4 \\ A_3^4 \\ A_0^2 \end{bmatrix}$$

$$\begin{bmatrix} A_0^4 \\ A_3^4 \\ A_0^2 \end{bmatrix} = \begin{bmatrix} -1.6733200 & 1.5936381 & 3.3806170 \\ 2.0 & 0.66666666 & 1.41421356 \\ 0.0 & -1.1952286 & 3.3806170 \end{bmatrix} \begin{bmatrix} \Delta \\ v \\ v' \end{bmatrix}$$

APPENDIX FIVE
CELL THEORY PROGRAM

In a dense monatomic liquid neighbour atoms tend to pack together closely, which can result in short range order. A model utilising this is the cell model of the liquid state, which considers each atom as surrounded by twelve others in face-centred cubic coordination^{6.3}. No order of longer range than this is assumed. The forces acting between the atoms restrain the central atom into a definite volume, in which it is free to move in a potential well $\psi(\underline{r})$ due to the interatomic interactions. If the well is localised near the origin, the atom will have restricted movement, but if the well is wide, the atom can move throughout the whole of the volume inside the planes bisecting the distances between the origin and the nearest neighbour positions.

This freedom of movement can be expressed in terms of a quantity called the Free Volume v_f , defined as

$$v_f = \int e^{-\frac{\psi(\underline{r})}{kT}} d\tau$$

where the integral is taken over the whole dodecahedral cell, and the origin is taken as the zero of energy. If ψ remains small over the cell, the integral will approach the cell volume, if ψ increases sharply away from the origin v_f

will be decreased.

The theory is normally applied to liquids such as Argon, where the interatomic potential has the form

$$\phi(r) = \epsilon \left[\left(\frac{a}{r}\right)^{12} - 2\left(\frac{a}{r}\right)^6 \right]$$

and the energy term $\psi(x,y,z) = \sum_i [\phi_i(x,y,z) - \phi_i(0,0,0)]$, with i ranging over the neighbours. The two parameters can be absorbed by defining reduced temperature as kT/ϵ , and taking a as the unit of length. The variables in the model are then the reduced temperature and the cell volume.

The integration is performed from the centre outwards over a regular grid for $x,y,z > 0$, stopping when significance is lost or the limit of integration is reached. The derivative $w \frac{\partial \psi}{\partial w}$ is calculated at the same time. The two cases of twelve and eleven neighbours are considered together, for five temperatures. This sharing of arithmetic between 20 calculations results in considerable time saving.

Several sense switch options are available. If Sw 1 is turned on before calculation begins, x,y and z values are accepted and integrand values calculated for that point. This facility is useful for deciding what grid step to use. If Sw 1 is turned on during calculation, the values of the running sums are typed out. Sw 2 is used during integration to allow for the possibility that a

significant contribution to the integral may come from the region near $x=y$, which passes between atoms. If the switch is on, this region is tested for each integration along an x line. Sw 3 is used for input/output of a partial calculation. If the switch is turned on, intermediate output is punched, and can be reread later if Sw 3 is on at input time.

PROGRAM LISTINGS

Cell Theory Integration

```

*0810
C   FORTRAN 2 VERSION OF CELL THEORY
C   SPS APPENDIX TO ATTEMPT SPEEDING UP
C   FIVE TEMPERATURES IN ASCENDING ORDER
C
C   SW1  IF TURNED ON DURING CALCULATION GIVES PRESENT
C         VALUES OF SUMS AND CONTINUES
C   SW2  ON MID POINT SIGNIFICANCE CHECK
C   SW3  OFF SEGMENT INPUT, ON NORMAL INPUT
C         GIVES SEGOUT IF TURNED ON DURING CALCULATION
C   SW4  OFF NORMAL INPUT TYPE, ON CARDS
C
C   COMMON IXP1,IYM1,IXP2,IMX2,IX2,
1  IYP1,IYM1,IYP2,IYM2,IY2,IZPR,IZMR,IZ2,
2  S6T1,S6T2,S6T3,S6T4,S6T5,
3  S12T1,S12T2,S12T3,S12T4,S12T5
C   COMMON T1SA,T2SA,T3SA,T4SA,T5SA,
1  T1TWA,T2TWA,T3TWA,T4TWA,T5TWA,
2  T1SB,T2SB,T3SB,T4SB,T5SB,
3  T1TWB,T2TWB,T3TWB,T4TWB,T5TWB
C   COMMON T1SF,T2SF,T3SF,T4SF,T5SF,
1  T1TWF,T2TWF,T3TWF,T4TWF,T5TWF
C   WORKING VARIABLES
C   COMMON WEXP,WD,F10,LQ,LR
C   FINAL VALUES
C   COMMON S1F,S2F,S3F,S4F,S5F,
1  S1A,S2A,S3A,S4A,S5A,
2  S1B,S2B,S3B,S4B,S5B
C   COMMON SD1F,SD2F,SD3F,SD4F,SD5F,
1  SD1A,SD2A,SD3A,SD4A,SD5A,
2  SD1B,SD2B,SD3B,SD4B,SD5B
C   TEMPERATURES
C   COMMON T1,T2,T3,T4,T5
C   MORE WORKING VARIABLES
C   COMMON W,MP,MQ,MR,L,LP,
1MTR,MPS,IG,MBP,MBQ,MBR
C   EQUIVALENCE (IXP1,I)
C
1  IF(SENSE SWITCH 3)2,902
902 CALL SEGIN
GO TO 46
2  CALL INPUT
20 IF(SENSE SWITCH 1)801,6
6  ACCEPT 506,IG
C   FIND SQUARES OF DISTANCES
MBP=IG/2
MBQ=MBP
MBR=MBP
MR=MBR
43 WW=MR
MTR=WW*1.4142136-2.E+09
LR=1
IZ2=MR
CALL MULT(IZ2)
IZPR=MR+1414213562
CALL MULT(IZPR)
IZMR=MR-1414213562
CALL MULT(IZMR)
MQ=MBQ
42 L=1
MPS=0
LQ=1
IYP2=20000 00000+MQ
CALL MULT(IYP2)
IYP1=10000 00000+MQ
CALL MULT(IYP1)
IY2=MQ
CALL MULT(IY2)
IYM1=10000 00000-MQ
CALL MULT(IYM1)
IYM2=20000 00000-MQ
CALL MULT(IYM2)
MP=MBP
41 LP=1
IF(SENSE SWITCH 3)989,46
46 IXP2=20000 00000+MP
CALL MULT(IXP2)
IXP1=10000 00000+MP
CALL MULT(IXP1)
IX2=MP
CALL MULT(IX2)
IXM1=MP-10000 00000
CALL MULT(IXM1)
IXM2=MP-20000 00000
CALL MULT(IXM2)
C
CALL COORD
C
C   WE NOW HAVE 30 FG NUMBERS
C   26 CALL USE(T1TWF,T1SF,S1F,SD1F)
C   CALL USE(T2TWF,T2SF,S2F,SD2F)
C   CALL USE(T3TWF,T3SF,S3F,SD3F)
C   CALL USE(T4TWF,T4SF,S4F,SD4F)
C   CALL USE(T5TWF,T5SF,S5F,SD5F)
C   CALL USE(T1TWA,T1SA,S1A,SD1A)
C   CALL USE(T2TWA,T2SA,S2A,SD2A)
C   CALL USE(T3TWA,T3SA,S3A,SD3A)
C   CALL USE(T4TWA,T4SA,S4A,SD4A)
C   CALL USE(T5TWA,T5SA,S5A,SD5A)
C   CALL USE(T1TWB,T1SB,S1B,SD1B)
C   CALL USE(T2TWB,T2SB,S2B,SD2B)
C   CALL USE(T3TWB,T3SB,S3B,SD3B)
C   CALL USE(T4TWB,T4SB,S4B,SD4B)
C   CALL USE(T5TWB,T5SB,S5B,SD5B)
C   NEXT POINT
C   IF(SENSE SWITCH 1)899,12
12 IF(MP+IG+MQ+MTR)8,9,9
8 IF(MP-1000000000)13,9,9
C   LAST POINT ANY USE
13 GO TO (102,14),LP
14 GO TO (15,15,108),L
C
C   OUTSIDE LIMIT
9 GO TO (17,110,13 ),L
C
C   MID-PLANE ROUTINE
102 IF(SENSE SWITCH 2)109,17
109 GO TO (103,110,17),L
103 IF(MP-MQ)104,17,17
104 MPS=MP
IF(MQ+MQ+MTR)106,107,107
106 MP=MQ
L=7
GO TO 41
107 MP=MTR-MQ
L=3
GO TO 41
C   BACKSPACE ROUTINE
110 L=3
MP=MQ-IG
GO TO 41
C   CONTINUING
108 MP=MP-IG
IF(MP-MPS)17,17,41
C
C   INCREMENT MP
15 MP=MP+IG
GO TO 41
C   TEST AND INCREMENT MQ
17 GO TO (39,31),LQ
31 IF(MQ-1000000000)32,39,39
32 MQ=MQ+IG
GO TO 42
C   TEST AND INCREMENT MR
39 GO TO (701,38),LR
38 IF(MR-1414213562)37,701,701
37 MR=MR+IG
GO TO 43
701 CALL FNOUT
GO TO 1
801 CALL SEEK
GO TO 43
989 CALL SEGOUT
STOP
899 CALL FIND
C   INTEGRATING OR LOOKING
GO TO (12,898),I
898 IF(SENSE SWITCH 2)2,20
506 FORMAT(110)
END

```

*0810

```

SUBROUTINE INPUT
DIMENSION ID1(13),D2(32),T(5),S(10),ANS(30),M(3)
COMMON ID1,S,D2,W,M,I,LR,ANS,T,W,M,L,LC,MTR,MPS,IG
4 PRINT 573
ACCEPT 504,W,(T(1),I=1,5)
5 W=M*W/32.
DO 1 I=6,10
1 S(I)=1./(W*M*T(I-5))
W=M*W*M
DO 2 I=1,5
2 S(I)=1./(W*M*T(I))
PRINT 507
PAUSE
NOW INITIALISE
85 DO 101=1,30
101 ANS(I)=0.
IG=0.
RETURN
501 FORMAT(6F10.3)
503 FORMAT(7H,M,TEMPS)
504 FORMAT(F10.3)
507 FORMAT(7H$W3 OFF)
END

```

*0810

```

SUBROUTINE SFFK
DIMENSION ID1(96),ID2(5)
COMMON ID1,MR,ID2,MBP,MBQ
PRINT 508

P06 ACCEPT 506,MBP,MBQ,MR
R08 RETURN
506 FORMAT(110)
508 FORMAT(//SHY/Y/7)
513 FORMAT(3110)
END

```

*0810

```

SUBROUTINE FIND
TO TYPE OUT RUNNING SUMS IF SW 1 ON
DIMENSION ID1(55),S(5,6),T(5),ID2(4)
COMMON IRET,I,J,ID1,S,T,W,
1MP,MQ,MR,ID2,IG
PRINT 10,MP,MQ,MR,W
10 FORMAT(/4H X=10,4H Y=110,4H Z=110/21H=E14.7/
14H T 8X 11Y10 14H 11V1A 12X 2HVC)
DO 2 I=1,5
IF(SENSE SWITCH 1)2,3
2 PRINT 20,T(I),S(I,J),J=1,6)
3 IF(I)5,4,5
5 I RET=1
RETURN
4 I RET=2
PAUSE
DO 6 I=1,5
DO 6 J=1,6
6 S(I,J)=0.
RETURN
20 FORMAT(F6.3,3F15.7/6X,3E15.7)
END

```

*0810

```

SUBROUTINE USE (A,B,P,C)
DIMENSION D(52),OD(40)
COMMON IV,D,WEXP,WD,FID,LQ,LR,DD,L0
C ARGUMENTS IN COMMON SO NO FLAGS NEEDED
C ON PATCH INSTRUCTIONS
WEXP=2.*B-A
WD=A-B
IV=WEXP
C INTEGER VALUE OF EXPONENT
IV=-15-IV
C IF POSITIVE,EXP(-WEXP) INSIGNIFICANT
IF(IV)1,1,2
C NOW TEST WD TERM
C MM WD,23,10,EXPONENT ONLY
2 PAUSE 11111
C S IV,00098.,NOW READY TO TEST WD
PAUSE 11111
IF(IV)1,1,3
C ME OR BOTH USEFUL
1 LP=2
LQ=2
LR=2
FID=EYF(WEXP)
P=P+FID
C=C+WD*FID
RETURN
3 LP=1
RETURN
END

```

*0810

```

SUBROUTINE FIDHT
DIMENSION D1(38),F(5),A(5),B(5),FD(5),FA(5),FB(5),T(5),ID2(6)
DIMENSION VE(5),VF(5),DVE(5),DVF(5)
COMMON VF,VE,DVF,DVE,D1,F,A,B,FD,FA,FB,T,W,I,ID2,IG
EQUIVALENCE (GRIV,D1(35)),(GRIS,D1(37))
GRIV=IG/100
GRIS=GRIV/1000.000.
GRIV=GRIS*GRIS*GRIS*W*.176776695
IF(SENSE SWITCH 1) 703,702
702 PRINT 517,GRIS
PRINT 518,W
703 PUNCH 517,GRIS
PUNCH 518,W
DO 3 I=1,5
VF(I)=8.*GRIV*F(I)
VE(I)=4.*GRIV*(A(I)+R(I))
DVF(I)=VF(I)+32.*GRIV*FD(I)
1 DVE(I)=VE(I)+16.*GRIV*(FA(I)+FB(I))
IF(SENSE SWITCH 1)4,2
2 PRINT 519,T(I),VF(I),VE(I)
PRINT 520,DVF(I),DVE(I)
4 PUNCH 519,T(I),VF(I),VE(I),W,IG
3 PUNCH 521,T(I),DVF(I),DVE(I),W,IG
PAUSE
RETURN
517 FORMAT(11HGRID INCRT=F10.6)
518 FORMAT(21H=F10.6,7X,8HV12/DV12 10X,8HV11/DV11 )
519 FORMAT(2HT=F10.6,4X,E14.7,3X,E14.7,8X,E14.8,111)
520 FORMAT(16X,E14.7,3X,E14.7//)
521 FORMAT(2X,F10.6,4X,E14.7,3Y,E14.7,8X,E14.8,111)
END

```

*0810

```

SUBROUTINE SEGOUT
DIMENSION ID1(5),D1(30)
COMMON ID1,
11YP1,1YM1,1YP2,1YM2,1Y2,1ZPR,1ZMR,1Z2,
2S6T1,S6T2,S6T3,S6T4,S6T5,
3S12T1,S12T2,S12T3,S12T4,S12T5
COMMON D1
COMMON NSEK,1SWCH,D2,LQ,LR
C FINAL VALUES
COMMON 51F,S2F,S3F,S4F,55F,
1 S1A,S2A,S3A,S4A,55A,
2 S1B,S2B,S3B,S4B,55B,
COMMON SD1F,SD2F,SD3F,SD4F,SD5F,
1 SD1A,SD2A,SD3A,SD4A,SD5A,
2 SD1B,SD2B,SD3B,SD4B,SD5B
C TEMPERATURES
COMMON T1,T2,T3,T4,T5
C MORE WORKING VARIABLES
COMMON W,MP,MQ,MR,L,IP,
1MTR,MPS,IG,MBP,MBQ,MBR
NSEK=1
PUNCH 510, MP,MQ,MR,MTR,MPS,IG,NSEK
NSEK=2
PUNCH 510, 1Z2,1ZPR,1ZMR,1YP2,1YP1,1Y2,NSEK
NSEK=3
PUNCH 510,1YM1,1YM2,L,L,1Q,1R,NSEK
NSEK=4
PUNCH 509,S1F,S2F,S3F,S4F,55F,NSEK
NSEK=5
PUNCH 509,S1A,S2A,S3A,S4A,55A,NSEK
NSEK=6
PUNCH 509,S1B,S2B,S3B,S4B,55B,NSEK
NSEK=7
PUNCH 509,SD1F,SD2F,SD3F,SD4F,SD5F,NSEK
NSEK=8
PUNCH 509,SD1A,SD2A,SD3A,SD4A,SD5A,NSEK
NSEK=9
PUNCH 509,SD1B,SD2B,SD3B,SD4B,SD5B,NSEK
NSEK=10
PUNCH 509,S6T1,S6T2,S6T3,S6T4,S6T5,NSEK
NSEK=11
PUNCH 509,S12T1,S12T2,S12T3,S12T4,S12T5,NSEK
NSEK=12
PUNCH 509,T1,T2,T3,T4,T5,NSEK
IF(SENSE SWITCH 2)1,2
1 1SWCH=1
GO TO 3
2 1SWCH=2
3 NSEK=13
PUNCH 512,W,1SWCH,NSEK
STOP
509 FORMAT(5E14.8,110)
510 FORMAT(611,3X,111)
512 FORMAT(E14.8,6Y,110,29X,111)
END

```

```

*0910
SUBROUTINE BEGIN
DIMENSION ID1(5),D1(30)
COMMON ID1,
1 IYP1,IYM1,IYP2,IYM2,IY2,IZPR,IZMR,IZ2,
2 S6T1,S6T2,S6T3,S6T4,S6T5,
3 S12T1,S12T2,S12T3,S12T4,S12T5
COMMON D1
COMMON NSEK,ISWCH,D2,LQ,LR
C
C FINAL VALUES
COMMON S1F,S2F,S3F,S4F,S5F,
1 S1A,S2A,S3A,S4A,S5A,
2 S1B,S2B,S3B,S4B,S5B
COMMON SD1F,SD2F,SD3F,SD4F,SD5F,
1 SD1A,SD2A,SD3A,SD4A,SD5A,
2 SD1B,SD2B,SD3B,SD4B,SD5B
C
C TEMPERATURES
COMMON T1,T2,T3,T4,T5
C
C MORE WORKING VARIABLES
COMMON W,MP,MQ,MR,L,LP,
1 MTR,MPS,IG,MBP,MBQ,MBR
97 READ 510,MP,MQ,MR,MTR,MPS,IG,NSEK
MBP=IG/2
MBQ=MBP
MBR=MBP
IF(NSEK-1)99,1,99
1 READ 510,IZ2,IZPR,IZMR,IYP2,IYP1,IY2,NSEK
IF(NSEK-2)99,2,99
2 READ 510,IYM1,IYM2,L,LP,IQ,LR,NSEK
IF(NSEK-3)99,3,99
3 READ 509,S1F,S2F,S3F,S4F,S5F,NSEK
IF(NSEK-4)99,4,99
4 READ 509,S1A,S2A,S3A,S4A,S5A,NSEK
IF(NSEK-5)99,5,99
5 READ 509,S1B,S2B,S3B,S4B,S5B,NSEK
IF(NSEK-6)99,6,99
6 READ 509,SD1F,SD2F,SD3F,SD4F,SD5F,NSEK
IF(NSEK-7)99,7,99
7 READ 509,SD1A,SD2A,SD3A,SD4A,SD5A,NSEK
IF(NSEK-8)99,8,99
8 READ 509,SD1B,SD2B,SD3B,SD4B,SD5B,NSEK
IF(NSEK-9)99,9,99
9 READ 509,S6T1,S6T2,S6T3,S6T4,S6T5,NSEK
IF(NSEK-10)99,10,99
10 READ 509,S12T1,S12T2,S12T3,S12T4,S12T5,NSEK
IF(NSEK-11)99,11,99
11 READ 509,T1,T2,T3,T4,T5,NSEK
IF(NSEK-12)99,12,99
12 READ 512,W,ISWCH,NSEK
IF(NSEK-13)99,13,99
99 PRINT 514
PAUSE
GO TO 97
13 GO TO (14,15),ISWCH
14 PRINT 516
98 PAUSE
RETURN
15 PRINT 515
GO TO 98
509 FORMAT(5E14.8,110)
510 FORMAT(6I11,3X,111)
512 FORMAT(F14.8,6X,110,39X,111)
514 FORMAT(20HCARD OUT OF SEQUENCE)
515 FORMAT(17HPRG SWITCHES OFF)
516 FORMAT(16HSW2 ON, REST OFF)
END

```

```

*0810
SUBROUTINE MULT(NUM)
FOR SQUARING TEN-FIGURE NUMBERS
C
C PAUSE
C Object deck
C PAUSE
C altered
C M NUM,NUM,0126711
C SF 00081,,SIZE OF NUMBER LIMITED
C TF NUM,00090,026
C
C RETURN
C
C END

```

```

*0810
SUBROUTINE CORD
PAUSE
RETURN
END

```

Header cards added to
following SPS program

```

01010 * APPENDIX WRITTEN AS SIMULATED
01020 * FORTRAN SUBROUTINE 18/7/64
01030 *
01040 * DISTANCE FINDING
01050 DORG 12050
01060 INIT AM INIT-1,1,0210
01065 TF RS6,ZERO-3,0127
01070 TF RS12,ZERO,0127
01080 FIRST TF L6,ZERO-4,0127
01090 A L6,XP1,02
01100 A L6,YP1,02
01110 A L6,ZPR,02
01120 BTM RECIP,*+12,0127
01130 TWO TF L6,ZERO-4,0127
01140 A L6,XP1,02
01150 A L6,YP1,02
01160 A L6,ZMR,02
01170 BTM RECIP,*+12,0127
01180 THREE TF L6,ZERO-4,0127
01190 A L6,XP1,02
01200 A L6,YM1,02
01210 A L6,ZPR,02
01220 BTM RECIP,*+12,0127
01230 FOUR TF L6,ZERO-4,0127
01240 A L6,XP1,02
01250 A L6,YM1,02
01260 A L6,ZMR,02
01270 BTM RECIP,*+12,0127
01280 FIVE TF L6,ZERO-4,0127
01290 A L6,XM1,02
01300 A L6,YP1,02
01310 A L6,ZPR,02
01320 BTM RECIP,*+12,0127
01330 SIX TF L6,ZERO-4,0127
01340 A L6,XM1,02
01350 A L6,YP1,02
01360 A L6,ZMR,02
01370 BTM RECIP,*+12,0127
01380 SEVEN TF L6,ZERO-4,0127
01390 A L6,XM1,02
01400 A L6,YM1,02
01410 A L6,ZPR,02
01420 BTM RECIP,*+12,0127
01430 EIGHT TF L6,ZERO-4,0127
01440 A L6,XM1,02
01450 A L6,YM1,02
01460 A L6,ZMR,02
01470 BTM RECIP,*+12,0127
01480 NINE TF L6,ZERO-4,0127
01490 A L6,Y2,02
01500 A L6,YP2,02
01510 A L6,Z2,02
01520 BTM RECIP,*+12,0127
01530 TEN TF L6,ZERO-4,0127
01540 A L6,Y2,02
01550 A L6,YM2,02
01560 A L6,Z2,02
01570 BTM RECIP,*+12,0127
01580 * ZEROAT ORIGIN FOR ELEVEN
01590 S RS6,06,0127
01600 S RS12,012,0127
01610 * SAVE SUMS
01620 TF R10,RS6,0127
01630 TF T10,RS12,0127
01640 TF L6,ZERO-4,0127
01650 ELEVA A L6,XP2,02
01660 A L6,Y2,02
01670 A L6,Z2,02
01680 BTM RECIP,*+12,0127
01690 * NOW FLOAT
01700 TFH FLOAT+23,39767,027
01710 BTM FLOAT,*+12,0127
01720 ELEV TF L6,ZERO-4,0127
01730 TF RS6,R10,0127
01740 TF RS12,T10,0127
01750 A L6,XM2,02
01760 A L6,Y2,02
01770 A L6,Z2,02
01780 BTM RECIP,*+12,0127
01790 * SAVE SUMS AGAIN
01800 TF R10,RS6,0127
01810 TF T10,RS12,0127
01820 * FLOAT NEW SUMS
01830 TFH FLOAT+23,39667,027
01840 BTM FLOAT,*+12,0127
01850 TF RS6,R10,0127
01860 TF RS12,T10,0127
01870 * ZEROAT ORIGIN FOR TWELVE
01880 S RS6,06,0127
01890 S RS12,C12,0127
01900 TF L6,ZERO-4,0127
01910 TWELVE A L6,XP2,02
01920 A L6,Y2,02
01930 A L6,Z2,02
01940 BTM RECIP,*+12,0127
01950 * FLOAT LAST SET
01960 TFH FLOAT+23,39517,027
01970 BTM FLOAT,*+12,0127
01980 * NOW FINISHED, RETURN
01990 PETURN B INIT-1,,026
02000 *
02010 *
02020 *
02030 *
02040 *
02050 *

```

```

05010 *
05020 *
05030 *
05040 XP1 DS ,39999
05050 XM1 DS ,39989
05060 XP2 DS ,39979
05070 XM2 DS ,39969
05080 X2 DS ,39959
05090 YP1 DS ,39949
05100 YM1 DS ,39939
05110 YP2 DS ,39929
05120 YM2 DS ,39919
05130 Y2 DS ,39909
05140 ZPR DS ,39899
05150 ZMR DS ,39889
05160 Z2 DS ,39879
05170 ZERO DC 15,0
05180 DC 1,0
05190 RS6 DS 12
05200 DC 1,0
05210 RS12 DS 15
05220 DC 1,0
05230 L6 DS 11
05240 DC 1,0
05250 R10 DS 12
06010 T10 DS 15
06020 ST06 DS 12
06030 ST012 DS 15
06040 ONE DC 10 , 1000000000
06050 C6 DC 9 , 156250000
06060 O6 DC 10 , 1718750000
06070 C12 DC 10 , 2441406250
06080 D12 DC 11 , 26855468750
06090 WORK DS 11
06100 SPACE DS 5
06110 * ROOM FOR Q OF BTM
06120 *
06130 *
07010 *
07020 *
07030 RECIP RD R1 , L6-10,0127
07040 BD R2 , L6-9,0127
07050 TR L6-10,L6-9,0127
07060 * POSITION NUMBERS FOR DIVISION
07070 TDM L6 , 0,02
07080 B R2,,02
07090 R1 TF L6 , L6-1 ,0127
07100 R2 SF L6-9 , ,02
07110 * NOW TEN SIG FIGS
07120 TF 00079,ZERO,17,CLEAR DIV AREA
07130 LD 00089, ONE,17
07140 D 00088, L6 ,17
07150 BD FLUKE,0079,02
07160 SF 00080
07170 TF L6, 00089 ,02,TEN SIG FIG
07180 M L6 , L6 ,0127
07190 TF WORK,00089,02
07200 M L6 , WORK ,0127
07210 BD R3 , L6-10,0127
07220 BNF R4 , L6-10,0127
07230 TF ST06,00089,02
07240 RR M ST06, ST06,0127
07250 A RS12,00092,02
08010 RRR A RS6, ST06 ,0127
08020 B RECIP-1 ,026
08030 R3 TF ST06,00086,02
08040 B RR , ,02
08050 R4 SF 00082
08060 BO 142,81
08070 TF ST06,00092,02
08075 B 00079,ZERO-8,127
08080 B RR , ,02
08090 FLUKE BNF ST0P,L6-10,0127
08100 BD FT , L6-10,0127
08110 TF ST06-1,ONE,0127
08120 TDM ST06 , 0,02
08130 TF ST012,ONE-5,0127
08140 TF ST012-4,ONE,0127
08150 A RS12,ST012,0127
08160 B RRR , ,02
08170 STOP H
08180 B *-12 , ,02
08181 FT TF ST06,ONE-2,0127
08182 A RS12,ONE-2,0127
08183 B RRP , ,02
08190 *

```

STORAGE ALLOCATION

```

08200 *
08210 FLOAT TFM X , 2 ,0210
08220 X DS ,*-2
08230 TFM BACK , ,02
08240 TFM EXT,RS6-11,0127
08250 MF SAFLAG,RS6,0127
09010 BTM F1 , 39867,027
09020 TFM X , 2 ,0210
09030 SM FLOAT+23,50,027
09040 TFM EXT,RS12-14,0127
09050 TF BACK,FLOAT+23,0127
09060 MF SAFLAG,RS12,0127
09070 BTM F1 , 39817,027
09080 B FLOAT-1 , ,026
09090 F1 TF LIM, F1-1 ,0127
09100 SM LIM , 50 ,027
09110 TF ADTOP,EYT ,0127
09120 * FINDFIRST DIGIT
09130 SETB BD SET , EXT ,012711
09140 AM EXT , 1 ,0210
09150 SM X , 1 ,0210
09160 B SFTB , ,02
09170 LIM DS ,*
09180 SET TF ADB , EYT ,0127
09190 BNR *-24, ADB ,012711
09200 B LOW , ,02
09210 ADTOP DS ,*
09220 CLEAR DS ,ZERO-7
09230 AM ADB , ,0210
09240 B SET+12 , ,02
09250 ADB DS ,*
10010 LOW S ADB , EXT ,0127,NO OF DIGITS
10020 TR ADTOP,EXT ,0126711
10030 CM ADB , 8 ,027
10040 BNN NOT NES ,02
10050 TFM CLR, CLEAR,0127
10060 A CLR , ADB ,0127
10070 TF CLRD,ADTOP,0127
10080 A CLRD , ADB ,0127
10090 TR
10100 CLR DS ,*
10110 CLRD DS ,*-5
10120 NOTNES SF ADTOP , ,026
10130 BACK DS ,*
10140 SAFLAG DS ,NOTNES
10150 TF EXT, ADTOP,0127
10160 AM EXT , 7 ,0210
10170 MF EXT,SAFLAG,01267
10180 * NOW HAVE FLAGGED AND
10190 * SIGNED MANTISSA
10200 F2 M F1-1, EXT ,0126711
10210 AM F1-1 , 2 ,027,MULT EXPT ADDRESS
10220 TF EXS , ,0127
10230 A EXS, F1-1 ,012711
10240 BD SETOUT, 84,02
10250 SM EXS , 1 ,0210
11010 SF 00085
11020 TF BACK,00092,076
11030 B SETOUT+12,,02
11040 EXT DS ,*
11050 SETOUT TF BACK,00091,026
11060 AM BACK , 2 ,0210,PRODUCT EXPT ADR.
11070 EXS DS ,*-2
11080 TF BACK, EXS ,01267
11090 SM F1-1 , 12 ,0210
11100 SM BACK , 12 ,0210
11110 C F1-1, LIM ,0127
11120 BHZ F2 , ,02
11130 BB
11140 *
11150 * TO SIMULATE SUBROUTINE,REMOVE LOADER
11160 * AND TRAILER, REPLACE BY HEADER AND
11170 * TRAILER CARDS
11190 DEND

```

*111112.14 ABSORBANCE PROGRAM

*0505

C PROGRAM TO SUBTRACT BACKGROUND
C FROM INPUT SPECTRUM
C COMMENCED 6/11/64
C FINISHED 25/11/64
C

```

      IF(SENSE SWITCH 9)1,1
      PRINT 101
101  FORMAT(26HENTER CARDS FOR BACKGROUND)
      DIMENSION DATA(1000),Y(5),W LGTH(5)
      COMMON DATA
      EQUIVALENCE (DATA(2),W LGTH(2),Y(1))
      STORE EACH Y DIRECTLY ABOVE ITS X
      K=1
      READ ORDER,INITL AND FINAL COUNTER READINGS,
      DRIFT, AND X VALUES
      5  READ 102,N ORDER,N FIRST,X FIRST,DRIFT F,
      IN LAST,X LAST,DRIFT L
102  FORMAT(15,2(15,2E10.0))
      FIRST=N FIRST/N ORDER
      F LAST=N LAST/N ORDER
      SCALE=(F LAST-FIRST)/(X LAST-X FIRST)
      DRIFT=(DRIFT L-DRIFT F)/(X LAST-X FIRST)
      GO TO (4,6),K
      4  DO 2 I=1,1000,2
      READ 201,XX,YY
      201  FORMAT(2E10.0)
      REDUCE XX TO WAVELENGTH
      W LGTH(1)=FIRST+SCALE*(XX-X FIRST)
      REMOVE DRIFT FROM Y
      Y(1)=YY+DRIFT*(XX-X FIRST)+DRIFT F
      C FINISHED THE DATA
      IF(SENSE SWITCH 9)3,2
      2  CONTINUE
      C FULL STORAGE
      PRINT 202
      202  FORMAT(35HDATA STORAGE FULL,RUN OUT ALL CARDS)
      C SET MAXIMUM
      I=999
      C NOW READ SPECTRUM
      3  PRINT 301
      301  FORMAT(19HREAD SPECTRUM CARDS)
      PAUSE
      K=2
      GO TO 5
      C NOW READ X AND Y VALUES,INTERPOLATE,
      C AND PUNCH OUTPUT
      C
      6  READ 201,X,YY
      SPECT=YY+DRIFT F+DRIFT*(X-X FIRST)
      X=FIRST+SCALE*(X-X FIRST)
      N TREC=1
      DIMENSION TERPOL(8),TX(4),TY(4)
      EQUIVALENCE (TO,TERPOL(1),TX(1),TY(0))
      C
      7  CALL T REC(TO,DATA(N TREC),8)
      C AN SPS TRANSMIT RECORD SUBROUTINE
      C TO SHIFT ARRAYS
      C
      FIND PARAMETERS WANTED FOR
      DIVIDED DIFFERENCES INTERPOLATION
      EQUIVALENCE (X1,TX(1)),(X2,TX(3)),(X3,TX(5)),(X4,TX(7))
      A=(TY(3)-TY(1))/(X2-X1)
      B=(TY(5)-TY(3))/(X3-X2)
      C=(TY(7)-TY(5))/(X4-X3)
      A=(B-A)/(X3-X1)
      B=(C-B)/(X4-X2)
      A=(B-A)/(X4-X1)
      D=TY(7)
      C
      LOCATE POINT IN TREC
      15  IF((X-X3)*(X LAST-X FIRST))8,9,10
      C REACHED TOP OF DATA
      10  IF(1-7-N TREC)8,8,11
      11  N TREC=N TREC+2
      GO TO 7
      9  DIV=TY(5)
      GO TO 12
      C DO INTERPOLATION
      8  DIV=D+(X-X4)*(C+(Y-X3)*(B+(X-X2)*A))
      C NOW WANT DIV/SPEC AS FN OF X
      12  TRANS=DIV/SPECT
      ABSN=LOGF(TRANS)
      U BAR=1.E+8/X
      CALL PUNCH(X, ABSN,1,UBAR,ABSN,2)
      C
      ANY MORE DATA
      IF(SENSE SWITCH 9)14,13
      13  READ 201,X,YY
      SPECT=YY+DRIFT F+DRIFT*(X-X FIRST)
      X=FIRST+SCALE*(X-X FIRST)
      GO TO 15
      C
      14  FINISHED
      C PAUSE
      GO TO 1
      C END

```

ABSORBANCE PROGRAM 1

```

*0505 SUBROUTINE PUNCH(A,B,L,C,D,J)
      K=1(0)
      PUNCH 1,A,B,L,K,C,D,J,K
      RETURN
      1  FORMAT(2E10.4,4OX,15,1OX,15)
      C SEPARATE ON COLUMN 65
      END

```

```

*0505 FUNCTION I(K)
      K=K+1
      I=K
      RETURN
      END

```

```

*0505 SUBROUTINE T REC(TO,FROM,NUMBER)
      RETURN
      END

```

LINKAGE CARDS ON FOLLOWING DECK

```

01010*      TREC A FORTRAN SUBPROGRAM
01020*      T.A.BROWN
01030      DC 1,2
01040      DC 1,3
01050      DC 1,4
01060      DC 1,5
02120START OS ,11258
01070      OORGSTART
01080      BV *+12,,0,TURN OFF O/FLOW IF NECESSARY
01090      TF LENGTH,K,0,INITIALISE IF FIXED
01100      SM A, 0, 0'6 8,SEE IF FIXED OR FLOATING
01110      BNW REST,, 0 ,O/FLO IF FLOATING
01120      BT REST,FP2,0,INITIALISE FOR FLOATING
01130ERROR OAC 9,TREC ERR*
01131ABOVE C B,00099,0
01132      BNN OKAY,,0
01133      RCTY
01134      WATYERROR,,0
01135      H
01136      B *-12,,0
01136LENGTHDS *
01140REST S A,LENGTH,0 1,RECORD POSITION
01150      S B,LENGTH,0 1
01160      M H,LENGTH,0 1 6,RECORD LENGTH
01170      A 99,A,1
01171*      TEST FOR OVERWRITING OF *
01172      C B,A, 0 1
01173      BP ABOVE,,0
01180DKAY TO BACK,99,0 11,SAVE LAST DIGIT
01190      TO 99,FAC+1, 6,MAKE RECORD
01200      AM A,1,0 10
01210      AM B,1,0 10
01220      TR B,A, 0 1 6 11, SHIFT
01230      TOM 99,,6,SHIFT LAST DIGIT BACK
01240BACK OS *
01250      A 99,B,1,PREPARE TO PUT LAST DIGIT
01260      S 99,A,1,ON END OF SHIFTED RECORD
02010      TO 99,BACK, 1 6
02020      B RETN AD,,0 6,RETURN
02030*
02040*      ADDRESSES USED
02050*
02060A      OS ,11048
02070B      OS ,11053
02080M      OS ,11058
02090FP2     OS ,05253
02100FAC     OS ,00485
02110RETNAD  OS ,11065
02130K       OS ,00404
02140      DEND

```

```

**11 12.14 WAVELENGTH TO WAVENUMBER WITH BACKGROUND REMOVED
*0605
C READ BACKGROUND AND SPECTRUM DECKS IN PACKED FORMAT,
C PUNCH DECK FOR A VERSUS WAVE NUMBER
C DIMENSION LAMBOA(1000),K ABS(1000),LENGTH(2),KODE(5),KODE 2(5)
C READ A HEADER CARD, TYPE N, C, OR B
C
999 READ 1,KODE
1 FORMAT(70H
1
25A2)
C
C PRINT 1,KODE
C
C SET SWITCH FOR BACKGROUND FOR SPECTRUM
C MN OR PL=1
C IF(KODE(1)/1000-42)3,2,3
C MN OR PL=1
3
C READ BATCH
C CALL INPUT(LAMBOA,K ABS,LENGTH(1))
C
C SORTING OPTION
C CALL SORT(LAMBOA,K ABS,LENGTH(1))
C
C READ SECOND HEADER
C READ 40,KODE 2
40 FORMAT(70H
1
25A2)
C
C PRINT 40,KODE 2
C
C PUT SECOND BATCH AFTER FIRST
C EQUIVALENCE (LOAD,LENGTH(1)),(MAX NU,MIN L),(MIN NU,MAX L)
C
C CALL INPUT(LAMBOA(LOAD),K ABS(LOAD),LENGTH(2))
C CALL SORT(LAMBOA(LOAD),K ABS(LOAD),LENGTH(2))
C
C STORE MAX AND MIN VALUES
C MIN L=LAMBOA(LOAD+1)
C IF(LAMBOA(1)-MIN L)41,42,42
C MIN L=LAMBOA(1)
C L=LENGTH(1)+LENGTH(2)
C MAX L=LAMBOA(LOAD)
C IF(LAMBOA(L)-MAX L)44,44,43
C MAX L=LAMBOA(L)
C43
C44 FLOAT=MAX L
C MIN NU=1.E+8/FLOAT
C FLOAT=MIN L
C MAX NU=1.E+8/FLOAT
C IF(SENSE SWITCH 3)52,51
C51 PRINT 50
C50 FORMAT(25HSTART/FINISH/STEP WAVE NO)
C52 ACCEPT 520,NU,NU FIN,INCRMT
C520 FORMAT(E12.5)
C EQUIVALENCE (K,NU FIN)
C
C IF(INCRT)528,527,528
C IF INCRMT IS ZERO, USE SAME POINTS FOR OUTPUT
C
C TEST LIMITS
C528 IF(NU-MIN NU)522,521,521
C521 IF(NU FIN-MAX NU)527,527,522
C522 PRINT 523,MIN NU,MAX NU
C523 FORMAT(7HLIMITS 15,3H - 15)
C
C OPTIONS CARRY ON, NEW TYPING, OR NEW START
C IF(SENSE SWITCH 3)526,524
C524 PRINT 525
C525 FORMAT(19H$W2 OFF TO CARRY ON)
C526 PAUSE
C IF(SENSE SWITCH 2)7,527
C
C DUPLICATE HEADER
C527 IF(MN OR PL)53,54,54
C53 PUNCH 40,KODE 2
C DO 531,1=1,5
C531 KODE(1)=KODE 2(1)
C GO TO 55
C54 PUNCH 1,KODE
C
C WILL PUNCH KODE AND A SEQUENCE NUMBER ON EACH CARD
C
C NO SEQ=0
C55 J=9999
C IF(INCRT)60,56,60
C IF(MN OR PL)57,57,58
C56 J=L
C57 K=LENGTH(1)
C GO TO 59
C58 J=LENGTH(1)
C K=0
C59 NU=LAMBOA(J)

```

ABSORBANCE PROGRAM 2

```

C DIMENSION KARD(18)
C EQUIVALENCE (KARD,KODE 2),(KARD(13),KODE(1)),(KARD(18),NO SEQ)
C
C LOOP TO PUNCH CARDS
C
C60 DO 61 1=1,12
C61 KARD(1)=0
C NO SEQ=NO SEQ+1
C DO 62 1=1,11,2
C KARD(1)=NU
C FLOAT=NU
C LAM INT=1.E+8/FLOAT
C IF(INCRT)614,613,614
C613 KARD(1)=LAM INT
C LAM INT=LAMBOA(J)
C614 CONTINUE
C COMMON LAM INT,INT VAL
C CALL INTERP(LAMBOA,K ABS,LENGTH(1))
C KEEP=INT VAL
C CALL INTERP(LAMBOA(LOAD),K ABS(LOAD),LENGTH(2))
C KARD(1+1)=MN OR PL*(KEEP-INT VAL)
C IF(SENSE SWITCH 1)617,618
C FOR TRANSMITTANCE DATA
C617 FLOAT=KEEP
C SINK=INT VAL
C FLOAT=SINK/FLOAT
C SINK=MN OR PL
C KARD(1+1)=0.4343*SINK*LOGF(FLOAT)
C
C INCREMENT AND TEST
C618 IF(INCRT)619,611,619
C611 J=J-1
C612 IF(J-K)63,63,612
C NU=LAMBOA(J)
C GO TO 62
C619 NU=NU+INCRMT
C IF(NU-MIN NU)62,62,63
C62 CONTINUE
C
C FINISHED CARD, PUNCH IT
C63 PUNCH 630,KARD
C630 FORMAT(12I5,5A2,5X,15)
C
C SEE IF MORE CARDS WANTED
C IF(J-K)631,7,60
C631 IF(NU-MIN NU)60,60,7
C
C IF(SENSE SWITCH 3)8,71
C71 PRINT 70
C70 FORMAT(24H$W2 ON TO READ NEW CARDS )
C PAUSE
C8 IF(SENSE SWITCH 2)999,49
C END

```

**11 12.14 READ SPECTRUM

```
*0605
      SUBROUTINE INPUT(I,J,NUMBER)
      L=1
      DIMENSION I(20),J(20)
      IF(SENSE SWITCH 9)2,2
2     LPSX=L+6
      READ 20,(I(K),J(K),K=L,LPSX)
20    FORMAT(14I5)
      DO 21 K=L,7
      C
      C     TEST TO SEE IF I VALUES NON-ZERO
      C
      IF(I(L))22,1,22
22    L=L+1
21    CONTINUE
      IF(SENSE SWITCH 9)9,2
      C
      C     NUMBER=L-1
      C     RETURN
      C     END
```

**11 12.14 SORT TWO VECTORS SO ONE IN INCREASING ORDER

```
*0605
      SUBROUTINE SORT(IX,IY,N)
      C     METHOD OF SHELL
      C     DIMENSION IX(20),IY(20)
      C
      M=N
      M=M/2
      IF(M)30,40,30
30    K=N-M
      J=1
41    I=J
49    L=I+M
      IF(IX(I)-IX(L))60,60,50
50    MOVE=IX(I)
      IX(I)=IX(L)
      IX(L)=MOVE
      MOVE=IY(I)
      IY(I)=IY(L)
      IY(L)=MOVE
      C
      I=I-M
      IF(I-1)60,49,49
60    J=J+1
      IF(J-K)41,41,20
40    RETURN
      C     ENO
```

**11 12.14 THPO ORDER INTERPOLATION

```
*0605
      SUBROUTINE INTERP(I VEC,J VEC,LENGTH)
      DIMENSION I VEC(20), J VEC(20)
      C     ARRAYS I VEC,J VEC,I VEC IN INCREASING ORDER
      C     WANT J(I)
      C
      COMMON I,INT VAL
      MIN=2
      MAX=LENGTH-1
13    MIDDLE=(MAX+MIN)/2
      C
      C     MIN AND MAX CLOSE TOGETHER
      C     IF(MIDDLE-MIN)1,2,1
      C
      C     WHERE IN INTERVAL IS X
      C     IF(I-I VEC(MIDDLE))11,20,12
      C
11    MAX=MIDDLE
      GO TO 13
12    MIN=MIDDLE
      GO TO 13
      C
      C     FOUND EXACT PLACE
      C     INT VAL=J VEC(MIDDLE)
      C     RETURN
      C
      C     HAVE NOW FOUND POINTS SURROUNDING I
      C     OR AT END OF RANGE
      C
2    X1=I VEC(MIN-1)
      X2=I VEC(MIN)
      X3=I VEC(MIN+1)
      X4=I VEC(MIN+2)
      Y2=J VEC(MIN)
      Y3=J VEC(MIN+1)
      Y4=J VEC(MIN+2)
      Y1=J VEC(MIN-1)
      A=(Y2-Y1)/(X2-X1)
      B=(Y3-Y2)/(X3-X2)
      C=(Y4-Y3)/(X4-X3)
      A=(B-A)/(X3-X1)
      B=(C-B)/(X4-X2)
      A=(B-A)/(X4-X1)
      X=1
      INT VAL=Y4+(X-X4)*(C+(X-X3)*(B+(X-X2)*A))
      C
      C     RETURN
      C
      C     FMD
```


FIT GAUSS OR LORENTZ LINES TO SPECTRUM

**11 12.14 SPECTRAL LINE OPTIMISATION PROGRAM

*0605

C METHOD OF STONE, JOSA 52.9, 992, (1962)
C MODIFICATION OF ANDERSON OF MOD OF BLOOM

C
C DIMENSION G(33),H(33),TH(33),THA(33),
1X(96),Y(96),W(96),T(96),LTY(10),
2A(96,10),B(96,10)

C
98 READ 3,M,N P,LTY,NB,N1,GQ,STOP
3 FORMAT(12,13,1112,13,2E10.4)
3 NO BANOS, NO POINTS, TYPE FOR BANOS(+GAUSS,-LORENTZ)
C NO BACKGROUND TERMS, MAX NO ITERATIONS
C STOPPING VALUE FOR MODULUS OF GRADIENT VECTOR
C SMALLEST Y VALUE FOR CONSIDERING LINES

C SET SOME VALUES

C N=3*M+3
C FLNP=N
C N IT=0
C FL=1.0E+20
C TAU=1.
C IT=0
C FL START=4-N B
C FL N=N

C READ DECREASING ORDER COEFFICIENTS OF BACKGROUND QUADRATIC,
C THEN INTENSITY, POSITION, WIDTH OF TRIAL BANOS
C THEN DATA HEADER, THEN DATA

C READ 6,(TH(1),I=1,N)
C READ 4,(X(1),Y(1),I=1,N P)

4 FORMAT(20H
1/(1215))

PRINT 4

PRINT 5

5 FORMAT(38HINTENSITY

DG 94 J=1,N

94 THA(J)=TH(J)

H(3)=FLNP

H(2)=0.

H(1)=0.

DO 107 I=1,N P

X SQD=X(1)**2

H(2)=H(2)+X SQD

H(1)=H(1)+X SQD*X SQD

107 W(1)=X SQD

C
C MAIN LOOP BEGINS HERE

103 PRINT 100

10J FORMAT(/)

PRINT 6,(TH(1),I=1,N)

FORMAT(E12.4,2E14.4)

C
C DOUBLE LOOP TO STORE EXPECTED SPECTRUM

C
C F=0.
C DO 20 I=1,N P
C T OF I=Y(1)-TH(3)-X(1)*TH(2)-W(1)*TH(1)
C DO 200 J=4,N,3
C K=J/3
C A OF IJ=(X(1)-TH(J+1))/TH(J+2)
C AB=A OF IJ*A OF IJ

C
C WHICH SORT OF LINE
C IF(LTY(K))350,351,351

C
C GAUSSIAN, TEST IF BEYOND WINGS

351 IF(AB-15.0)251,250,250

250 B OF IJ=0.

GO TO 200

251 B OF IJ=EXP(-AB)

GO TO 83

350 B OF IJ=1.0/(1.0+AB)

83 T OF I=T OF I-TH(J)*B OF IJ

A(I,K)=A OF IJ

200 B(I,K)=B OF IJ

C
C NOW TIDY UP FOR GIVEN POINT

F=F+T OF I

T(I)=T OF I

IF(FL=F)201,201,202

201 TAU=0.5*TAU

IT=0

GO TO 95

202 FL=F

DO 204 J=N START,N

204 THA(J)=TH(J)

IT=IT+1

IF(4-IT)205,205,206

205 TAU=2.0*TAU

IT=0

C
C
C NOW FURTHER BIG LOOP FOR GRADIENT VECTOR

206 DO 24 J=4,N,3

K=J/3

GJ=0.

HJ=0.

GJ1=0.

HJ1=0.

GJ2=0.

HJ2=0.

AB=TH(J)

E=2.0*AB/TH(J+2)

DO 86 I=1,N P

B OF IJ=B(I,K)

C ANY USE

IF(B OF IJ*AB-STOP)86,86,85

85 T OF I=T(I)

GJ=GJ+T OF I*B OF IJ

B SQRO=B OF IJ*B OF IJ

HJ=HJ+B SQRO

A OF IJ=A(I,K)

E A B2=E*A OF IJ*B SQRO

E2 A2 B4=E A B7=E A B2

E T A B2=T OF I*E A B2

C
C GJ1=GJ1+E T A B2

HJ1=HJ1+E2 A2 B4

GJ2=GJ2+E T A B2*A OF IJ

HJ2=HJ2+E2 A2 B4*A OF IJ*A OF IJ

86 CONTINUE

C(J)=GJ

H(J)=HJ

G(J+1)=GJ1

H(J+1)=HJ1

G(J+2)=GJ2

H(J+2)=HJ2

24 G(1)=0.

G(2)=0.

G(3)=0.

IF(NB)71,71,300

DO 70 I=1,N P

300 T OF I=T(I)

G(3)=G(3)+T OF I

G(2)=G(2)+T OF I*X(I)

G(1)=G(1)+T OF I*W(I)

70
C

71 IF(SENSE SWITCH 2)73,72

72 PRINT 11

11 FORMAT(8HGRADIENT)

PRINT 6,(G(J),J=1,N)

PRINT 13

13 FORMAT(11HINFORMATION)

PRINT 6,(H(J),J=1,N)

73 GQT=0.

DO 30 J=N START,N

30 GQT=GQT+G(J)**2

N IT=N IT+1

PRINT 7,GQT,F,N IT,TAU

7 FORMAT(4HGQT=E12.4,7H

16H

IF(N1)97,97,96

96 IF(N IT-N1)97,32,32

97 IF(GQT-GQ)32,32,31

310 IF(SENSE SWITCH 1)32,31

32 VAR=F/(FLNP-FLN)

PUNCH 6,(TH(1),I=1,N)

PUNCH 4

PRINT 8,VAR

8 FORMAT(10HVARANCE=E10.4)

PUNCH 14,(X(1),T(1),Y(1),I=1,N P)

14 FORMAT(3E10.4)

GO TO 98

C
C MODIFY VECTOR FOR NEXT TRY

C
C

31 DO 25 J=N START,N

25 TH(J)=THA(J)+TAU*G(J)/H(J)

GO TO 103

C
C

ENO

THIS PROGRAM COMPARES INTEGER DIFFERENCES OF WAVE NUMBERS
THIS IS A VERY MESSILY WRITTEN PROGRAM

LOOK FOR SIMILAR SPACINGS IN AN ENERGY TABLE

```
01010START RCTY
01020 WATYHEAD1
01021 RCTY
01023 RCTY
01024 WATYHEAD3
01025 RCTY
01026 SAYTABWATYTAB
01027 H
01028STARPIAM =1,25,10,INCREMENT COUNTER
01029 BD SAY TAB,STAR P 1-2
```

CONNECTION BETWEEN ROUTINES *

```
01030BEGIN RCTY
01040 WATYNUM STT
01050 TF SUB+42,*+23
01060 B SUB,SRCH1,7
01070SORTF RCTY
01080 WATYSM1
01085 H
01090 BNC1HUNT
01100 B SEARCHM
01110SRCHF RCTY
01120 WATYSW2
01125 H
01130 BNC2BEGIN
01140 B SORTF
01150SUB PNTYREAD-79
01160 SF READ-79
01170 BC4 SUB
01180 B
01190HUNTF TF ADIT,ADOUT
01191SUPPR BD TYPE,ADIT,11
01192HOP AM ADIT,1,10
01193 AM ADIT,1,10
01194 B HOP
01195TYPE WNTY-ADIT
01196 B SUPPR-1,*6
```

SORTING OF INPUT VALUES *

```
02010SORT TFM AD IN,READ-80
02015 TFM SET FLC,READ-80
02020 A SET FLC,READ-78
02025 TFM ACC,1,10
02027 S ACC,READ-78
02028 WATYNUM STP
02029 TF SUB+42,*+23
02030 B SUB,*+12,7
02031 A ACC,READ-78
02032 A AD IN,READ-78
02033 CF TOP ST
02034 TFM DIFF+34,ACC
02035 TFM MAX,0,10
02036 TD ARRAY,REC
02037 TFM AD MAX,ARRAY-1
02038 TFM ADOUT,READ
02039 S ADOUT,ACC
02040 RACDHEADER,,, READ AND TYPE A HEADER CARD
02041 RCTY
02042 TA HEADER+80*2-1,NUM SSP-1+10*2
02043 WATYHEADER
02045 BLC *+12
02050IM BLC SORT B
02060 RNCOREAD-79
02070SORT1 SF
02071SETFLGDS **5
02080 TFM N,1,10
02081 TFM ADM,ARRAY
02082 A ADM,ACC
02083 S ADM,N,1,10
02090SORT2 C N,MAX
02100 BP SORT3
02110 C -ADIN,-ADM
02120 BP SORT3
02121 AM N,1,10
02122 A ADM,ACC
02123 B SORT2
02130SORT3 A ADMAX,ACC
02140 TF ADK1,ADM
02150 AM ADK1,1,10
02160 TF ADK2,ADK1
02170 S ADK2,ACC
02180 TR -ADMAX,-ADK2
02190 TR -ADK1,-ADMAX
02200 TF -ADM,-ADIN
02210 AM MAX,1,10
02220 B IN
02230SORT8 TFM N,1,10
02235 TD READ,REC
02240 TFM ADM,ARRAY
02250 SM ADM,1,10
02260 RCTY
02263 A ADM,ACC
02270SORT9 TBTY
02280 BT NO FLAG,N
02300 TF READ-1,-ADM
02310 BTM SUPPR,*+12
02320 C N,MAX
02330 BNN SORTF
02340 A ADM,ACC
02350 AM N,1,10
02360 B SORT9
```

COMPARISON WITH AN INPUT DIFFERENCE *

```
0310SEARCHRCTY
03020 WATYDIFF
03030 TF SUB+42,*+23
03040 B SUB,SRCH1,7
03050SRCH1 TF PRE,-ADIN
03070 WATYFIT
03080 TF SUB+42,*+23
03090 B SUB,SRCH2,7
03100SRCH2 TF D,READ-77
03110 TFM N,0,10
03120 TFM ADM,ARRAY
03130 SM ADM,1,10
03140SRCH3 AM N,1,10
03150 A ADM,ACC
03160 TF READ-70,-ADM
03170 S READ-70,PRE
03180 TF READ-60,READ-70
03190 A READ-70,D
03200 S READ-60,D
04010 TF ADMUM,ADM
04020 TF NUM,N
04030SRCH4 AM NUM,1,10
04040 A ADMUM,ACC
04050 C NUM,MAX
04060 BP SRCHF
04070 C READ-70,-ADMUM
04080 BNN SRCH4
04090 C READ-60,-ADMUM
04100 BP SRCH3
04105 RCTY
04110 BT NO FLAG,N
04130 BT NO FLAG,NUM
04140 TF READ-1,-ADM
04150 S READ-1,-ADMUM
04160 BTM SUPPR,*+12
04170 B SRCH4
```

LOOKING FOR EQUAL SPACING PAIRS *

```
05010HUNT RCTY
05020 WATYFIT
05030 TF SUB+42,*+23
05040 B SUB,HUNT1,7
05050HUNT1 TF D,READ-77
05060 TFM N,0,10
05061HSTOP WATYLM
05062 PNTYSARE
05063 BCL *+12
05064 TFM ADM,ARRAY
05065 SM ADM,1,10
05070HUNT2 AM N,1,10
05075 TF NUM,N
05080 AM NUM,1,10
05081 A ADM,ACC
05082 TF ADMUM,ADM
05083 A ADMUM,ACC
05085 TDM SPACE,0
05090 C NUM,MAX
05100 BNN HUNTF
05110HUNT3 TDM DONT,0
05120 TF READ-70,-ADM
05130 S READ-70,-ADMUM
05131 C READ-70,DMAX
05132 BP HUNT2
05133 C READ-70,DMIN
05134 BNN HUNT2
05140 TF READ-1,READ-70
05150 TF READ-50,READ-70
05160 A READ-50,D
05170 S READ-70,D
05180 TF K1,N
05190 TF ADK1,ADM
05200HUNT4 AM K1,1,10
05205 A ADK1,ACC
05210 TF K2,K1
06001 TF ADK2,ADK1
06002HUNT5 AM K2,1,10
06003 A ADK2,ACC
06010 C K2,MAX
06020 BP HUNT6
06030 TF READ-60,-ADK1
06040 S READ-60,-ADK2
06050 C READ-60,READ-70
06060 BNN HUNTS
06070 C READ-60,READ-50
06080 BP HUNTA
06090 BTM NOMP,0,10
06090 BTM HUNT9,DONT
06095 RCTY
06100 RCTY
06101 BD HUNT11,SPACE
06102 TDM SPACE,1
06103 RCTY
```

```
06110HUNT11BT NO FLAG,N
06130 BT NO FLAG,NUM
06150 BTM SUPPR,*+12
06170 TDM DONT,1
06175HUNT9 TBTY
06180 BT NO FLAG,K1
06200 BT NO FLAG,K2
07020 TF READ-1,READ-60
07030 BTM SUPPR,*+12
07050 B HUNTS
07060HUNT6 AM NUM,1,10
07065 BC3 HST
07070 A ADMUM,ACC
07075 C NUM,MAX
07080 BNN HUNT3
07090 B HUNT2
07091HST RCTY
07092 RNTY-N-1
07093 SF N-1
07094 MF TOP ST,N
07095 SM N,1,10
07095 TFM ADM,ARRAY-1,7
07096 M N,ACC
07097 SF 01095
07098 A ADM,01099
07099 B HUNT2
09001NOFLAGTF RT,*-1,REMOVES FLAG
09002 BD *+24,RT-2
09003 TDM RT-3,0,,SUPPRESS ZERO
09004 WATYRT-2
09005 BB
09006RT DSC S,*+12
09007 DS S
```

ROUTINE TO SUPPRESS INFORMATION PREVIOUSLY TYPED *

```
09009STOPST DS 39999
09010HSTOP TF
09020 TF ADTEST,K1
09030 MF ADTEST,ADTEST-1
09040 TFM ADSUP,TOP ST
09050 BNF PUT,ADSUP,11
09060 C -ADSUP,ADTEST
09070 BZ HUNTS
09080 SM ADSUP,4,10
09090 B LOOK
09100HPUT TF ADSTOP,ADSUP
09110 SM ADSTOP,4,10
09120 C ADSTOP,ADMAX
09130 BP PUTIN
09140 BB
09150PUTIN TDM -ADSTOP,0
09160 TF -ADSUP,ADTEST
09170 BB
```

STORAGE ALLOCATIONS *

```
07100ADIN DS
07105ADOUT DS
07110ADM DS
07115ADMUM DS
07116ADIT DS
07117ADMAX DS
07120ACC DS
07130NUMSTTDAC 19 ,NUMBER STARTS COL @
07135NUMSTPDAC 11 ,STOPS COL @
07140MAX DS 2
07150SW1 DAC 30,SW1 ON LOOK FOR SET PAIR DIFF**
07151 DAC 26 ,OFF COMPARE PAIR SPACING**
07160NUM DS 2
07180SW2 DAC 25,SW2 OFF TO READ NEW DATA@
07190 DS 2
08010HEAD1 DAC 45,DIFFERENCES OF LESS THAN 98 INTEGER WAVE NOS@
08015HEAD3 DAC 13 ,TURN SW3 OFF@
08020READ DS 80
08030PRE DS 10
08031ADK1 DS 5
08037ADK2 DS 5
08040FIT DAC 20,ACCURACY (3 DIGITS)@
08050 DS 4
08060DONT DS 1
08065SPACE DS 1
08070K1 DS 2
08080REC DS 1,*
08100K2 DS 2
08115SPARE DS 1
08112DMAX DC 4,1000
08113 DC 5,0
08114ADM DC 2,0
08114LM DAC 15 , UPPER LIMIT*
08120DIFF DAC 27,SET DIFFERENCE ( DIGITS)@
08125TAB DAC 17 , SET TAB HERE*
08126ADTEST DS 4
08127ADSTOP DS 4
08128ADSTOP DS 4
08130ARRAY DC 1,*
08135HEAD0 DS 2
08140 DEMOSTART
```

COMMON DIFFERENCES TABLE

```

**11 12.14 SAME DIFFERENCES
*0605
C READ TWO SPECTRA, OUTPUT DIFFERENCES
C NEARLY COMMON TO BOTH
2 PRINT 20
20 FORMAT(11HMAXIMUM/FIT)
21 ACCEPT 100, NO GO, NEAR
DIMENSION KODE(20), IDENTA(780), IDENTB(780),
1 NUMSA(780), NUMSB(780), IDIOT(40)
COMMON NO GO, NUMSB
EQUIVALENCE (IDIOT(40), NUMSB(780))
DO 1 I=1, 40
1 IDIOT(I)=0
CALL DIFFER(KODE, IDENTA, NUMSA, NA, NOA)
CALL DIFFER(KODE(10), IDENTB, NUMSB, NB, NOB)
C
C PUNCH A HEADER
C PUNCH 10, KODE
10 FORMAT(10A2, 13X, 10A2)
100 FORMAT(E10.4)
CALL DIF OUT (NUMSA, NOA, NUMSB, NOB,
1 NEAR, IDENTA, IDENTB)
IF (SENSE SWITCH 1) 21, 2
END

```

```

**11 12.14 INPUT AND FIND DIFFERENCES
*0605
SUBROUTINE DIFFER(KODE, IDENT, NUMS, N, ND)
DIMENSION KODE(10), IDENT(30), NUMS(30), INPUT(40), IDIOT(40)
COMMON NO GO, IDIOT
N=0
IF (SENSE SWITCH 9) 1, 1
1 READ 10, KODE
10 FORMAT(10A2)
11 N=N+1
IF (N=40) 13, 13, 12
12 PRINT 120
120 FORMAT(7HOVERLAP)
PAUSE
GO TO 2
13 READ 110, INPUT(N)
110 FORMAT(25X, 15)
IF (SENSE SWITCH 9) 2, 2, 11
2 CALL SORT(INPUT, IDIOT, N)
C
C PUNCH OUT
C PUNCH 20, KODE, (1, INPUT(1), 1=1, N)
20 FORMAT(10A2/(10I6))
PUNCH 200
200 FORMAT(/)
C
C LOOP TO FIND DIFFERENCES
ND=0
NDST=N-1
DO 4 I=1, NDST
4 JST=I+1
DO 5 J=JST, N
C
C ITRY=INPUT(J)-INPUT(I)
IF (ITRY-ND GO) 3, 4, 4
3 ND=ND+1
NUMS(ND)=ITRY
IDENT(ND)=1000*I+J
CONTINUE
CONTINUE
C
C HAVE ARRAY, SORT
CALL SORT(NUMS, IDENT, ND)
RETURN
END

```

SORT
AS FOR ABSORBANCE PROGRAM 2

```

**11 12.14 OUTPUT
*0605
SUBROUTINE DIF OUT (LISTA, MAXA, LISTB, MAXB, NEAR, IDENTA, IDENTB)
C
C LISTS A AND B OF GIVEN LENGTH, FIT TO
C TOLERANCE NEAR
C
DIMENSION LIST A(20), LIST B(20), KARD(24), KARDB(12)
DIMENSION IDENTA(20), IDENTB(20)
EQUIVALENCE (KARD(13), KARDB)
I=1
DO 11 K=1, 24
11 KARD(K)=0
C
C TEST FOR FIT
1 IS IT=LISTA(1)-LISTB(J)
IF (ABS (IS IT)-NEAR) 3, 3, 2
C
C NOT FIT
2 IF (IS IT) 21, 3, 22
21 I=I+1
IF (I-MAX A) 1, 1, 9
22 J=J+1
IF (J-MAX B) 1, 1, 9
C
C TWO FIT
NI=1
NJ=1
NEXT=1
300 INDEX=3*NI
KARD(INDEX)=LISTA(I)
INDEX=INDEX-1
KARD(INDEX)=IDENTA(I)
GO TO (301, 53), NEXT
301 INDEX=3*NJ
KARDB(INDEX)=LISTB(J)
INDEX=INDEX-1
KARDB(INDEX)=IDENTB(J)
GO TO (4, 43), NEXT
C
C
C LASTRY=1
IF (J-MAXB) 41, 5, 5
41 IF (ABS (LISTA(I)-LISTB(J+1))-NEAR) 42, 42, 5
42 LASTRY=0
NJ=NJ+1
J=J+1
NEXT=2
GO TO 301
C
C SEE IF PUNCHING ARRAY FULL
43 IF (NJ=4) 5, 8, 8
C
C
C I=I+1
IF (I-MAX A) 51, 51, 6
51 IF (ABS (LIST A(I)-LIST B(J))-NEAR) 52, 52, 6
C
C
C NI=NI+1
NEXT=2
GO TO 300
52 IF (NI=4) 4, 8, 8
C
C TEST USEFULNESS OF LAST J
6 IF (LASTRY) 7, 61, 7
61 I=I-1
GO TO 4
C
C NO USE, PUNCH IF ANY OUTPUT
7 IF (NI+NJ) 1, 1, 8
C
C
C OUTPUT PUNCH ROUTINE
C
C RESET NI AND NJ
NI=NI/4
NJ=NJ/4
NUMSAV=KARD(11)
DO 81 K=2, 20, 3
KARD(K-1)=KARD(K)/1000
KARD(K)=KARD(K)-KARD(K-1)*1000
81
C
C PUNCH
80 PUNCH 80, (KARD(K), K=1, 9), (KARD(K), K=13, 21)
FORMAT(5(13, 13, 15))
KARD(2)=NUMSAV
KARD(3)=KARD(12)
DO 82 K=4, 21
82 KARD(K)=0
KARD(14)=KARD(23)
KARD(15)=KARD(24)
C
C CARD NOW RESET FOR NEXT PUNCH,
C FIND RE-ENTRY POINT
C
IF (NI+NJ) 4, 1, 4
C
C NO FURTHER INTEREST
9 PRINT 90
90 FORMAT(8HFINISHED)
RETURN
END

```

EIGENVALUES AND EIGENVECTORS OF MATRIX UP TO ORDER 35

*011 12.14 EIGENVALUES AND EIGENVECTORS

*0808

DIMENSION N ELS(2),DUM(633),DIAG(35),OFFO(595),V(35,35)
DIMENSION NAME(5),ROW(39),MASK(39),LS(39)
LAST FEW ARE TEMPORARY STORAGE ONLY

C

C

COMMON A,D,I,OUH,DUMMY,MASK,LS,NAME,ROW,MASBI,NBLOX,TRACE,SUMSQ,
1 HASOIV,PARAM,NBL,M ROW,M COL,M STOP,LEN,NT OR 1.
2 N CD,LSJM,N OD,L,MASBIT,N
EQUIVALENCE (N ELS(1),N ORD),(N ELS(2),N OFF),(DUMMY,V(1225)),
1 (DUM(1),FINAL),(DUM(2),ORDER),(DUM(3),TEST).
2 (DUM(38),DIAG(35),OFFO(0))

C

C

EQUIVALENCE TO LOOK AT REMAINDER
DIMENSION MAIN(4986)
EQUIVALENCE (MAIN(4986),I),(MAIN(1),MAINOR)
IF YOU CHANGE THE FIELD LENGTHS
THE GREMLINS WILL GET YOU

C

C

H37=37
999 IF(SENSE SWITCH 9)1,1
C SEGMENT INPUT IF NECESS
1 IF(SENSE SWITCH 3)160,100
100 N ORD=0
DO 10 I=1,630
DIAG(I)=0.

10

C

C

READ MATRIX HEADER
11 READ 110,NAME,N BLOX,MASDIV
110 FORMAT(5A4,15,15)
PRINT 110,NAME
ACCEPT 120,PARAM
DO 199 N BL=1,N BLOX

C

C

READ HEADER FOR BLOCK OF MATRIX
READ 1200,M ROW,M COL,M STOP,LEN
1200 FORMAT(5I10)
120 FORMAT(5E14,0)

C

C

NT OR 1=1/(LEN+1)
C NO OF VALUES FOR FIRST ROW, 1 IF LEN=0
N IN ROW=LEN+NT OR 1
N CD=1

C

C

READ CORRECT NUMBER OF ELEMENTS
1201 READ 120,LSJM,(ROW(1),I=1,N IN ROW)
IF(MASDIV=1)12,12,13

C

C

FIRST MATRIX DEFINES STATES
I=1
IF(NORO)123,123,121
DO 122 I=1,NORO
IF(LSJH-MASK(I))122,1235,122
122 CONTINUE
123 MASK(I)=LSJM
NORO=NORO+1

C

C

FIND COLUMN TO PUT IT IN
1235 IF(N CD=1)124,124,126
124 DO 125 J=1,I
IF(M COL-MASK(J))125,126,125
125 CONTINUE
GO TO 499

C

C

TRANSFER ROW
126 K=(I-3)*1/2+1+J
C IS DIAGONAL ELEMENT THERE
N OD=N IN ROW
IF(LEN*(J+LEN-1-I))128,127,128
127 OIAG(I)=ROW(N IN ROW)*PARAM+OIAI(I)
N OD=N OD-1

128

C

CONTINUE
ANY OFF-DIAGONAL
IF(N OD)131,131,129
DO 130 L=1,N OD
OFFO(K)=ROW(L)*PARAM+OFFO(K)

129

C

K=K+1
130 N IN ROW=N IN ROW+NT OR 1
N CO=N CO+1

131

C

IF(LSJH-MSTOP)1201,199,1201

C

C

NOT FIRST MATRIX,SEARCH MORE THOROUGHLY
MAS BI =LSJM/MASDIV
LS(N CD)=MAS BI
DO 149 I=1,N ORD
IF(ABSF(MASK(I)/MASOIV)-MASBI)149,132,149
132 N OFF=MAINOR
K=(I-3)*1/2+1
DO 148 J=1,N ORD
K=K+1
MAS BIT=ABSF(MASK(J)/MAS DIV)

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

IF THIS AND THE PREVIOUS REMAINDER NOT THE SAME, GO ON

IF(NOFF-MAINOR)148,1325,148

DO 147 N=1,N CO

IF(LS(N)-MAS BIT)147,133,147

FOUND ONE THAT FITS

TRANSFER

133 A=ROW(N)*PARAM

134 DIAGONAL

DIAG(I)=DIAG(I)+A

GO TO 147

139 IF(N=N CO)136,147,138

J I TH ELEMENT

138 K=(J-3)*J/2+1+I

135 OFFO(K)=OFFO(K)+A

147 CONTINUE

148 CONTINUE

149 CONTINUE

PREPARE TO READ NEXT CARD

GO TO 131

MORE BLOCKS WANTED

199 CONTINUE

NO, ANY MORE MATRICES THERE

IF(SENSE SWITCH 9)200,11

SEGMENT INPUT

160 READ 120, N ELS,(OFFO(I),I=H37,N OFF),

3 ((V(I,J),I=1,N ORD),J=1,N ORD)

GO TO 211

FIND SUM OF SQUARES FOR NORM

SUMSQ=0.

TRACE=0.

N OFF=N ORD*(N ORD-1)/2

DO 201 I=1,N OFF

SUMSQ=SUMSQ+OFFO(I)**2

SUMSQ=SUMSQ*2.

DO 202 I=1,N ORD

A=DIAG(I)

TRACE=TRACE+A

SUMSQ=SUMSQ+A*A

PRINT 2020,TRACE,SUM SQ

FORMAT(6HTRACE E14.7/6HSUMSQ E14.7//6HSTATES)

OROR=N ORD

SET FINAL CRITERION

FINAL=SUMSQ*1.E-16/OROR

TEST=SUM SQ

198 PUNCH 190,(MASK(I),I=1,N ORD)

190 FORMAT(111,4114)

PRINT 190,(MASK(I),I=1,N ORD)

NEARLY READY TO ROLL

DO 197 I=1,N ORD

DO 196 J=1,N ORD

V(I,J)=0.

V(I,I)=1.

NOW MATRIX IS STORED WITH OIAG(I) AS

DIAGONAL ELEMENTS, OFFO(I) NON-DIAGONAL

ELEMENTS OF LOWER HALF OF MATRIX STORED

IN ROWS OF INCREASING LENGTH

N ORD ORDER OF MATRIX,N OFF LENGTH OF OFFO

```

C      REDUCE NORM FOR A TEST
210  TEST=TEST/ORDER
211  INSIG=0
      I OFFD=0
      I ROW ST=0
      DO 299 J=2,N ORD
C      LOOP OVER ROWS
      N IN ROW=1-1
      I ROW ST=I ROW ST+1-2
      J ROW ST=1
C      LOOP OVER A COLUMN
      DO 299 J=1,N IN ROW
      J ROW ST=J ROW ST+J-2
      I OFFD=I OFFD+1
      A=OFFD(I OFFD)**2
      IF (SENSE SWITCH 3) 510,212
212  IF (A-TEST) 299,299,215
C      PREPARE FOR ROTATION
215  O=DIAG(I)
      T=0.5*(DIAG(J)+D)
      O=T-D
      SURO=SQRT(A+D*O)
      A=1./SQRT(A+(O-SURO)**2)
      COSINE=A*OFFD(I OFFD)
      SANE=(SURO-D)*A
      DIAG(I)=T+SURO
      DIAG(J)=T-SURO
      OFFD(I OFFD)=0.
      INSIG=1
C      NOW ROTATE ELEMENTS AND VECTOR MATRIX
C
      DO 299 K=1,N ORD
      IF (K-J) 270,220,240
220  K J=K+J ROW ST
230  K I=K+I ROW ST
C      K J IS NOW EFFECTIVELY (K ROW ST+J), K I SIMILAR
C      FOR K ABOVE I,J, ADD LENGTH OF (K-1)TH ROW
      GO TO 295
240  K J=K J+K-2
      IF (K-I) 280,230,250
250  K I=K I+K-2
      GO TO 290
270  K J=K+J ROW ST
280  K I=K+I ROW ST
290  A KJ=OFFD(K J)
      A KI=OFFD(K I)
      OFFD(K J)=COSINE*A KI-SANE*A KJ
      OFFD(K I)=SANE*A KI+COSINE*A KJ
C
C      NOW EIGENVECTORS
C
295  A KJ=V(J,K)
      A KI=V(I,K)
      V(J,K)=COSINE*A KI-SANE*A KJ
      V(I,K)=SANE*A KI+COSINE*A KJ
C
299  CONTINUE
C
C      TEST WHETHER ALL ELEMENTS BELOW LIMIT
C
      IF (INSIG) 211,298,211
298  IF (TEST-FINAL) 300,300,210
C
C      OUTPUT
C
300  DO 301 I=1,N ORD
      PUNCH 30,DIAG(I),(V(I,J),J=1,N ORD)
30  FORMAT(E14.7,(5F14.8))
      PRINT 30,DIAG(I)
32  PRINT 77F12.5
      IF (SENSE SWITCH 1) 301,31
31  PRINT 310,(V(I,J),J=1,N ORD)
310  FORMAT(5F14.8)
301  CONTINUE
      GO TO 999
C
C      OUTPUT
C
510  PUNCH 120,N ELS,(OFFD(I),I=M37,N OFF),
3 ((V(I,J),I=1,N ORD),J=1,N ORD)
C
499  CONTINUE
      END

```

PROGRAM TO READ MATRICES IN SURD FORM

**11 12.14 E AND E INPUT PREPARATION

*0808

DIMENSION DIAG(42),OFFD(861),DUM(903),NAME(5),
1 ROW(42),SA(42),SB(42),SC(42),MASK(42),LS(42),M ST(42),M CL(42)
EQUIVALENCE (DUM(42),OFFD(0),DIAG(42))
COMMON A,D,I

C EQUIVALENCE TO LOOK AT REMAINDER
C DIMENSION MAIN(4986)
C EQUIVALENCE (MAIN(4986),I),(MAIN(1),MAINDR)
C IF YOU CHANGE THE FIELD LENGTHS
C THE GREMLINS WILL GET YOU

9999 IF(SENSE SWITCH 9)100,100
100 N ORD=0
DO 10 I=1,903
DIAG(I)=0.

C READ MATRIX HEADER
C READ 110,NAME,N BLOX,MASDIV
110 FORMAT(SA4,I5,I5)
PRINT 110,NAME
ACCEPT 120,PARAM
DO 199 N BL=1,N BLOX

C READ HEADER FOR BLOCK OF MATRIX
C READ 1200,M ROW,M COL,M STOP,LEN
1200 FORMAT(5I10)

120 FORMAT(5E14.0)
NT OR I=1/(LEN+1)
C NO OF VALUES FOR FIRST ROW, 1 IF LEN=0
N IN ROW=LEN+NT OR 1
N CD=1

IF(N IN ROW=NORD-1)1201,1201,51
C READ CORRECT NUMBER OF ELEMENTS
1201 READ 1210,LSJM,(SA(1),SB(1),SC(1),I=1,N IN ROW)
1210 FORMAT(110/(15I5))
DO 1203 I=1,N IN ROW
ROW(I)=0,
IF(SB(I))1202,1203,1202
1202 ROW(I)=SA(I)/SB(I)*SQRT(SC(I))
1203 CONTINUE
IF(MASDIV-1)12,12,13

C FIRST MATRIX DEFINES STATES
C I=1
12 IF(NORD)123,123,121
121 DO 122 I=1,NORD
IF(LSJH=MASK(I))122,1235,122
122 CONTINUE
123 MASK(I)=LSJM
NORD=NORD+1
IF(N ORD=42)1235,1235,6

C FIND COLUMN TO PUT IT IN
1235 IF(N CD=1)124,124,126
124 DO 125 J=1,I
IF(M COL=MASK(J))125,126,125
125 CONTINUE
GO TO 499

C TRANSFER ROW
126 K=(I-3)*1/2+1+J
C IS DIAGONAL ELEMENT THERE
N OD=M IN ROW
IF(LEN*(J+LEN-1-1))128,127,128
127 DIAG(I)=ROW(N IN ROW)*PARAM+DIAG(I)
N OD=M OD-1
128 CONTINUE

C ANY OFF-DIAGONAL
IF(N OD)131,131,129
129 DO 130 L=1,N OD
OFFD(K)=ROW(L)*PARAM+OFFD(K)
130 K=K+1
131 N IN ROW=N IN ROW+NT OR 1
N CD=N CD+1

C IF(LSJH=MSTOP)1201,199,1201

C NOT FIRST MATRIX,SEARCH MORE THOROUGHLY
13 MAS BI =LSJM/MASDIV
LS(N CD)=MAS BI
DO 149 I=1,N ORD
IF(ABSF(MASK(I)/MASDIV)-MASBI)149,132,149
132 N OFF=MAINDR
K=(I-3)*1/2+1
DO 148 J=1,N ORD
K=K+1
MAS BIT=ABSF(MASK(J)/MAS DIV)

C IF THIS AND THE PREVIOUS REMAINDER NOT THE SAME, GO ON
C IF(NOFF=MAINDR)148,1325,148

1325 DO 147 N=1,N CD
IF(LS(N)-MAS BIT)147,133,147
FOUND ONE THAT FITS

C TRANSFER
133 A=ROW(N)*PARAM
IF(I=J)139,134,135
DIAGONAL

134 DIAG(I)=DIAG(I)+A
GO TO 147
139 IF(N=N CD)138,147,138

C J I TH ELEMENT
138 K=(J-3)*1/2+1
135 OFFD(K)=OFFD(K)+A
147 CONTINUE
148 CONTINUE
149 CONTINUE

C PREPARE TO READ NEXT CARD
C GO TO 131

C MORE BLOCKS WANTED
199 CONTINUE
C NO, ANY MORE MATRICES THERE
IF(SENSE SWITCH 9)200,11

C ACCEPT LABEL

200 PRINT 210
210 FORMAT(13HNAME/MASK DIV)

ACCEPT 110,NAME
N BLOX=1
NUFF=0
IR=1
LEFT=1
IROW=1

C ACCEPT 120,MAS DIV
SET TO 1 IF NOTHING ENTERED
MAS DIV=MASDIV+1/(1+MASDIV)
GO TO 21

C LOOK FOR AN EMPTY BLOCK
23 DO 22 IROW=IR,NORD
K=K+1 ROW=2
L=K+LEFT
DO 22 I COL=LEFT,NUFF
IF(OFFD(L))25,22,25

22 L=L+1
IROW=IR
C A BLOCK COMPLETE
LEFT=NUFF+1
M ST(N BLOX)=MASK(IR-1)
N BLOX=N BLOX+1
M CL(N BLOX)=MASK(IR)
21 NUFF=IROW
25 IR=IROW+1

K=(IR-2)*(IR-3)/2
IF(IR=NORD)23,23,26

C MATRIX COVERED
26 M ST(N BLOX)=MASK(NORD)

C NOW READY TO PUNCH MATRIX

C PUNCH 110,NAME,N BLOX,MASDIV
IR=0
DO 5 N BL=1,N BLOX
MSLST=M ST(N BL)
PUNCH 1200,M CL(N BL),M CL(N BL),MSLST
IR=IR+1
PUNCH 120,MASK(IR),DIAG(IR)
IF(MASK(IR)-MSLST)3,5,3

3 LEF=IR
4 LEFT=IR*(IR-1)/2+LEF
IRP=IR+1
NUFF=IR*(IR+1)/2
PUNCH 120,MASK(IRP),(OFFD(I),I=LEFT,NUFF),DIAG(IRP)
IR=IR+1
IF(MASK(IRP)-MSLST)4,5,4
CONTINUE

C FINISHED PUNCHING
PRINT 60,N ORD
GO TO 9999

C SPECIFICATION ERROR
499 PRINT 4990,M COL
4990 FORMAT(6HCOLUMN 19, 9HUNDEFINED)
PAUSE

GO TO 9999
51 PRINT 50
50 FORMAT(13HOVER DIAGONAL)
GO TO 1201
6 PRINT 60,N ORD
60 FORMAT(SHORDER 13)
PAUSE
GO TO 9999
END

ENERGY TABLE AND PARAMETER DEPENDENCE

**11 12.14 ENERGY TABLE

```
*0808
  DIMENSION NICE(7)
  NICE(1)=6200
  NICE(2)=5700
  NICE(3)=4400
  NICE(4)=4600
  NICE(5)=4700
  NICE(6)=4800
  NICE(7)=4900
  N ORD=0
  DIMENSION VAL(60), LABEL(60), P(300)
  K=1
  NUM=1
  READ 3 PARAMETER VALUES
  DIMENSION PARAM(6)
  READ 110, PARAM
  FORMAT(A4, E14.8)
  DIMENSION OP(20), OQ(20), OR(20), OP(190), OQ(190), OR(190)
  IF(SENSE SWITCH 9)11,11
  DO 12 I=1,630
  OP(I)=0.
  READ 3 MATRICES FOR 1 REP
  DIMENSION NAME(9)
  CALL READ M(OP, OP, NAME, N ORD)
  CALL READ M(OQ, OQ, NAME(3), N ORD)
  CALL READ M(OR, OR, NAME(6), N ORD)
  PRINT 120, NAME
  FORMAT(9A4)
  READ 120, REP
  READ MASKS
  DIMENSION MASK(20), VEC(20)
  READ 10, MASK(1), I=1, N ORD)
  FORMAT(111, 4114)
  DO 4 L=1, N ORD
  READ 100, VAL(NUM), TEST, (VEC(I), I=1, N ORD)
  FORMAT(2E14.7 / (5E14.8))
  IF(TEST)2,3,2
  PRINT 20
  FORMAT(11HWRUNG ORDER)
  PAUSE
  GO TO 15
  P(K)=REP
  FIND MAIN COMPT
  TEST=0.
  DO 31 J=1, N ORD
  TRY=ABS(VEC(J))
  IF(TRY-TEST)31,32,32
  MAS=MASK(J)
  TEST=TRY
  CONTINUE
  MAKE MASK PRESENTABLE
  MULT=ABS(MAS/1 000 000)
  ML=ABS(MAS*100/1 000 000)
  LABEL(NUM)=K
  K=K+1
  P(K)=7000 0000+MULT*100 0000+NICE(ML+1)
  PARAMETER DEPENDENCE
  K=K+1
  CALL PROD(OP, OP, P(K), N ORD, VEC)
  K=K+1
  CALL PROD(OQ, OQ, P(K), N ORD, VEC)
  K=K+1
  CALL PROD(OR, OR, P(K), N ORD, VEC)
  NUM=NUM+1
  K=K+1
  IF(SENSE SWITCH 9)5,11
  SORT INTO ORDER
  NUM=NUM-1
  CALL SORT(VAL, LABEL, NUM)
  OUTPUT
  PUNCH 50, PARAM, PARAM(1), PARAM(3), PARAM(5)
  FORMAT(3(A4, F10.3 /) / 13X, 4HMAIN 6X, 2UHPARAMETER DEPENDENCE /
  1 6HENERGY 2X, 4HREPR 2X, 5HSTATE 3(5X, A4) /)
  DO 6 I=1, NUM
  K=LABEL(I)
  KP4=K+4
  EVAL=VAL(I)-VAL(NUM)+0.5
  PUNCH 60, EVAL, (P(L), L=K, KP4), VAL(I)
  FORMAT(16, 3X, A3, 3X, A4, 3F9.5, 4X, F12.5)
  CONTINUE
  GO TO 1
  END
```

**11 12.14 SORT TO DECREASING ORDER

```
*0808
  SUBROUTINE SORT(X, KK, N)
  DIMENSION X(10), KK(10)
  M=N
  M=M/2
  IF(M)30, 40, 30
  K=N-M
  J=1
  L=1+M
  IF(X(1)-X(L))50, 60, 60
  A=X(1)
  X(1)=X(L)
  X(L)=A
  IA=KK(1)
  KK(1)=KK(L)
  KK(L)=IA
  I=1-M
  IF(I-1)60, 49, 49
  J=J+1
  IF(J-K)41, 41, 20
  RETURN
  END
```

**11 12.14 READ MATRIX

```
*0808
  SUBROUTINE READ M(DIAG, OFFD, NAME, N ORD)
  PARAM=1.
  DIMENSION DIAG(5), NAME(3), ROW(35), MASK(35), OFFD(25)
  COMMON ROW
  N ORD=0
  READ HEADER
  READ 110, NAME, N BLOX
  FORMAT(3A4, 8Y, 15)
  DO 199 N BLOC=1, N BLOX
  READ HEADER FOR BLOCK OF MATRIX
  READ 120J, M ROW, M COL, M STOP, LEN
  FORMAT(5110)
  120J FORMAT(5E14.0)
  NT OR 1=1/(LEN+1)
  NO OF VALUES FOR FIRST ROW, 1 IF LEN=0
  N IN ROW=LEN+NT OR 1
  N CO=1
  READ CORRECT NUMBER OF ELEMENTS
  120J READ 120, LSJM, (ROW(I), I=1, N IN ROW)
  12 I=1
  IF(NORD)123, 123, 121
  121 DO 122 I=1, NORD
  IF(LSJM-MASK(I))122, 1235, 122
  122 CONTINUE
  123 MASK(I)=LSJM
  NORD=NORD+1
  FIND COLUMN TO PUT IT IN
  1235 IF(N CO-1)124, 124, 126
  124 DO 125 J=1, 1
  IF(M COL-MASK(J))125, 126, 125
  125 CONTINUE
  STOP
  TRANSFER ROW
  126 K=(I-3)*I/2+1+J
  IS DIAGONAL ELEMENT THERE
  N OD=N IN ROW
  IF(LEN*(J+LEN-1-1))128, 127, 128
  DIAG(I)=ROW(N IN ROW)*PARAM+DIAG(I)
  N OD=N OD-1
  CONTINUE
  ANY OFF-DIAGONAL
  IF(N OD)131, 131, 129
  129 DO 130 L=1, N OD
  OFFD(K)=ROW(I)*PARAM+OFFD(K)
  K=K+1
  N IN ROW=N IN ROW+NT OR 1
  N CO=N CO+1
  IF(LSJM-MSTOP)120J, 199, 120J
  MORE BLOCKS WANTED
  199 CONTINUE
  RETURN
  END
```

**11 12.14 VAV PRODUCT

```
*0808
  SUBROUTINE PROD(D, OO, P, N ORD, VEC)
  DIMENSION D(10), OD(35), VEC(10)
  P=0(1)*VEC(1)**2
  K=0
  DO 2 I=2, N ORD
  J MAX=I-1
  DO 3 J=1, J MAX
  K=K+1
  P=P+VEC(I)*OD(K)*VEC(J)*2.
  3 P=P+0(1)*VEC(I)**2
  RETURN
  END
```